

Diffusion in the matrix of granitic rock. Field test in the Stripa mine. Final report

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DIFFUSION IN THE MATRIX OF GRANITIC ROCK FIELD.TEST IN THE STRIPA MINE FINAL REPORT

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This report concerns a study which was conducted for SKB. The conclusions and viewpoints presented in the report are those of the author(s) and do not necessarily coincide with those of the client.

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FIELD TEST IN THE STRIPA MINE.

FINAL REPORT.

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SUMMARY

Three similar migration experiments in the matrix of granitic rock have been performed and are presented. The experiments have been carried out in "undisturbed" rock, that is rock under its natural stress environment. Since the experiments were performed at the 360 m level in the Stripa Mine (Stripa, Sweden), the rock was subjected to nearly the same conditions as the rock surrounding a nuclear waste repository as proposed in the Swedish concept (SKB) where the nuclear waste is to be stored in canisters at approximately 500 m depth in crystalline rock.

A mixture of three nonsorbing (conservative) tracers, Uranine, Cr-EDTA, and I^- , were injected into the granitic rock matrix for three different time periods: about 3 months, about 6 months, and about 3.5 years. The subsequent overcorings of the injection holes showed that the tracers had in some cases migrated at least about 400 mm (measuring limit) into the rock matrix for the experiment with the longest injection time. It could also be seen that there were large differences in migration distance into the rock matrix for samples taken fairly close to each other.

The results from all three experiments showed that all three tracers had migrated through the disturbed zone close to the injection hole, through the fissure coating material, and a distance into the "undisturbed" rock matrix.

These results therefore indicate that it is possible for dissolved compounds to migrate into the rock matrix. This migration into the rock matrix will permit the uptake of dissolved species in water flowing in fractures and will increase the area available for sorption of sorbing radionuclides significantly and therefore retard the radionuclides by order(s) of magnitude.

Diffusivities and hydraulic conductivities obtained in this in-situ experiment compare well with those obtained in laboratory experiments.

1. BACKGROUND

Our present concept of the micro structure of granite is illustrated in Figure 1.1 (Neretnieks, 1980).



Figure 1.1. A two-dimensional view of the micro structure of granite showing "typical" sizes of grains, microfissures, and fissures.

The granite is intersected by a number of fissures in which water flows. In the rock matrix, a connected pore system (microfissure system) exists where molecules can move by diffusion. The fissures are sometimes coated with a thin layer of fissure coating material, which the molecules must diffuse through before they can penetrate the pore system within the rock matrix.

In the Swedish repository concept it is proposed that the nuclear waste is to be stored in canisters at approximately 500 m depth in crystalline rock. The canisters may eventually degrade in time and the radionuclides may then be transported away by the seeping water in the fissures. The radionuclides migrating with the seeping water may be considerably retarded if they diffuse into the rock and sorb on the surfaces of the microfissures in the rock matrix (Neretnieks, 1980).

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The importance of matrix diffusion is illustrated in Figure 1.2 where projected breakthrough curves for some radionuclides in a decay chain at a long distance from the waste storage are shown for surface sorption and surface sorption + matrix diffusion (Rasmuson et al, 1982).



Figure 1.2. The influence of matrix diffusion. $D_p \epsilon_p = 10^{-1/2} \text{ m}^2/\text{s}$.

From Figure 1.2 and the discussion above it is obvious that diffusion into the rock matrix is a very important mechanism for radionuclide retardation. It is therefore important to ensure that this connected pore system exists under natural stress conditions and can be utilized for diffusion.

In a migration experiment performed in the Stripa Mine at the 360 m level, sorbing as well as nonsorbing tracers were injected into a natural fracture (Abelin et al, 1985). The subsequent excavation of the fracture plane and analysis of the rock matrix close to the fracture plane indicated that some of the sorbing tracers had migrated a short distance into the rock matrix.

Furthermore, a series of laboratory experiments have been performed with the purpose to determine diffusion coefficients for various tracers in granite and other crystalline rocks (Skagius, 1986; Bradbury et al, 1982). These laboratory experiments show that it is possible for sorbing as well as nonsorbing tracers to migrate in the rock matrix by diffusion, but these experiments were not carried out in "undisturbed" rock. It can not be ruled out that the reduction in the rock stresses which occur when samples are taken out have induced the microfissures. It is thus necessary to make in-situ experiments in rock in the natural stress environment before a first stress release, since a recompression will not necessarily close irreversibly induced microfissures.

The in-situ diffusion experiments were performed in the Stripa mine at the 360 m level. At this level, it will give nearly the same stress conditions as in the planned nuclear waste repository.

2. INFLUENCE OF THE STRESS FIELD AND EXPERIMENTAL DESIGN

2.1 Experimental considerations

Performing an in-situ experiment where the tracers are to be subjected to natural conditions requires some experimental considerations. In the Swedish repository concept it is presumed that the nuclear waste is to be stored in canisters at 500 m depth in the bedrock. Because of these conditions, the experiments need to be performed at a large depth under natural conditions. To obtain such a working environment, the experiments were performed at the 360 m level in the Stripa mine.

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Even at large depths the rock stresses might be disturbed by excavations and boreholes and the experiments performed in this disturbed rock might not be representative for the adjacent undisturbed rock. The disturbance in the stress field is, however, limited to a close vicinity of the excavation and borehole and the undisturbed rock can be reached by using a proper drilling arrangement.

The main aim of this experiment was to investigate if diffusion into the porous rock matrix takes place under natural conditions. The most satisfactory way of doing this kind of experiment is to perform a migration experiment with only diffusion. This was however considered as almost impossible (see Chapter 2.3), so the performed experiments included advection as well as diffusion. However, if these experiments can show that it is possible for tracers to migrate within the connected pore system by advection and diffusion, then the pore system would also be available for only diffusion.

2.2 Influence of the stress field

Close to a drift or a borehole, the rock stresses will be changed compared to "undisturbed" rock. This change is dependent on the values and directions of the rock stresses, but as a general rule one can say that the rock stresses are changed approximately 2 hole diameters out from and below the hole, see Figure 2.1. At distances larger than the 2 hole diameters essentially "undisturbed" rock exists (Stephansson, 1981).



Figure 2.1. One example of the deviation from natural stress vs distance from a hole.

Since the objective with these experiments is to do migration experiments in "undisturbed" rock, the experiments had to take place more than 2 drift diameters away from the drift at the 360 m level. This ensured that the experiments were made in rock where the stresses were only marginally influenced by the drift.

The diameter of the drift where the experiments took place was approximately 5 m. Holes with a diameter of 146 mm were drilled downwards from the drift. The depths of the holes were between 11 and 18 m. At these distances from the drift, the changes in rock stresses due to the drift can be neglected and essentially "undisturbed" rock is reached. In one of the holes a rock stress measurement was performed at the depth of 15.5 - 17.5 m which confirmed that "undisturbed" rock was reached (see Appendix 1). Since these experiments took place in holes separated by just a few meters, it was assumed that "undisturbed" rock was reached also in the other experiments.

However, even if the changes due to the drift can be neglected, the existence of the 146 mm hole will cause a change in the rock stresses approximately 0.3 m (2 hole diameters) outward and below the bottom of the hole. To reduce the change in the rock stresses, a 20 mm hole (approximately 3 m long) was drilled in the bottom of the 146 mm hole. The 20 mm hole caused a change in the rock stresses approximately 40 mm outward. Outside this disturbed zone and about 0.3 m below the 146 mm hole essentially "undisturbed" rock was reached.

With the 146 mm packer positioned just above the little hole, see Figure 2.2, this hole will serve as injection hole in the experiments. The experimental layout was identical for the three experiments.

If tracers can migrate from the little injection hole, past the disturbed zone and into "undisturbed" rock, then these experiments will indicate the existence of a connected pore system in "undisturbed" rock.



Figure 2.2 Drilling dimensions and packer positions.

2.3 Experimental alternatives : Diffusion / Diffusion + Advection

2.3.1 Pressure gradients

The most satisfactory way of doing this kind of experiment is to do a diffusion experiment without any overpressure in the injection hole. But considering the pressure measurements done by Lawrence Berkely Laboratories (Wilson, 1981) at the same level (360 m level) and only about 100 m away from the drift where these experiments have taken place, it was found that the pressure gradients for the water (tracer solution) in the injection hole and the pore water in the surrounding rock were different, see Appendix 2.

The pressure gradient in the water (tracer solution) in the injection hole is 1 m/m if the hole is drilled straight downward and < 1 m/m if the hole is drilled in any other direction. But according to the above mentioned pressure measurements, the pressure gradient in the rock should be between 3 and 4.5 m/m at reasonable distances (10-20 m) from the drift independent of direction from the drift. The differences in pressure gradients will give pressure differences between the injection hole and the rock, and since a pressure difference is the driving force for advection in a permeable medium, advection will occur simultaneously with diffusion unless the experiment is performed at an "infinite" distance from the drift. Figure 2.3 illustrates the pressure gradients for the injection hole and the surrounding rock.



Figure 2.3. Pressure gradients for injection hole and surrounding rock.

If the pressure gradients looks like what is illustrated in Figure 2.3, it means that simultaneously with diffusion, advection will occur out from the injection hole in the top and into the injection hole in the bottom. Since there is no pressure difference in the central part of the injection hole, no advection will occur there.

The discussion above indicates that the diffusion profile from a "pure" diffusion experiment might be more or less displaced because of advection. Since diffusion and advection may be of the same order of magnitude, it may not be possible to separate the concentration profile due to diffusion from that due to advection.

2.3.2 Diffusion : Expected migration distances

The diffusion coefficients for Uranine, I^- , and Cr-EDTA have been determined in laboratory experiments (Skagius, 1986). The diffusivities, D_p , were found to be between $0.1*10^{-13} - 5*10^{-13} \text{ m}^2/\text{s}$ in those experiments. The diffusivities are expected to

be approximately a factor 2 lower in an in-situ experiment due to the existence of rock stresses and somewhat lower temperature. In the following discussion the diffusivity, D_p , is assumed to be $1*10^{-10}$ m²/s.

The concentration for radial diffusion from a cylindrical source is only a function of radius r and time t. For a nonsorbing component the equation becomes:

Diffusion equation :
$$\frac{\partial c}{\partial t} = D_p \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial c}{\partial r}\right)$$
 (1)

Solving this equation with the appropriate initial and boundary conditions gives concentration profiles as a function of r and t, see Figure 2.4.



Figure 2.4. DIFFUSION. C/C vs r for various migration times.

2.3.3 Advection : Expected migration distances

A pressure gradient will induce advection in a permeable medium. What significance this pressure gradient will have on the flowrate into the rock matrix is mainly determined by the hydraulic conductivity (K_p) of the rock matrix. At the time when this experiment started there had not been any work done in determining the hydraulic conductivity in the rock matrix for Stripa granite. But according to measurements in other granitic rocks (Brace, 1968: Heard, 1979; Freeze, 1979), the hydraulic conductivity in granitic rock is expected to be between $10^{-13} - 10^{-12}$ m/s.

The equation that predicts the radial flowrate (v_r) and the radial flow distance (r_f) for a nonsorbing component is :

Radial flow equation :
$$v_r = \frac{\text{const.}}{r_f}$$
 (2)

This equation can be solved to obtain the radius of a moving front at time t. Assuming that Darcy's law is valid, we obtain for stationary flow:

$$r_{f} = \frac{2 * t * K_{p} * (P_{1} - P_{2})}{\epsilon_{p} * \ln(r_{2}/r_{1})} + r_{1}^{2}$$
(3)

The parameters and their expected values are:

$$K_{p} - hydraulic conductivity for the rock matrix , 10^{-12} - 10^{-13} m/s$$

$$P_{1}-P_{2} - pressure difference between injection hole and surrounding rock$$

$$\epsilon_{p} - porosity in the rock matrix , assumed to be 0.345 % (Műller-Vonmoos, 1981)$$

$$r_{1} - radius of injection hole (0.01 m)$$

$$r_{2} - distance for pressure difference (assumed to be 4 m => ln r_{2}/r_{1} = 6)$$

The radial flow distance can be calculated by Equation (3) with the expected values of the parameters. Figure 2.5 illustrates the flow distance for the largest pressure difference that would occur between a 2 m long injection hole and the surrounding rock if the experiment was carried out as a diffusion experiment.



Figure 2.5. ADVECTION. Advective distance into the rock matrix vs time for different values on K_p . $P_1 - P_2 = 0.025$ MPa.

In Figure 2.5 it is shown how far into the rock matrix the tracers will migrate as a function of time and K_p . It is difficult to predict the effect of dispersion when the flowrates are as low as those in Figure 2.5, therefore, dispersion is not included.

2.3.4 Experimental considerations

Comparing Figures 2.4 and 2.5, it is obvious that if the experiment is carried out as a diffusion experiment then the radial flow distance due to the pressure difference is of the same order of magnitude as the expected diffusion distance, assuming a hydraulic conductivity $K_p \ge 10^{-13}$ m/s. Another effect that would disturb the concentration profile from a diffusion experiment is the dispersion connected with the also shows how sensitive diffusion radial advection. Furthermore, Figure 2.5 а experiment is for leakage. If there is some leakage in the system, then the injection pressure will be lower than the water pressure in the surrounding rock. That would lead to flow from the surrounding rock into the injection hole.

Because of the difficulties indicated above it was decided to carry out the experiment with an overpressure of approximately 1 MPa in Part I and approximately 0.5 MPa in Parts II and III. The chosen overpressures were large enough to eliminate the problem with the different pressure gradients and small enough to avoid influencing the micro structure of the rock (Stephansson, 1981).

The advective distances due to an overpressure of 1 MPa calculated with Equation (3) are illustrated in Figure 2.6.



Figure 2.6. ADVECTION. Advective distance into the rock matrix vs time, for different values on K_p . $P_1 - P_2 = 1$ MPa.

Based on the calculations illustrated in Figure 2.6 it was decided to use an injection time of 3 months for Part I of the experiment.

2.3.5 Diffusion + advection : Expected migration distances

The equations that predict the migration distance when radial diffusion and advection occur simultaneously are:

Diffusion equation :
$$\frac{\partial c}{\partial t} + v_r \frac{\partial c}{\partial r} = D_p \frac{1}{r} \frac{\partial}{\partial r} (r \frac{\partial c}{\partial r})$$
 (4)
Radial advection equation : $v_r = \frac{const}{r}$ (2)

The initial and boundary conditions imply that there are no tracers in the rock at the start and a constant concentration in the injection hole all times thereafter.



Figure 2.7. ADVECTION AND DIFFUSION. Concentration profiles in the rock matrix vs time for different values on K_p and D_p . $P_1 - P_2 = 0.9$ MPa.

It can be seen in Figure 2.7 that if the values of K_p and D_p are of the same order as expected, then the tracers would migrate beyond the disturbed zone (approximately 40 mm) and a distance into the rock matrix within an injection time of 3 months.

2.4 Experimental design

After drilling the holes (\emptyset 146 mm and \emptyset 20 mm), one small packer was installed in the little hole and one big packer was placed close to the bottom of the large hole, see Figure 2.2. Both packers were mechanically operated.

The small packer was used to get a nylon tube to the bottom of the small hole in order to get a good circulation of the tracers before starting the tracer injection. The large packer was used to close off the injection compartment from the rest of the hole. In this way the lower approximately 100 mm of the large hole and all of the small hole were used for the tracer injection.

After the installations of the packers, the water flowrate into the the injection compartment as well as the water pressure were monitored. However, no reliable values on the natural water pressure were found due to the very low water inflow rates.

According to other measurements in the Stripa mine at the same level and only about 100 m from the drift were these experiments have been performed the water pressures at the distances from the drift were the experiments took place is expected to be between 1.0 - 1.4 MPa (see Appendix 2).

A constant overpressure was used for the injection of the tracer solution. This overpressure ensured that the tracers would migrate by advection and diffusion out from the injection hole and into the pore system of the rock matrix. The overpressure was supplied by using compressed nitrogen.

2.5 <u>Part I</u>

Part I of the in-situ experiment was a preparatory experiment with a tracer injection time of about 3 months where the main purpose was to answer the following questions:

- Can holes be drilled in the way shown in Figure 2.2 ?
- Does the injection system work well ?
- Does the suggested sampling arrangement for tracers work ?
- Can the experiment give any indication about if there exists a connected pore system or not in the rock matrix, and if there seems to exist a connected pore system, can any rough values on the hydraulic conductivity and the diffusivity be obtained ?

2.6 Part II and Part III

Part II and Part III of the field experiment were started simultaneously. The aims were to obtain more evidence over longer times on the existence of matrix diffusion.

The method of drilling a 20 mm hole in the bottom of the 146 mm hole, injecting tracers in the small hole and later overcore the hole worked well. The packer system and injection system also worked well. The sampling arrangement for tracers, i.e.

overcoring, cutting, drilling sampling cores, leaching these sampling cores, and analysing the tracer content, also worked well.

Based on the results from Part I it was decided to use almost the same drilling arrangement, injection system, sampling arrangement, and tracers.

Parts I and II of this field experiment have been reported earlier (Birgersson and Neretnieks, 1982; 1983).

3. OVERCORING AND SAMPLING

The injection of tracers were terminated after 3 months (Part I), 6 months (Part II) and 3.5 years (Part III). The packers were retrieved and the little hole was overcored. The core from the overcoring had a diameter of 132 mm and length of approximately 3.5 m, see Figure 3.1. The core was cut into approximately 50 mm long cylinders.



Figure 3.1. Sampling, step 1.

From these cylinders, a number of sampling cores (\emptyset 10 mm) were drilled at different distances from the injection hole, see Figure 3.2. The number of sampling cores obtained were about 200 in Part I, about 650 in Part II, and about 1800 in Part III. The sampling cores were leached in distilled water.



The tracer concentration in the distilled water was determined and recalculated for the concentration in the pore water. The recalculated concentrations in Parts II and III were based on the porosity that was obtained for every individual sampling core from the weight difference between a wet and dry core. In Part I, all concentrations were based on an assumed uniform porosity of 0.345 % (Müller-Vonmoos, 1981).

In Parts II and III of the experiment, additional holes were drilled adjacent to the injection hole. This was done in order to study the concentration profile further out than the approximately 110 mm that was obtained from the overcoring of the injection hole. For more information about the drilling arrangements in Parts II and III, see Chapter 5.

4. TRACERS AND ANALYTICAL METHODS

4.1 Tracers

The objective of this tracer experiment was to investigate the existence of a connected pore system in "undisturbed" rock. This was accomplish by injecting mixtures of nonsorbing tracers. Since nonsorbing tracers do not sorb on the surfaces in the micropores, the migration rate into the matrix is "high", which means penetration into "undisturbed" rock occurs in a "short" time.

The method of finding suitable nonsorbing tracers has been:

- Test on stability
- Test on sorption on the materials used in the equipment
- Test on sorption on crushed granite.

These tests showed that Cr-EDTA, Uranine, and I⁻ were stable and did not sorb on either the construction materials or crushed granite. Since a mixture of these tracers did not show any chemical reaction, it was decided to use them in the experiments (Birgersson and Neretnieks, 1982).

4.2 Analytical methods

The tracers were analysed using three different methods. This analyzing procedure will decrease the risk in obtaining a systematic error due to the analysis equipment.

Table 4.1. Tracers used

Tracer	Molecular weight	Analytical method	Injection concentration
Cr-EDTA	344	Atomic absorption	5 000 - 10 000 ppm
Uranine (Na–fluorescein)	376	UV – VIS spectrophotometer	20 000 - 80 000 ppm
I —	127	Ion selective electrode	100 000 — 150 000 ppm

After the leaching in distilled water, the Cr-EDTA concentration could be analysed directly in the leached water. Since the absorbance for Uranine is very pH-dependent in the region pH 4-8, the pH was increased to pH 8.5 - 9.5 by addition of a solid buffer (a mixture of H_3BO_3 , KCl, and NaOH) before Uranine was analysed. Before the I⁻ concentration could be analysed, the ionic strength had to be increased by addition of a small amount 5 M NaNO₃

The analysis sequence was as follows:

Solid buffer 5M NaNO₃ Cr-EDTA ______> Uranine _____> I⁻

The addition of the solid buffer did not influence the I^- measurements.

As can be seen in Table 4.1 above, the injection concentrations of the tracers were high. This was because the tracer concentrations were diluted 500 - 1000 times from leaching the sampling cores. The concentrations were chosen in such a way that the dynamic range of the tracer concentrations in the distilled water should be approximately 4 orders of magnitude so it would be possible to detect the tracers down to a relative concentration C/C₀ of 0.01. The accuracy was about ± 10 % for all tracers at the lowest concentration.

5. CORE DESCRIPTIONS

5.1 <u>Part I</u>



Figure 5.1. Core description, Part I.

The injection of tracers continued for approximately 3 months in Part I of the field experiment. Because of this "short" injection time only the injection hole was overcored, i.e. no additional holes were drilled. This drilling arrangement made it possible to study the concentration profile approximately 110 mm outward from the injection hole, i.e. considerably further out than the 40 mm (2 hole diameters) that have a changed stress field compared to "undisturbed" rock.

The core from the overcoring of the injection hole was intersected by a number of fissures. The water inflow rate into the injection compartment was approximately 7 ml/h which means that at least one of the fissures must have been water bearing. Therefore, a number of samples were taken close to the fissures in order to see if there was any indication of tracers having migrated first into the fissure by water flow and then through the fissure coating material and into the rock matrix by diffusion.

Core. injection hole, fissures and sampling places

Comments on the sampling pieces:

3, 6-10, 15, and 16 - Investigation of the concentration profile in the rock matrix.
4, 5, 11, and 12 - Samples taken far from the injection hole and close to a fissure. Could indicate diffusion through the fissure coating material.
13 and 14 - Samples taken behind a fissure. If tracers are found here they must have passed through the fissure coating material.

Since a lot of fissures intersected the core and that the length of the injection hole was just 2 m, only a few samples were obtained where the migration into the "undisturbed" rock could be studied.

5.2 Part II

The injection of tracers continued for about 6 months in this experiment. Because of this "long" injection time and the results from Part I regarding obtained values on D_p and K_p it was decided to drill another @ 146 mm hole, see Figure 5.2.



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Figure 5.3. Core description, Part II.

The length of the injection hole was 3 m in Part II. This made it possible to study the differences in penetration depth into the rock matrix in many sampling pieces located at different depths.

Samples were taken at 22 different levels from core 1. This made it possible to study the variation in migration distance into the rock matrix versus depth in core. Because of core 2, the concentration profile could in some cases be followed approximately 250 mm outward from the injection hole at approximately the same depth. Chapter 7 contains information on the concentration profiles.

5.3 Part III

The injection of tracers continued for about 3.5 years in Part III. This long injection time and the results from Parts I and II led to 5 additional holes being drilled, see Figure 5.4.



Figure 5.4. Drilling arrangement, Part III.

This drilling arrangement made it possible to study the concentration profile approximately 400 mm outward from the injection hole in one direction. In order to study the concentration profiles in other directions, three smaller (\emptyset 76 mm) holes were drilled approximately 250 mm from the injection hole. Only minor parts of the cores were crushed during the drilling and samples could be taken from the major parts of the cores. Examples of concentration profiles are found in Chapter 8.

6. RESULTS, PART I



Figure 6.1. Drilling arrangement, Part I.

6.1 Concentration profiles

Figure 6.2.

The concentration profiles in the pieces where migration had taken place in the rock matrix, i.e. "far" from any fissures, all showed the same results. All the tracers had passed the disturbed zone (approximately 40 mm) and had migrated a distance into "undisturbed" rock.

As an example, the concentration profile for the sample taken approximately 1.2 m below the bottom of the 146 mm hole and a theoretical curve is shown in Figure 6.2. Note that all experimental points in Part I are calculated with a uniform porosity of 0.345 % in the rock matrix (see Chapter 2.3.3).



from injection hole.

The tracer concentrations for the individual sampling cores are presented in Appendix 3.

6.1.1 Influence of fissures

The granite is intersected by a number of fissures where water flows. Figure 6.2 indicates that tracers can migrate by advection and diffusion within the pore system in the rock matrix. If this pore system should be available for tracers (and radionuclides), then the sometimes present thin layer of fissure coating material between the fissure and the rock matrix must be possible to pass through.

The water inflow rate into the injection hole was approximately 7 ml/h in Part I. Therefore, at least one of the fissures intersecting the injection hole must have been water bearing. The investigation of points No. 4, 5, 11, and 12 in Figure 5.1 could have indicated migration through the fissure coating material if the concentrations of tracers had been increased close to the fissure compared with sampling points a little way out. Unfortunately there was not enough data to show this.

From the two pieces taken behind a fissure the samples from piece No. 13 showed no or very low concentrations (C/C₀ < 2 % for all tracers). Samples from piece No. 14, however, showed that tracers had migrated into a piece surrounded by fractures, see Figure 6.3. The distance from the injection hole to the fissure coating material was approximately 70 mm, i.e. the fissure was located in "undisturbed" rock. There were three ways for tracers to reach piece No. 14, see Figure 6.4.



- A and B Migration through the rock matrix (and/or in the fissure) and through the fissure coating material.
- Migration outside the fissure. But this alternative can be excluded since no (or very little) tracers were found in piece No. 15. That is probably because the bottom of the injection hole was filled with granite particles that remained from the drilling.

The discussion above shows that the existence of tracers in piece No. 14 indicates migration through fissure coating material located in a natural stress environment.

It can be seen from Figure 6.3 that the relative concentration (C/C_0) behind the fissure is low compared to the relative concentration at the same distance for migration in the rock matrix as shown in Figure 6.2. This could, however, be explained by a number of factors, for example:

- The tracers migrated through the rock matrix and to the fissure where dilution occurred due to the natural water content within the fissure.
- The tracers reached the fissures and were then transported away by the water flow.
- The fissure is connected to a fissure system that is under lower pressure. Then the whole (or at least the major) pressure drop occurs between the injection hole and the fissure. In this case the tracers would migrate from the injection hole to the fissure by advection and diffusion, and into the rock matrix of piece No. 14 by just diffusion.
- The fissure coating material decreases the migration rate.

Although the tracer concentration was relatively low in piece No. 14, which can be explained by either one or a combination of the factors above, the fact remains that tracers were found in the rock matrix behind fissure coating material in its natural stress environment.

6.2 <u>Conclusions</u>

All three tracers passed the disturbed zone and migrated a distance into the "undisturbed" rock matrix. At least one of the concentration profiles (Cr-EDTA) can be explained by simple advection – diffusion migration without chemical interaction. Also the tracers migrated through fissure coating material located in the "undisturbed" rock.

The concentration profile for Cr-EDTA seemed to differ from those for Uranine and I^- in such a way that Cr-EDTA reached concentrations close to $C/C_0=1$ near the injection hole. Some fraction of the tracer content within the sampling core could have leached out during the cutting of the core into slices and the subsequent drilling of sampling cores. Therefore, the differences between the concentration profiles for Cr-EDTA and for Uranine and I^- can be explained if Cr-EDTA is slightly sorbing. If this is the case, then Cr-EDTA would have an increased concentration close to the injection hole and would not be affected by the leaching in the same way as Uranine and I^- . One explanation to the with distance from the injection hole decreasing

concentrations and the low concentrations of Uranine and I^- even closer to the injection hole might be that just a part of the measured porosity is available for the tracers, i.e. a lot of dead end pores within the rock matrix. If that is the case then only a minor part of the area within the pore system in the rock matrix would be available for sorption of radionuclides. This will be discussed further in Chapters 7 and 8.

6.3 Decisions based on the results

The decisions that were based on the experiences from Part I regarding the equipment are described in Chapter 2.6. Since the core from Part I was intersected with a great number of fissures, the migration into the rock matrix could be followed through the whole sampling piece at only 6 different locations. The concentration profiles in these 6 sampling pieces showed almost the same result, i.e. the difference in depth (≤ 0.5 m) did not seem to affect the shape of the concentration profile. In order to study the concentration profiles over a longer distance, it was decided to increase the length of the injection hole from 2 m in Part I to 3 m in Parts II and III.

Furthermore, all three tracers seemed to have migrated further out into the rock matrix than the approximately 110 mm that could be followed in the core from the overcoring. Due to that it was decided to use a lower overpressure when injecting the tracers in Parts II and III and to drill out some additional cores in order to study the concentration profile further out than the approximately 110 mm that is possible if one only overcores the injection hole.



Figure 7.1. Drilling arrangement, Part II.

7.1 Concentration profiles

The length of the injection hole was 3 m in Part II and just a few parts of the core was intersected by fissures or crushed during the drilling. Therefore it was possible to study the concentration profiles into the rock matrix at several locations separated in distance from the bottom of the large (\emptyset 146 mm) hole.

No observations of migration through the fissure coating material could be done in this experiment for the following reasons: (1) The water inflow rate into the injection hole was below the detection limit (<0.1 ml/h), which implies that the fissures intersecting the injection hole do not carry water in measurable rates; (2) no fissure was located as nicely as the fissure in Part I described in Chapter 6.1.1.

All tracer concentrations in Part II are based on the porosity obtained from the weight difference between wet and dry sampling core. The porosities and tracer concentrations for the individual sampling cores are presented in Appendix 4.

7.1.1 Concentration profiles in core 1

Compared to Part I, the results in Part II showed a considerable variation in migration distance with depth in the core. The penetration depth could in some cases vary by a factor 3 or more in sampling pieces that were separated by just a few tens of centimeters in depth.

The prevailing trend is that all three tracers have migrated a long distance into the rock matrix at the top and the bottom of the injection hole, while the migration distance is rather short in the middle section of the hole.

The variation in migration distance with depth in the core located closest to the injection hole (core 1) is illustrated in the Figures 7.2-7.7.



There is almost no decline in tracer concentration with distance in this sampling piece for at least the first 100 mm that could be studied from core 1. Sampling piece 1 at depth 0.36 m has the same tendency.

Figure 7.2.

Part II. Tracer concentration vs distance from injection hole for sampling piece 2, depth 0.48 m.



The concentration profiles for sampling pieces 3 to 9 were quite similar. It can be seen that the concentration decreases rapidly between 40 and 70 mm outward from the injection hole and that the penetration depth (i.e. concentrations above the detection limit) is at least 80 mm.

Figure 7.3.

Part II. Tracer concentration vs distance from injection hole for sampling piece 6, depth 1.27 m.


Sampling pieces 10 to 13 (depth 1.46 - 1.59 m) showed the shortest penetration depths. The concentration in these sampling pieces was low even close to the injection hole and the penetration depth was just about 50 mm.

Figure 7.4. Part II. Tracer concentration vs distance from injection hole for sampling piece 12, depth 1.55 m.



In sampling pieces 14-19(depth 1.74 - 2.08 m) somewhat higher concentrations were found. Uranine and I⁻ migrated at least 110 mm, while the Cr-EDTA concentration became very low approximately 90 mm from the injection hole.

Figure 7.5.

Part II. Tracer concentration vs distance from injection hole for sampling piece 19, depth 2.08 m.



In sampling piece 20 the concentration had increased a little further. For Uranine and I⁻ the concentration tends to decrease at approximately 90 mm from the injection hole, while the decrease occurs approximately 20 mm earlier for Cr-EDTA.

Figure 7.6.

Part II. Tracer concentration vs distance from injection hole for sampling piece 20, depth 2.24 m.



For sampling pieces 21 and 22 (depth 2.62 - 2.67 m) none of the three tracers showed any decrease in concentration for at least the 110 mm that could be followed from core 1.

Figure 7.7.

Part II. Tracer concentration vs distance from injection hole for sampling piece 21, depth 2.62 m. From looking at the figures above, it is obvious that the migration distance into the rock matrix varies considerably between samples taken at different depths in the core.

The same concentration differences between the tracers are seen in Part II as in Part I. In the cases of a high tracer concentration it seems that Cr-EDTA has an increased concentration compared to Uranine and I^- , while these tracers have migrated further out into the rock matrix when the concentration is low.

7.1.2 Concentration profiles in core 2

The distance between the injection hole and the sampling cores from core 2 was between 150 and 250 mm.

Tracers were found in 8 of the 24 sampling pieces from core 2. These 8 sampling pieces were 1E-3E (depth 0.31 - 0.42 m) and 19E-23E (depth 2.41 - 2.64 m), see Figure 5.3. The fact that tracers were found just in the top and the bottom of core 2 agrees with the results from core 1 presented in the previous chapter.

Since some of the sampling pieces from cores 1 and 2 were located at approximately the same depth, it was in some cases possible to study the concentration profile at the same depth all the way from the injection hole and approximately 250 mm outward.

The Figures 7.8-7.11 show some examples from different depths in the cores where the concentrations could be followed in the two cores.



Figure 7.8. Part II. Tracer concentration vs distance from injection hole for sampling pieces 1 and 2E. Difference in depth is 15 mm.

Figure 7.8 indicates that the I^- concentration does not decrease with distance from the injection hole for at least 250 mm. However, the Cr-EDTA concentration shows a significant decrease 200-250 mm from the injection hole.

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Figure 7.9 illustrates the depth in core 2 where the highest Cr-EDTA concentrations were found. There is no significant decrease in concentration for Cr-EDTA (or the other traces) for at least 250 mm.



Figure 7.10 shows that neither Cr-EDTA nor Uranine were found in sampling piece 22E, but that I had penetrated this sampling piece. It can also be seen that there is a drastic decrease in concentration between core 1 and core 2, i.e. between 110-170mm outward from the injection hole.



Difference in depth is 20 mm.

The results from sampling pieces 22E and 23E (Figures 7.10 and 7.11) both show that only I^- had penetrated core 2 at these depths and that the I^- concentration decreased rapidly between core 1 and core 2.

The concentration profiles for sampling pieces 19E-21E (depth 2.41 - 2.51 m) could not be followed all the way from the injection hole since core 1 was crushed at the corresponding depth. However, sampling pieces 19E-21E showed high concentrations of all three tracers.

7.1.3 Penetration depth for a fixed concentration

The difference in migration distance with depth can be illustrated very clearly by the penetration depth for a fixed concentration plotted versus the depth in core.



Figure 7.12. Part II. Core 1. Penetration depth for different concentrations for Cr-EDTA, Uranine and I^- vs depth in core.

It can be seen in Figure 7.12 that only 3 of the 22 sampling pieces from core 1 had Uranine and I⁻ concentrations C/C_0 of 40 % or higher, while this concentration for Cr-EDTA was found in 14 sampling pieces. The diagrams for $C/C_0 = 10$ % indicate that the penetration distance for this concentration is approximately the same for all three tracers. The diagrams clearly shows for the concentration $C/C_0 = 1$ % that I⁻ has the longest and Cr-EDTA the shortest penetration distances.



Figure 7.13. Part II. Cores 1 and 2. Penetration distance for $C/C_0 = 1 \%$ for Cr-EDTA, Uranine, and I⁻ vs depth in the cores.

Figure 7.13 shows that the concentration profiles for all three tracers could be followed at the same depth in core 1 and core 2 at the top of the cores. This was also possible at the bottom of the cores for I^- .

7.2 Causes of the differences in penetration depth

The fact that the migration distance is different at different depths can be caused by

- Differences in porosity (ϵ_p)
- Differences in the migration parameters $(K_p \text{ and } D_p)$.

The possibility of the tracers migrating within a fracture intersecting the injection hole has been excluded in this part of the field experiment since the water inflow rate and injection flowrate are so small that the existence of water bearing fractures intersecting the injection hole can be excluded.

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The porosity was measured for every individual sampling core (about 650 sampling cores) by comparing the weight difference between a wet and dry core. Figure 7.14 illustrates the mean value of the porosity (\pm the standard deviation) for each sampling piece from core 1 and core 2.



Figure 7.14.

Part II. Core 1 and core 2. The porosity (± the standard deviation) vs depth.

From the observations in the figure the difference in migration distance with depth can not be explained by the porosity, since the porosity is almost the same for all sampling pieces.

7.2.2 Hydraulic conductivity and diffusivity

The reason for the considerable difference in migration distance for sampling pieces separated by just a few tens of centimeters seems to be caused by the variation in the migration parameters (K_p and D_p) with location due to inhomogeneities.

The values of the migration parameters have been evaluated by comparing the experimentally obtained concentration profiles with theoretical concentration profiles obtained by using Equations (2) and (4) and the TRUMP (Edwards, 1972) computer code. These approximative values of D_p and K_p are summarized in Table 7.1.

Sampling piece	Depth (m)	$D_p (m^2/s)$	K _p (m/s)
1 - 2	0.36-0.48	> 1*10-10	≥ 2-5*10-13
3 - 9	0.78-1.41	≈ 0.5*10-10	≈ 0.1*10-13
10-13	1.46-1.59	≈ 0.05*10-10	≼ 0.1*10 ⁻¹³
14-20	1.74-2.24	≈ 1*10-10	≈ 1×10-13
21-22	2.62-2.67	≥ 1*10-10	> 2-5*10-13

Table 7.1. Approximate values on D_p and K_p for different depths.

Table 7.1 shows that D_p and K_p can vary with an order of magnitude for sampling pieces separated by just a few tens of centimeters. There was no obvious decline in concentration for the approximately 250 mm that could be studied in some pieces in the top and bottom of the core. In these cases no value of D_p or K_p (except for a lower limit) could be obtained.

7.3 Conclusions

All three tracers migrated through the zone disturbed by the presence of the injection hole and a distance into the "undisturbed" rock.

The same difference between Cr-EDTA and the tracers Uranine and I^- that was found in Part I was also found in Part II. Both Uranine and I^- migrated a longer

distance into the rock matrix, even though the two had lower concentrations compared to Cr-EDTA close to the injection hole.

In some cases there was no obvious decrease at all in the tracer concentrations for at least the first 250 mm that could be studied from core 1 and 2. Therefore, the possibility about dead end pores can be excluded (Chapter 6.2). If part of the migration had taken place in dead end pores then the tracer concentrations would have to decrease with distance from the injection hole. The reason for this is that dead end pores have just a limited extent.

In Part I, the length of the injection hole was 2 m and large parts of the core from the overcoring were crushed. The length of the injection hole was 3 m in Part II and since only minor parts of the core were crushed during the overcoring it was possible to study the concentration profiles at different depths. It was found that the values of the hydraulic conductivity (K_p) and diffusivity (D_p) could vary with an order of magnitude for sampling pieces separated just a few tens of centimeters. The differences in migration distances could not be explained by the porosity since the porosity was almost the same for all sampling pieces.

7.4 Decisions based on the results

In Part II, the tracers were injected for about 6 months and had at some locations migrated further out than the 250 mm that could be studied from the two cores from the overcoring. In Part III, the tracers were injected for about 3.5 years and it was decided to drill out another core in order to study the concentration profile further out into the rock matrix. It was also decided to include some laboratory work in order to try to explain the differences in K_p and D_p .

8. RESULTS, PART III

It can be seen in Figure 8.1 that three large holes (O 146 mm) made it possible to study the concentration profile as far as about 400 mm outward from the injection hole. The three additional small holes (O 76 mm) made it possible to study the concentrations in other directions.



Figure 8.1 Part III. Drilling arrangement and notation of the cores.

8.1 Concentration profiles

The length of the injection hole as well as the cores from the overcoring were approximately 3 m. The cores had only minor parts that were crushed during the overcoring and between 28 and 45 sampling pieces were taken from each core. The concentration profiles could in some cases be followed about 400 mm outward from the injection hole and in different directions at the same level.

As in Part II, no water entered into the injection hole, which implies that migration within the intersecting fissures can be neglected.

All tracer concentrations in Part III are based on the porosity obtained from the weight difference between a wet and dry sampling core. The porosities and tracer concentrations for the individual cores are presented in Appendix 5.

8.1.1 Concentration profiles

The results from Part III of the experiment show that the tracer concentrations seem to vary considerably with depth along the core as well as with direction from the injection hole. The penetration depth could in some cases vary by a factor 2 or more in sampling pieces that were separated by just a few tens of centimeters in depth or located at the same depth but in different directions from the injection hole

The prevailing trend is that the tracers migrated a long distance into the rock matrix from the upper part of the injection hole.

Some examples of concentration profiles for depths where the profile could be followed in many of the cores are given in Figures 8.2-8.16.



Sections: ▲3 0.725 ■3E 0.725 ●7X 0.715 o10T 0.745 ★11A 0.725

Figure 8.2 Part III. Uranine concentration vs distance at ≈ 0.725 m depth.

Figure 8.2 illustrates the concentration profile for Uranine in the sampling pieces located around 0.725 m below the 146 mm hole. The tracer concentration within the

large cores is almost independent of distance from the injection hole. However, the samples from one of the cores taken in another direction, but still at the same depth in the injection hole, show concentrations that are approximately 2 orders of magnitude lower. This indicates that the transport properties can vary considerably in different directions. The concentration profiles for I^- and Cr-EDTA showed similar results.



Sections: ▲4 0.775 ■4E 0.775 ●8X 0.765 o11T 0.795 ★12A 0.775

Figure 8.3 Part III. I concentration vs distance at ≈ 0.775 m depth.

The concentration profiles at the 0.775 m depth, illustrated with I^- in Figure 8.3, show that the concentration is almost independent of distance from the injection hole. The decrease in concentration in one of the small cores is also seen at this location, but not to the same extent as illustrated in Figure 8.2.



Figure 8.4 Part III. I⁻ concentration vs distance at ≈ 0.825 m depth.

Even at the 0.825 m depth, see Figure 8.4 for the I^- concentration, the concentration is almost independent of distance from the injection hole. In this example, the concentrations in the small cores are of the same order of magnitude as the concentration in the large core at the same distance from the injection hole.



Sections: ▲6 0.975 ■7E 0.965 ●10X 0.965 O15T 0.995 *6R 0.965

Figure 8.5 Part III. I⁻ concentration vs distance at ≈ 0.975 m depth.

Figure 8.5 illustrates that the I^- concentration decreases somewhat with distance from the injection hole. There does not seem to be any difference in concentration between samples taken in different directions from the injection hole.



Figure 8.6 Part III. Uranine concentration vs distance at ≈ 1.275 m depth.

The concentration for Uranine decreases rapidly far out from the injection hole at the 1.275 m level as shown in Figure 8.6, but the tracers still penetrated the rock matrix at least the 370 mm that could be studied. There does not seem to be any major differences in penetration depth in the different directions from the injection hole.



In Figure 8.7 the concentration for I^- decreases with distance from the injection hole at the 1.325 m level, but there does not seem to be any major differences in penetration depth in different directions from the injection hole.

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Sections: ▲16 1.775 ■14E 1.775 ●20X 1.765 ★23A 1.795

Figure 8.8 Part III. I concentration vs distance at ≈ 1.775 m depth.

In Figure 8.8 the I^- concentration decreases continuously with distance from the injection hole at the 1.775 m level. No real difference in the concentration is observed in the different directions from the injection hole. Figure 8.9 shows the Uranine concentration for the same locations.



Figures 8.8 and 8.9 show the difference between the tracers I^- and Uranine. For the tracer I^- , it migrated at least 370 mm into the rock matrix, while Uranine could only be found about 200 mm outward from the injection hole, see Figure 8.9. Cr-EDTA could only be found about 110 mm out from the injection hole.



Sections: A17 1.825 ■15E 1.825 ●21X 1.815 027T 1.840

Figure 8.10 Part III. Uranine concentration vs distance at ≈ 1.825 m depth.

The concentration profile at the 1.825 m level in Figure 8.10 is very similar to the concentration profile illustrated in Figure 8.9. However, these figures shows the same tracer for injection points separated with only about 50 mm.



Figure 8.11 Part III. Uranine concentration vs distance at ≈ 2.025 m depth.

In Figure 8.11, Uranine migrated a slightly shorter distance into the rock matrix at the 2.025 m level than at the above presented levels. I^- and Cr-EDTA also migrated a shorter distance at this level compared to the above levels.



Sections: A21 2.225 ■19E 2.225 ●25X 2.215 O33T 2.210 *27R 2.200

Figure 8.12. Part III. Uranine concentration vs distance at ≈ 2.225 m depth.

At the 2.225 m level shown in Figure 8.12, Uranine can be followed approximately 200 mm outward into the rock matrix in the large cores, while the small cores show high Uranine concentrations about 250 mm outward from the injection hole. This is another indication that the variation in penetration depth can be quite different in different directions.



Figure 8.13. Part III. Uranine concentration vs distance at ≈ 2.375 m

depth.

The concentration profiles could only be followed in two of the large cores and one of the small cores at the 2.375 m level, see Figure 8.13.



Sections: ▲25 2.575 ■24E 2.555

Figure 8.14. Part III. Cr-EDTA concentration vs distance at ≈ 2.575 m depth.

At the 2.575 m level, the concentration profiles could only be followed in two of the large cores. Figure 8.14 shows the Cr-EDTA concentration. The concentrations for I^- and Uranine are somewhat higher, but still decreased in the core located furthest away from the injection hole.



The tracer concentrations could be followed in two large cores and two small cores at the 2.925 m level as shown in Figure 8.15. The Uranine concentration was slightly increased in one of the small cores, 38A, compared to the samples taken in the other cores at the same distance from the injection hole.



Figure 8.16. Part III. I⁻ concentration vs distance at ≈ 2.975 m depth.

From Figure 8.16 it can be seen that the I^- concentrations at the 2.925 m level was fairly high even as far from the injection holes as 350 mm. Also there does not seem to be any differences in concentration between the different directions.

From looking at the Figures 8.2-8.16 it is obvious that the migration distance varies considerably with the depth in the cores, the direction from the injection hole and the chosen tracer.

8.1.2 Concentration for a fixed distance from the injection hole

Since the concentration profiles can not be followed the whole distance from the injection hole to the sampling cores for the three small cores (\emptyset 76 mm, see Figure 8.1), it is meaningless to illustrate the penetration depth for a fixed concentration. Instead the tracer concentrations for a fixed distance from the injection hole as illustrated in Figures 8.17 to 8.19 show the differences in concentration with depth in the cores and direction from the injection hole. The distance from the injection hole to the sampling cores in the \emptyset 76 mm cores are 200-250 mm. Therefore, the concentrations illustrated below are mean values for sampling cores located 200-250 mm from the injection hole.







Figure 8.18. Average Iodide concentration 200-250 mm from the injection hole.



Figure 8.19. Average Cr-EDTA concentration 200-250 mm from the injection hole.

Figures 8.17 to 8.19 show that there are large differences in the concentration at different depths in the cores. The concentrations are fairly high in the upper meter and then decreases to 0 at approximately 2 m depth. The concentrations around 2.5-3 m depth are quite different in the different directions. Samples taken from the cores denoted E,T, and A have concentrations that are well above 0 but still lower than those found in the upper part of the cores. However, samples taken from the core denoted by R have concentrations that are well above any concentration found at any other level in that core.

It can also be seen that there is a large difference in behaviour between the tracers. I^- has penetrated a larger number of sampling pieces than Uranine which was found in a larger number of sampling pieces than Cr-EDTA. However, the Cr-EDTA concentrations are in many cases well above those for I^- and Uranine.

8.2 Causes of the differences in penetration depth

It was observed also in Part III of this experiment that the migration distances were different at different depths and directions from the injection hole. One explanation for these differences could be differences in the porosity (ϵ_p). But even if the porosity is the same, the pore size distribution could be different. That is, assuming the same porosity, a large number of small pores would give different migration properties compared to a few large pores. Another explanation for the difference in the concentration in pieces located at the same depth but in different directions could be if the pores (microfissures) had specific directions.

The following laboratory investigations were performed in order to determine the reason for the differences in penetration depth:

- Determination of the porosity (ϵ_p)
- Determination of the pore size distribution
- Determination of the directions for the microfissures

8.2.1 Porosity

The porosity was measured for every individual sampling core (about 1800 sampling cores in Part III) by comparing the weight difference between a wet and dry core. This measurement gave the same result as presented for Part II, i.e. no significant differences in porosities were found between the sampling pieces. The porosity was found to be between 0.12-0.51 % with an average close to 0.3 %, see Appendix 5. Therefore, the difference in migration distance with depth and direction from the injection hole can not be explained by the porosity, since the porosity is almost the same for all sampling pieces.

8.2.2 Pore size distribution

The pore size distributions were measured using three different methods. The methods used were a Hg-method, BET-method and a surface investigation via an electron-microscope.

First the method with mercury penetrometry was tried. But due to the low porosity of approximately 0.3 %, the amount of mercury that penetrated the rock matrix was to small to give any reliable results about the pore size distribution.

The second method that was tried was the BET-method using N_2 gas. But as with the Hg-method, the porosity was to low for the method to give any results on the pore size distribution.

The third method tried was to investigate the surface with electron microscope. From these pictures it was possible to count the number of pores and determine the size of the pores. One must however keep in mind that the investigated rock surface was just a few mm², so the obtained pore size distributions must be considered as very local and might therefore not at all represent the rock matrix around the location for the sample. The pore size distribution for 5 samples were determined by this method. Figure 8.20 shows an example of the obtained results.





Results obtained by electron microscope.

It can be seen in Figure 8.20 that the major part of the pores in this specific sample have a opening of less than 0.5 μ m. Almost no pores have a opening above 2 μ m.

Some small variations in pore size distribution was found when comparing the samples. The samples are arranged in increasing frequency of large pores in Table 8.1.

Table	8.1.	Pore	size	distribution
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Samples arranged in increasing frequency of large pores.

No	Sample	Depth (m)	¢p (%)	
1 2 3 4 5	25:9 2E:12 15E:9 5E:1 10E:13	2.575 0.555 1.825 0.825 1.315	0.212 0.468 0.415 0.422 0.362	Increased frequency of large pores

The pore size distributions were determined in sampling cores from the core obtained when overcoring the injection hole and the core denoted E, see Figure 8.1.

As the porosity is almost the same for the samples in Table 8.1, it should be that the sample with the highest frequency of large pores should have the largest hydraulic conductivity and thereby the highest tracer concentration at a distance from the injection hole. Figure 8.21 shows the average Uranine concentration 200-250 mm from the injection hole and the locations of the samples analysed for pore size distribution.



Figure 8.21. Average Uranine concentration 200-250 mm from the injection hole and location of samples analysed for pore size distribution.

It can be seen in Figure 8.21 that the samples denoted 2, 4, and 5 are located in areas with a high concentration at a distance from the injection hole. Sample No. 1 is located in an area with somewhat lower concentration and sample No. 3 in an area where the concentration is below the detection limit. The number of samples taken are few, but Figure 8.21 indicates that there might be a correlation between the pore size and the ability for tracers to penetrate the rock matrix. A sample with an increased frequency of large pores would then have an increased tracer concentration at a distance from the source.

8.2.3 Direction of microfissures

The direction of the microfissures was determined in three samples (Jaktlund, 1986). The method used was the DSA-method (Differential Strain Analysis). A small rock sample with a size of a few centimeters, was subjected to a surrounding stress whereby a portion of the fissures was closed. By subjecting the samples to a number of different stresses, the compression in different directions could be evaluated. The compression will be proportional to the number of fissures that are perpendicular to the compression direction. However, no specific microfissure direction could be found in any of the three samples.

8.2.4 Hydraulic conductivity and diffusivity

The reason for the considerable differences in migration distance for sampling pieces separated by just a few tens of centimeters in depth or at the same depth but in different directions seems to be caused by variations in the migration parameters, K_p and D_p due to inhomogeneities in the rock matrix.

Values on the diffusivity and the hydraulic conductivity were obtained when evaluating the concentration profiles shown in Chapter 8.1.1. Laboratory measurements were performed in order to compare laboratory and in-situ values for the hydraulic conductivity and the diffusivity. It should, however, be noted that the laboratory measurements were performed on fairly small samples so that these values should be considered as more or less local values for the specific sample and therefore maybe not representative for the rock matrix around the sample.

8.2.4.1 In-situ measurements

The values of the migration parameters, K_p and D_p , have been evaluated by comparing the experimentally obtained concentration profiles with theoretical concentration profiles obtained by using Equations (2) and (4) and the TRUMP program (Edwards, 1972).

If it should be possible to evaluate K_p and D_p from the concentration profiles one must be able to follow the concentration not only in the core from the overcoring of the injection hole but also in the cores denoted E and X, see Figure 8.1. There must also be a decrease in the concentration over the studied length, otherwise just a lower limit of K_p would be obtained. This is the case for the samples taken around 0.7 m depth from which just a lower limit of K_p can be obtained, see Figures 8.2 to 8.4. In these cases K_p is greater than or equal to $2*10^{-1.3}$ m/s.

It is not possible to obtain any values on K_p or D_p from the cores denoted T, R, and A since just a part of the concentration profile can be seen in these directions. The approximative values for D_p and K_p from the evaluation of the concentration profiles into the rock matrix are illustrated in Figures 8.22 and 8.23.



Figure 8.22. Part III. D_p vs depth in the cores for the three tracers.

The diffusivity were evaluated at the locations illustrated in Figure 8.22. It was not possible to follow the concentration profile as far out into the rock matrix as needed for the evaluation of D_p and K_p at the other locations. The difference in behaviour between the tracers is also clearly illustrated. Iodide has diffusivity values that are one to two orders of magnitude larger than Cr-EDTA, while the diffusivity for Uranine is somewhere between these two tracers. The diffusivities vary between $2*10^{-12}$ to $5*10^{-10}$ m²/s.



Figure 8.23. Part III. K_p vs depths in the cores for the three tracers.

In contrast to the diffusivity, the evaluation of the hydraulic conductivity is not dependent on the tracer but just on the properties of the rock matrix. Therefore, the hydraulic conductivity should be the same whether evaluated from the concentration profile for I⁻, Uranine, or Cr-EDTA. The conductivities were evaluated individually for the different tracers and it can be seen from Figure 8.23 that the difference between the tracers is not above a factor of 2. The hydraulic conductivity was found to vary between $1*10^{-1.4}$ to $\geq 2*10^{-1.3}$ m/s.

8.2.4.2 Laboratory measurements

The diffusivity in the rock matrix for a tracer can be measured in the laboratory. By using a diffusion cell in which a piece of rock is located between a volume of tracer solution and pure water, the increase in tracer concentration in the volume with "pure" water gives the value of $D_{p}e_{p}$, see Figure 8.24. For more information about through diffusion experiments, see Skagius (1986).

Diffusion cell



Figure 8.24. Equipment for the through diffusion experiment.

The rock piece used in the experiment had a diameter of 42 mm and a thickness of 10 mm. So the $D_p \epsilon_p$ value obtained from the through diffusion experiment would be considered as a very local value for the investigated rock. Plotting the amount of tracers that have diffused through the rock piece as a function of time gives a straight line which has a slope that is proportional to $D_p \epsilon_p$, see Figure 8.25.



Figure 8.25. Evaluation of a through diffusion experiment.

The diffusivity was measured on four different rock samples all from core E, see Figure 8.1. The measurements were performed for approximately 6 months. The diffusivities from the laboratory experiments are listed in Table 8.2.

Diffusivity $* 10^{-12} (m^2/s)$	
Iodide	Uranine
90	8
200	9
200	3
200	10
	Diffusivity Iodide 90 200 200 200

Table 8.2. Diffusivities obtained from laboratory experiments.

It can be seen in Table 8.2 that the diffusivity for I^- is at least one order of magnitude larger than for Uranine. This was also seen in the in-situ experiment. The two samples taken for laboratory experiments at the same level of 2.830 m were separated by just a few millimeters, but the difference in diffusivity for Uranine is a factor of three! However, these values are of the same order of magnitude as those obtained in-situ and are illustrated in Figure 8.26.



Figure 8.26. Comparison between diffusivities obtained in the laboratory and in-situ.

Factors that will increase the diffusivity obtained from laboratory experiments compared to in-situ experiments are the temperature and surrounding stress. In this case the temperature was higher ($\approx 20^{\circ}$) and the surrounding stress was lower (=0) in the laboratory experiment than in the in-situ experiment ($\approx 10^{\circ}$, ≈ 15 MPa). These findings compare well with the results shown in Figure 8.26 where it can be seen that the diffusivities obtained in the laboratory are slightly higher than those obtained in-situ. This result is important since it indicates that the diffusivities found in laboratory experiments also seem to be valid for in-situ conditions under natural stress conditions.

The hydraulic conductivity was determined by laboratory experiments for five different samples (Forsberg, 1987). The equipment used is illustrated in Figure 8.27.





Laboratory equipment used for determination of the hydraulic conductivity.

By monitoring the water flowrate through the rock sample and the water pressure gradient it is possible to evaluate the hydraulic conductivity. With the equipment illustrated in Figure 8.27 it is possible to simulate in-situ conditions by subjecting the rocksample to suitable radial and axial stresses.

The length of the rock sample was approximately 100 mm and the diameter approximately 66 mm why the obtained values on the hydraulic conductivity must be considered to be local values that do not have to be valid for the rock around the sample. It should however be noted that the five samples, all taken from core X, were drilled out in such a way that the water flow in this laboratory measurement was in the same direction as during the in-situ test.

The natural rock stress at the location where these experiments were performed was around 15 MPa, see Appendix 1. Therefore, the hydraulic conductivity was evaluated for all five rock samples using a uniform confining stress of 15 MPa. The hydraulic conductivity was also determined in some of the rock samples using other confining stresses in order to evaluate the effect of the confining stress on the hydraulic conductivity.

The procedure was performed using different pressure gradients. First, a water pressure difference of 51 kPa was applied over the 100 mm long sample. With this fairly low gradient the water injection flowrates decreased to 0 after a short while, so the water pressure was increased to 204 kPa. Evaluating the obtained hydraulic conductivity from using a water pressure difference of 204 kPa gave the same conductivity as when using a pressure difference of 450 kPa. So, it can be stated that an increased water pressure difference will increase the water flowrate through the rock sample which is a great advantage when the conductivities are as low as in this experiment, $K_p \approx 10^{-1.4} - 10^{-1.3}$ m/s. Therefore, a water pressure difference of 450 kPa was used for all samples.

The amount of water that had been transported through the rock sample was monitored several times every week. One example of the hydraulic conductivity for one of the five tested rock samples is given for two different confining stresses in Figure 8.28.

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Figure 8.28. Hydraulic conductivity obtained in the laboratory test as a function of time for two different confining stresses.

It can be seen in Figure 8.28 that the conductivity decreases by a factor of three when increasing the surrounding stress from 15 MPa to 30 MPa. The hydraulic conductivities obtained from the laboratory experiments are given in Table 8.3.

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Depth (m)	Conductivity (m/s)	Confining stress (MPa)
1.48	2*10-14	15
1.89	2*10-13	15
	5*10-14	2 5
2 14	1 * 1 0 - 1 3	15
2.14	3*10-14	30
0.7/	0 + 10 = 14	15
2.74	4*10 - 1 4	20
2.89	2*10-13	15

It can be seen in Table 8.3 that the hydraulic conductivity, K_p , was found to be between $2*10^{-14} - 2*10^{-13}$ m/s for the rock samples with a confining stress of 15 MPa. It can also be seen that an increase in the confining stress reduces the conductivity. If one compares the hydraulic conductivities obtained in-situ with those obtained in this laboratory experiment it is obvious that the values are of the same order of magnitude, see Figure 8.29. It might be that the conductivities found in the laboratory experiment were slightly larger than those obtained in-situ. This could be explained if the actual in-situ stress was above the assumed 15 MPa. The increased conductivity in the laboratory experiment could also be due to that these rock samples were subjected to a decrease in the stresses from the in-situ conditions to 0 stress when the samples were taken out. This decrease in the stresses might induce fractures that were not closed when the samples were recompressed.


Figure 8.29. Hydraulic conductivity vs depth in core. From in-situ conditions and laboratory experiments.

8.3 Conclusions

All three tracers migrated through the zone disturbed by the presence of the injection hole and a distance into "undisturbed" rock.

The same migration difference found between Cr-EDTA and the tracers Uranine and I^- in Parts I and II was also found in Part III. Uranine and I^- both migrated a longer distance into the rock matrix and also had lower concentrations than Cr-EDTA close to the injection hole.

In some cases, no obvious decrease in tracer concentrations for at least some 400 mm could be seen.

The differences in D_p and K_p could be an order of magnitude between samples separated by just a few tens of centimeters. This was also found in Part II. The drilling arrangement in Part III made it possible to study the concentration profile in more than one direction. In some cases there were large differences between the concentrations in different directions. This is an indication that the values of D_p and K_p are dependent on location (depth) as well as direction.

9. DISCUSSION

Π

Drilling (Ø 146, 76 mm)

9.1 Sources of error

An in-situ experiment is of course more difficult to perform than a laboratory experiment so that a number of errors of course will occur. The most important errors are listed below.

I Pressure release Before overcoring the injection hole, the pressure was released and the packers were removed. This release in pressure allows the tracers to migrate from the surrounding rock to the non-pressurized injection hole by advection. The time between pressure release and drilling was between 1 and 4 weeks.

> During the drillings, the cores were flushed with water (drilling fluid) and the tracers could migrate out from the cores by diffusion. It took about 3 hours to drill 3 m. When drilling out a core, the surrounding rock stress decreases which will increase the porosity within the core. This increased porosity means that the core "takes up" the surrounding drill fluid which will decrease the tracer concentration.

III	Sampling	The cores were flushed with water
		during the sampling (cutting into
		pieces and drilling of sampling cores).
		This means diffusion out from the
		core during about 5 minutes
		(cutting) respective
		about 2 minutes (drilling).
IV	Analysis	The errors in the analysis was about

The errors in the analysis was about ± 10 % for concentrations down to C/C $_0 = 0.01$.

V Porosity The porosities were determined for every individual sampling core in Parts II and III. The error in the porosity is estimated to be about ± 10 %.

Points I, II, and III decreased the tracer concentrations in the sampling cores. Therefore, the tracer concentrations in the sampling cores may have been higher than indicated in the preceding diagrams.

When looking at the drilling arrangement for Part III it should be noted that the injection hole was overcored first, whereupon the holes denoted E, X, T, R, and A were drilled. The tracers could then migrate closer to the injection hole due to the pressure gradient induced when the injection pressure was decreased and the packers taken up. The tracers could however never migrate further away from the injection hole. Therefore, the tracers could have penetrated even further out into the rock matrix than illustrated in the foregoing diagrams.

9.2 Recommended work

The major aim with this experiment was to investigate if tracers can diffuse into the rock matrix under natural stress conditions. Since the experiment can be regarded as a demonstration experiment for matrix diffusion it is important that the experimental conditions are as close to natural conditions as possible. The following points must

- Rock stresses
- Water pressure
- Diffusion through fissure coating material
- Sorbing tracers

The experiment has to take place in undisturbed rock. If the water pressure is reduced, then the risk to influence the micro structure of the rock is decreased. If the micropore system within the rock matrix should be available for sorption of radionuclides emerging from a repository, then the nuclides must first diffuse through the sometimes present thin layer of fissure coating material. In a demonstration experiment it might be useful to show that sorbing tracers as well as nonsorbing tracers can diffuse into the rock matrix.

Rock stresses

To avoid the problem with the rock stresses deep drill holes must be used, with fairly small diameter, where the last part of the hole is located in rock that is undisturbed because of the drift. This was done in the presented diffusion experiment.

Water pressure

To avoid using any overpressure when injecting the tracers, one could locate a fracture in the undisturbed part of the hole with natural water flow and close of a small section of it. That would not induce any problems with the pressure gradients. Then one could inject sorbing and nonsorbing (maybe radioactive) tracers for a long time without any overpressure into the fracture. Injection without using any overpressure requires a dilution probe. In the presented experiment a small overpressure was used for the tracer injection and only nonsorbing tracers were used.

Diffusion through fissure coating material

Injecting tracers with a dilution probe implies that the tracers would migrate with the natural water flow into the fracture and diffuse from the fracture, through the fracture coating material, and into the adjacent rock matrix. The fracture coating material as well as the rock matrix would be located in undisturbed rock just a short distance away from the injection zone. In the presented experiment, mainly diffusion in the rock matrix was observed except for one presented case where the tracers must have passed through fissure coating material located in undisturbed rock.

Sorbing tracers

In a demonstration experiment it might be useful to show that sorbing tracers as well as nonsorbing tracers can or cannot diffuse into the rock matrix. In the presented experiment just nonsorbing tracers were used.

Injecting tracers in a fracture with unknown direction and water flow paths will induce huge problems. One way would be to drill out a large number of large cores from the drift and then drill out a large number of sampling cores. To determine the tracer concentration versus distance from the fracture surface, leaching (nonsorbing tracers) and grinding (sorbing tracers) methods could be used. Since channeling occurs in single fractures (Abelin et al., 1985), most of the samples would be obtained from the rock where the adjacent fracture plane have not been in contact with the water. Enough sampling could, however, give information about the extent of channeling. Another problem would be to take samples in the flow direction. The tracers would migrate in the natural flow direction since no overpressure would be used for injection. The natural flow direction is difficult to determine. Therefore, this proposed migration experiment would take long time, cost a lot of money, and cause large analysing problems.

Compared to the presented experiment this proposed experiment would eliminate the need of an overpressure for the tracer injection. It would also be possible to use sorbing tracers since the migration in the fracture is "quick", then the subsequent diffusion through the fissure coating material and the diffusion into the rock matrix would be located in undisturbed rock.

The conclusions from these experiments are as follows :

- Nonsorbing tracers migrated through the disturbed zone and a distance into undisturbed rock.
- The tracers migrated through fissure coating/filling material located in undisturbed rock.
- Diffusivities and hydraulic conductivities found in-situ
 compared well with those found in laboratory experiments.
- Large differences in diffusivity and hydraulic conductivity were found in samples located just a few tens of centimeters apart.
- Laboratory measurements concerning pore size distribution, microfissure direction, and porosity could not explain the differences in migration distance between the samples.

The results indicate that it is possible for tracers (and therefore radionuclides) to migrate a considerable distance into a granitic rock matrix under natural stress conditions.

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С	concentration in liquid	mol/m ³
C _o	injection concentration	mol/m ³
D _p	diffusivity in water in pores	m ²/s
К _р	hydraulic conductivity in the rock matrix	m/s
L	length	m
Р	pressure	Pa
P _{"natural"}	natural pressure in the rock	Ра
$P_1 - P_2$	pressure difference between injection hole and surrounding rock	Pa
r	radial distance	m
rf	radial distance for flow	m
r ₁	radius of injection hole	m
r ₂	radial difference for pressure difference	m
t	time	S
^t c	contact time	S
v _r	radial velocity	m/s

Δ	difference	
¢p	porosity of unfractured rock, matrix porosity	m ³ /m ³
σr	radial tension	Pa
σ_t	tangential tension	Pa
Ø	diameter	m

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Rock stress measurement

A rock stress measurement was performed by the Swedish Power Board in the hole that was used for Parts I and II of the in-situ experiment. The rock stresses were measured in three points located at 15.5, 16.0, and 17.5 m depth from the floor of the drift, see Figure A1.1. The drift is located approximately 347 m below the ground level. Since the hole where Part III of the in-situ experiment was performed is located just about 5 m from the hole where the rock stress measurement took place the obtained rock stresses are assumed to be valid also for this hole.



Figure A1.1. Location of the measuring points for the rock stress measurement

The rock stress can be divided into three perpendicular principal stresses. It was found that the largest principal stress was almost horizontal and the minor almost vertical. The largest principal stress was found to be ≈ 28 MPa and the minor ≈ 5 MPa. The second largest principal stress (horizontal) was ≈ 8 MPa. Figure A1.2 shows the results in the three measuring points.



Figure A1.2. The principal stresses projected onto the horizontal plane

The above stress distribution agrees well with what is regarded as natural stress in the Stripa Mine.

Water pressure as a function of distance from a drift

A number of water pressure measurements were performed by Lawrence Berkeley Laboratory (LBL) at the ventilation drift in the Stripa Mine (Wilson, 1981). The presented diffusion experiments were carried out in the extensiometer drift which is located at the same level in the mine and just about 100 m from the ventilation drift. It is therefore assumed that the results from the ventilation drift is valid also for the extensiometer drift. The results from the water pressure measurements are illustrated in Figure A2.1.



Water pressure in the R-holes in the ventilation drift

If the water head above the axis of the drift is plotted as function of radial distance in a lin-log diagram as in Figure A2.2, a number of straight lines are obtained.



Figure A2.2. Water head above axis of the drift vs radial distance

A straight line in a lin-log diagram means that the pressure is defined as

$$P = C_1 + C_2 * \log r$$
 (A2.1)

where C_1 is the intercept, C_2 the slope of the line and r is the radial distance. Differentiation of Equation (A2.1) gives the pressure gradient as function of r,

$$\frac{\partial P}{\partial r} = \frac{C_2}{r \times \ln 10}$$
 (A2.2)

The slope for the weighted average curve is $C_2 = 75$, which gives

$$\frac{\partial P}{\partial r} = \frac{33}{r} \tag{A2.3}$$

This means that the difference between the pressure gradients for the injection hole and the surrounding rock is between 2 and 3 m/m (0.02-0.03 MPa/m) at the distance from the drift where the experiments have taken place ($\approx 10-20 \text{ m}$) if the injection hole is drilled straight downward. The difference will be less than 2-3 m/m if the injection hole is drilled in any other direction.

The only way to avoid the difficulties with the different pressure gradients and to perform a diffusion experiment is to drill a very deep hole, so that $\partial P/\partial r \rightarrow 0$. But this is unpractical.

Appendix 3

Tracer concentrations, Part I.

Table A3.1 gives the notation of the sampling cores, depth in the injection hole, radial distance from the injection hole as well as the relative concentrations for Uranine, Iodide and Cr-EDTA. The concentrations are based on an assumed uniform porosity of 0.345 % in the rock matrix and an assumed uniform density of 2.62 g/cm 3 . The relative concentrations are calculated using the tracer concentration in the water after leaching (see Chapter 3) and the porosity. The locations of the cores are given in Figure A3.1.



Core	No.	Depth [m]	Distance [mm]	Relative Uranine [%]	concent I ⁻ [%]	ration Cr-EDTA [%]
1	1 2 3 4 5	0.080	61 53 68 25	38.5 42.3 32.2 	38.7 43.8 34.8 	72.5 75.8 63.4
	6 7 8 9 10 11		52 52 105 90 83	35.0 30.6 35.5 -	36.8 32.9 37.1	64.3 56.8 64.9
	12		64	31.5	30.4	56.6
, 2	1 2 3	0.360	4 3 2 3 2 0	34.4 31.0	32.1 25.7	43.7 54.5 —
	4 5		37 38	37.0 36.1	33.6 32.2	42.7 71.3
3	1 2 3 4 5 6 7 8 9 10	0.585	18 43 104 56 81 70 72 59 100 40	29.0 35.2 13.6 23.0 24.0 24.1 29.9 35.6 9.3	24.9 34.4 13.1 18.1 33.6 28.5 29.4 35.2 13.3	54.3 66.3 22.2 42.7 21.7 22.2 54.0 64.8 11.3
4	1 2 3 4 5	≈0.645	≈110 ≈110 ≈110 ≈110 ≈110	9.0 23.7 18.0 40.6 22.8	6.1 19.6 17.8 40.0 21.1	21.6 28.0 15.4 29.9 41.5
5	1 2 3	≈0.670	≈110 ≈110 ≈110	33.4 33.3 19.6	26.6 29.5 18.0	50,4 61.5 39.8
6	1 2 3 4 5 6 7 8 9 10 11	0.925	43 35 64 70 80 103 83 101 81 63 107	39.7 16.3 38.0 	37.2 13.3 31.6 23.4 28.8 37.3 30.8 29.6 37.0 26.5	72.9 36.6 69.3 44.3 35.5 69.6 23.0 62.4 78.0 48.8

Table	A3.1.	Concentration	data,	Part	I
			,		_

Core	No.	Depth [m]	Distance [mm]	Relative Uranine [%]	concent I ⁻ [%]	ration Cr-EDTA [%]
7	1 2 3 4 5 6 7 8 9 10 11 12	0.980	83 99 58 63 42 104 80 94 17 33 62 21	30.0 19.0 36.1 25.7 30.7 13.8 18.9 22.4 16.7 20.7 28.7	25.9 18.2 31.8 23.9 26.5 15.5 23.0 25.7 15.3 17.7 26.6	29.1 25.0 56.1 43.9 68.6 23.8 31.4 37.8 43.1
8	1	1.035		_		_
9	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	1.085	105 106 100 83 69 87 93 73 73 73 53 61 41 31 18 53	11.9 13.6 13.1 22.2 22.1 20.7 19.9 17.3 35.5 23.1 25.7 31.3 29.9 37.0	$ \begin{array}{c} 10.6\\ 12.1\\ 11.1\\ 23.5\\ 26.0\\ 21.1\\ 20.7\\ 15.7\\ 29.7\\ 24.0\\ 22.6\\ 26.6\\ 25.7\\ 28.6\\ \end{array} $	11.5 24.9 39.7 37.5 24.2 42.2 21.6 39.0 66.0 49.7 65.5 72.8 68.1 72.0
10	$ \begin{array}{r} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ \end{array} $	1.140	113 102 81 96 79 74 49 48 28 32 12 31 95 80 61 47 100 84	10.8 11.3 14.0 19.3 26.2 30.9 38.6 38.2 40.3 39.6 37.3 29.8 15.0 16.4 26.2 31.3 13.5 19.9	14.2 15.0 14.9 15.7 22.8 25.8 33.6 34.5 38.0 38.2 34.0 27.2 20.3 15.8 24.6 26.3 7.2 12.2	12.2 10.8 18.6 39.1 43.4 57.6 78.4 78.3 79.0 84.1 73.4 64.9 13.4 33.1 45.2 63.9 19.2 45.2

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	Т	a	b	1	e	1	4 (3		1		с	0	n	t	i	n	u	е	ċ	l
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Core	No.	Depth [m]	Distance [mm]	Relative Uranine [%]	concent I ⁻ [%]	rätion Cr-EDTA [%]
11	1 2 3 4 5 6 7	≈1.270	≈90 ≈90 ≈90 ≈90 ≈90 ≈90 ≈90	4.6 7.9 10.8 10.5 11.4 6.7 6.1	5.8 7.8 9.2 7.9 7.8 10.7 10.5	2 . 1 6 . 3 1 2 . 0 1 1 . 2 3 . 5 2 . 7
12	1 2 3 4 5 6 7 8 9 10 11 12 13	≈1.330	 *80 	33.2 24.7 13.3 2.8 1.2 20.0 3.6 1.2 11.9 6.9 2.4 2.0 1.2	24.0 21.3 12.4 4.3 1.2 13.1 4.6 0.8 9.7 5.2 2.3 0.4 0.0	51.9 22.9 4.9 0.0 0.1 13.4 0.0 0.0 2.0 0.2 0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
13	1 2 3 4 5 6 7 8 9	1.605	117 95 109 89 110 90 70 91 66	3.7 2.0 1.0 1.4 0.8 0.7 1.1 0.6 1.0	$ \begin{array}{c} 1 . 0 \\ 0 . 6 \\ 0 . 3 \\ 0 . 3 \\ 0 . 1 \\ 0 . 1 \\ 0 . 1 \\ 0 . 1 \\ 0 . 1 \end{array} $	0.4 0.7 0.6 0.2 0.0 0.2 0.5 0.5 0.0
14	1 2 3 4 5 6 7 8 9 10 11 12	1.820	105 85 98 114 80 93 113 73 91 97 72 74	3.9 2.9 1.7 1.9 2.7 3.9 2.7 4.8 4.7 2.6 4.5 6.1	$ \begin{array}{r} 1 . 8 \\ 2 . 7 \\ 1 . 5 \\ 1 . 7 \\ 2 . 4 \\ 2 . 3 \\ 2 . 1 \\ 4 . 7 \\ 3 . 2 \\ 2 . 8 \\ 6 . 6 \\ 1 1 . 1 \end{array} $	0.2 0.9 0.0 0.8 0.1 0.0 1.8 0.7 0.2 0.0 0.0 0.0 1.7

Table A3.1 continued

Core	No.	Depth [m]	Distance [mm]	Relative Uranine [%]	concent I ⁻ [%]	ration Cr-EDTA [%]
15	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	2.025	62 81 62 95 78 106 92 116 98 103 108 87 98 81 66 21 40 71	$\begin{array}{c} 0.4\\ 0.6\\ 0.3\\ 0.7\\ 0.6\\ 0.7\\ 1.0\\ 0.4\\ 0.7\\ 1.9\\ 0.6\\ 0.9\\ 0.6\\ 2.4\\ 1.6\\ 0.8 \end{array}$	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 4 \\ 0 \ . \ 6 \\ 2 \ . \ 1 \\ - \\ 1 \ . \ 1 \\ 0 \ . \ 1 \\ 2 \ . \ 1 \\ 0 \ . \ 8 \\ 0 \ . \ 2 \end{array}$	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \ . \ 0 \\ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \$
16	1 2 3 4 5 6 7 8 9 10 11 12 13 14	2.125	42 20 40 35 18 50 58 81 118 100 100 82 60 106	1.0 0.6 0.9 1.4 1.4 0.6 0.7 0.8 0.5 0.6 0.4 0.8 0.7 0.8	$\begin{array}{c} 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\ 0 & . \\$	0.2 0.2 0.0 0.1 0.2 0.2 0.2 0.2 0.3 0.9 0.3 0.0 0.1 0.2 0.3 0.0 0.1 0.2 0.3

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Table A3.1 continued

Porosities and tracer concentrations, Part II.

Table A4.1 gives the notation of the sampling cores, depth in the injection hole, radial distance from the injection hole, porosity as well as the relative concentrations for Uranine, Iodide, and Cr-EDTA. The porosity is calculated from the weight difference between a wet and dry sampling core and an assumed uniform density of 2.62 g/cm³. The relative concentrations are calculated using the tracer concentration in the water after leaching (see chapter 3) and the porosity. The locations of the cores are given in Figure A4.1.

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Figure A4.1. Location of cores in Part II.

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I - [%]	ntration Cr-EDTA [%]
1	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	0.359	47 69 49 87 98 80 60 95 84 68 26 40 16 66 33	0.34 0.32 0.33 0.28 0.36 0.26 0.31 0.47 0.38 0.34 0.32 0.34 0.35 0.34 0.35	16.9 19.2 18.5 27.5 23.7 27.9 30.8 19.1 22.9 24.9 20.6 18.6 28.0 22.2 24.3	13.815.214.218.914.418.420.912.427.121.616.810.620.220.420.5	22.1 27.4 29.4 40.4 32.2 39.2 48.0 28.7 30.0 33.3 27.6 27.0 43.5 26.0 32.0
2	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	0.480	43 36 68 91 80 88 62 78 94 95 53 59 29 11 71 	0.28 0.31 0.36 0.43 0.30 0.29 0.25 0.31 0.30 0.27 0.25 0.31 0.30 0.27 0.25 0.30 0.33 0.36 0.22	35.2 34.6 30.8 29.6 25.2 27.6 32.0 23.9 25.1 28.2 35.3 38.1 34.0 33.1 26.4	27.1 25.7 27.8 24.0 15.4 17.6 21.4 15.2 12.6 22.0 18.7 20.1 22.3 22.8 18.1 	50.5 46.7 42.9 30.2 30.1 37.8 40.8 33.8 28.6 34.7 41.9 52.0 48.2 54.2 35.4 43.1
3	1 2 3 4 5 6 7 8 9 10 11	0.784	84 67 58 59 77 77 98 83 96 110 102	0.27 0.28 0.28 0.29 0.28 0.27 0.29 0.29 0.28 0.25 0.29 0.29 0.27	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \end{array}$	$\begin{array}{c} 0.3\\ 0.1\\ 0.2\\ 0.2\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0$	0.1 0.2 0.1 0.2 0.2 0.2 0.1 0.1 0.1 0.2 0.2 0.0

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Table A4.1. Porosity and concentration data, Part II

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concér I ⁻ [%]	ntration Cr-EDTA [%]
4	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	0.904	70 92 81 59 40 19 29 52 70 69 94 91 51 103 44 62 28	0.28 0.26 0.30 0.31 0.28 0.31 0.32 0.28 0.28 0.28 0.28 0.27 0.32 0.26 0.29 0.28 0.29 0.28 0.28 0.29 0.28 0.27 0.28 0.27 0.28	$\begin{array}{c} 0.3\\ 0.1\\ 0.1\\ 1.0\\ 16.9\\ 24.4\\ 20.0\\ 0.9\\ 0.2\\ 0.1\\ 0.1\\ 0.1\\ 0.0\\ 0.4\\ 0.1\\ 16.4\\ 1.7\\ 34.9 \end{array}$	2.3 0.2 0.2 2.8 10.5 13.7 11.1 2.8 0.0 0.5 0.1 0.1 1.8 0.1 14.2 30.3	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 6 \ . \ 8 \\ 3 \ 6 \ . \ 5 \\ 1 \ 0 \ . \ 4 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 1 \\ 7 \ . \ 3 \\ 0 \ . \ 0 \\ 4 \ . \ 0 \end{array}$
5	$ \begin{array}{r} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ \end{array} $	0.956	56 28 10 75 100 85 62 39 14 62 83 19 37 63 93 83 62 32	0.28 0.28 0.26 0.26 0.27 0.31 0.29 0.28 0.32 0.27 0.27 0.27 0.27 0.27 0.27 0.28 0.227 0.28 0.227 0.28 0.226 0.32 0.29 0.24 0.26	$\begin{array}{c} 0.9\\ 1.9\\ 16.3\\ 0.1\\ 0.0\\ 0.1\\ 0.7\\ 11.9\\ 22.9\\ 0.4\\ 0.1\\ 22.3\\ 20.6\\ 1.2\\ 0.1\\ 0.1\\ 5.6\\ 24.7 \end{array}$	$\begin{array}{c} 2 & . & 7 \\ 1 & 8 & . & 6 \\ 1 & 6 & . & 4 \\ 1 & . & 0 \\ 0 & . & 2 \\ 0 & . & 6 \\ 2 & . & 2 \\ 7 & . & 8 \\ 1 & 8 & . & 4 \\ 0 & . & 8 \\ 0 & . & 5 \\ 2 & 1 & . & 9 \\ 1 & 6 & . & 0 \\ 4 & . & 2 \\ 0 & . & 3 \\ 1 & . & 0 \\ 7 & . & 5 \\ 1 & 7 & . & 4 \end{array}$	$\begin{array}{c} 0.3\\ 12.5\\ 29.5\\ 0.2\\ 0.2\\ 0.0\\ 0.1\\ 4.5\\ 40.0\\ 0.1\\ 0.0\\ 37.8\\ 17.6\\ 0.0\\ 37.8\\ 17.6\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.3\\ 22.4 \end{array}$

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Table A4.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	ntration Cr-EDTA [%]
6	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	1.271	34 52 26 57 12 42 42 20 67 65 53 70 82 91 102 101 82 95 23	$\begin{array}{c} 0.33\\ 0.35\\ 0.34\\ 0.31\\ 0.35\\ 0.33\\ 0.33\\ 0.33\\ 0.43\\ 0.33\\ 0.34\\ 0.22\\ 0.25\\ 0.35\\ 0.35\\ 0.30\\ 0.34\\ 0.31\\ 0.26\\ 0.25\\ 0.31\\ \end{array}$	$\begin{array}{c} 9.1\\ 7.3\\ 16.5\\ 3.8\\ 17.8\\ 13.6\\ 5.2\\ 4.3\\ 0.5\\ 0.3\\ 0.6\\ 0.3\\ 0.6\\ 0.3\\ 0.1\\ 0.2\\ 0.2\\ 0.2\\ 0.6\\ 0.1\\ 13.5\end{array}$	$\begin{array}{c} 8.2\\ 5.8\\ 12.6\\ 4.2\\ 12.1\\ 11.5\\ 6.0\\ 6.0\\ 0.9\\ 1.1\\ 1.4\\ 0.2\\ 0.5\\ 0.1\\ 0.0\\ 0.1\\ 0.5\\ 0.2\\ 8.2 \end{array}$	9.4 1.8 20.5 0.2 27.2 8.7 2.6 4.7 0.0 0.0 0.0 0.0 0.0 0.0 0.1 0.0 0.1 0.0 0.0
7	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	1.315	76 68 31 55 42 63 86 100 92 87 69 42 19 15 19	0.29 0.26 0.32 0.36 0.30 0.32 0.41 0.31 0.31 0.31 0.32 0.27 0.28 0.27 0.29	$\begin{array}{c} 0.3\\ 1.9\\ 19.3\\ 1.2\\ 15.2\\ 2.1\\ 0.1\\ 0.1\\ 0.1\\ 0.1\\ 0.1\\ 0.5\\ 7.4\\ 23.5\\ 31.5\\ 17.9 \end{array}$	$\begin{array}{c} 0 \ . \ 7 \\ 2 \ . \ 8 \\ 1 \ 4 \ . \ 8 \\ 2 \ . \ 2 \\ 8 \ . \ 6 \\ 2 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 9 \\ 5 \ . \ 6 \\ 1 \ 2 \ . \ 7 \\ 1 \ 5 \ . \ 3 \\ 1 \ 1 \ . \ 0 \end{array}$	$\begin{array}{c} 0 \ . \ 2 \\ 0 \ . \ 3 \\ 1 \ 5 \ . \ 6 \\ 0 \ . \ 1 \\ 1 \ 0 \ . \ 3 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \ . \ 0 \\ 0 \ . \ 0 \ . \ 0 \\ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \$
8	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	1.365	52 68 75 89 67 74 89 102 94 12 16 39 63 23 46	0.28 0.30 0.29 0.29 0.28 0.33 0.29 0.25 0.31 0.27 0.26 0.33 0.30 0.34 0.30	9.9 2.2 1.3 0.3 3.3 1.1 0.2 0.1 0.1 21.8 27.2 11.6 2.0 16.7 10.3	$\begin{array}{c} 4 \ . \ 4 \\ 2 \ . \ 2 \\ 1 \ . \ 2 \\ 0 \ . \ 7 \\ 3 \ . \ 9 \\ 3 \ . \ 6 \\ 0 \ . \ 5 \\ 0 \ . \ 1 \\ 0 \ . \ 2 \\ 1 \ 3 \ . \ 7 \\ 2 \ 0 \ . \ 0 \\ 6 \ . \ 7 \\ 1 \ . \ 7 \\ 8 \ . \ 8 \\ 5 \ . \ 7 \end{array}$	$\begin{array}{c} 3.6\\ 0.7\\ 0.2\\ 0.0\\ 0.2\\ 0.1\\ 0.2\\ 0.0\\ 0.3\\ 33.7\\ 45.6\\ 10.9\\ 0.3\\ 16.5\\ 0.6\end{array}$

Table A4.1 continued

					Relative	conce	ntration
Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Uranine [%]	[%]	Cr-EDTA [%]
					······································		<u> </u>
9	1	1.409	20	0.29	19.9	11.7	20.0
	2		48	0.29	0.4	1.1	0.1
	3		70	0.28	0.0	0.2	0.0
	4		39	0.31	1.8	2.6	0.0
	5		45	0.26	3.1	2.5	0.9
	6		64	0.29	0.2	0.9	0.0
	7		81	0.28	0.0	0.1	0.0
	8		60	0.27	0.1	0.5	0.0
	9		68	0.34	0.1	0.5	0.1
	10		79	0.26	0.0	0.1	0.0
	11		105	0.25	0.1	0.0	0.0
	12		89	0.36	0.0	0.0	0.4
10	1	1.455	40	0.33	1.5	2.6	0.8
	2		65	0.36	0.1	0.0	0.0
	3		90	0.34	0.1	0.0	0.0
	4		69	0.27	0.1	0.0	0.0
	5		46	0.53	0.2	0.0	0.0
	6		36	0.33	0.1	0.1	0.0
	7		62	0.30	0.1	0.0	0.0
	8		65	0.40	0.0	0.0	0.1
	10		30	0.20	0.1	0.2	0.0
	10		6 <i>5</i> 67	0.00	0.1	0.0	0.0
	11		57	0.20	0.0	0.0	
11	1	1.505	11	0.29	13.6	13.5	17.2
	2		10	0.56	0.7	3.5	0.5
	3		26	-	—		, - ,
	4		36	0.39	4.4	5.2	4.4
	5		49	—			~ 7
	6		58	0.34	1.9	2.0	0.7
	7		36	-		0_0	0_0
	8		45	0.46	0.2	0.0	0.0
	9		64	0.34	0.1	0.0	0.0
	10		82	0.52	0.2	0.0	0 0
	11		100	0.51	0.1	0.0	0.0
12	1	1.551	17	0.35	3.4	3.9	1.5
	2		3 5	0.28	0.4	0.8	0.3
	3		55	0.27	0.1	0.0	0.5
	4		87	0.28	0.1	0.0	0.0
	5		34	0.30	0.1	0.0	0.0
	6		49	0.31	U.1 0 1	0.0	0.2
	/		/ 3	0.29	0.1	0.0	0.0
	8		/)	0.27	0.2	0.0	0 0
	У		20	0.04	U.1	0.0	· · ·

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Table A4.1 continued

Core No.		Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	ntration Cr-EDTA [%]
13	1 2 3 4 5 6 7 8 9	1.591	17 29 66 70 79 85 98 98 96 97	0.50 0.29 0.26 0.30 0.28 0.31 0.22 0.29 0.27	3.1 1.5 0.1 0.2 0.1 0.1 0.1 0.1 0.1 0.1	3.2 1.4 0.0 0.1 0.1 0.0 0.0 0.0 0.0 0.0	3.3 0.0 0.0 0.0 0.0 0.0 0.2 0.2 0.2 0.0
14	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	1.739	11 34 55 74 92 107 99 82 63 43 23 100 81 61 79 42 59 24 13 33 74 61	$\begin{array}{c} 0.32\\ 0.32\\ 0.38\\ 0.28\\ 0.30\\ 0.30\\ 0.28\\ 0.29\\ 0.31\\ 0.32\\ 0.31\\ 0.32\\ 0.34\\ 0.27\\ 0.28\\ 0.28\\ 0.34\\ 0.27\\ 0.28\\ 0.34\\ 0.30\\ 0.36\\ 0.31\\ 0.36\\ 0.31\\ 0.36\\ 0.34\\ 0.30\\ 0.32\\ 0.30\end{array}$	18.2 24.5 5.9 1.2 0.3 0.1 0.2 2.5 6.6 25.1 23.8 0.6 6.5 23.3 11.1 23.1 21.3 24.8 17.0 12.0 0.6 1.4	12.6 13.7 3.5 1.0 0.5 0.0 0.5 1.2 3.5 13.3 15.4 0.5 3.3 12.9 8.0 15.7 12.0 18.2 13.1 9.6 1.2 1.7	29.8 35.5 2.9 0.2 0.0 0.0 0.1 0.0 3.8 30.9 36.7 0.0 0.5 16.3 1.0 30.2 16.6 29.0 25.6 9.6 0.0 0.0 0.0 0.5 0.0 0.5 0.0 0.0
	23 24 25		75 90 96	0.30 0.34 0.44	0.8 0.2 0.1	1.5 0.5 0.3	0.0 0.0 0.0

Table A4.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I - [%]	ntration Cr-EDTA [%]
15	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	1.791	7 26 45 62 82 103 98 79 91 56 51 38 20 36 52 95 74 54 33 19 90 73 53 36 70	0.30 0.27 0.30 0.33 0.35 0.35 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32	$\begin{array}{c} 21.3\\ 27.6\\ 20.9\\ 11.3\\ 2.3\\ 0.1\\ 0.3\\ 1.4\\ 0.4\\ 6.8\\ 10.9\\ 12.0\\ 23.3\\ 24.4\\ 15.7\\ 1.1\\ 12.2\\ 14.5\\ 22.4\\ 23.3\\ 3.6\\ 10.5\\ 20.1\\ 21.3\\ 4.7 \end{array}$	14.316.511.77.42.90.50.82.41.25.67.912.015.412.98.51.44.67.012.816.32.04.29.09.310.3	$\begin{array}{c} 31.3\\ 42.8\\ 22.6\\ 5.6\\ 0.2\\ 0.0\\ 0.0\\ 0.2\\ 0.3\\ 1.6\\ 5.6\\ 19.2\\ 34.2\\ 33.0\\ 10.9\\ 0.0\\ 4.4\\ 16.2\\ 31.1\\ 36.6\\ 0.3\\ 0.8\\ 12.6\\ 23.3\\ 0.1\\ \end{array}$
16	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24	1.843	$ \begin{array}{r} 11 \\ 30 \\ 50 \\ 71 \\ 89 \\ 105 \\ 97 \\ 75 \\ 53 \\ 36 \\ 29 \\ 89 \\ 70 \\ 56 \\ 43 \\ 86 \\ 76 \\ 90 \\ 89 \\ 103 \\ 53 \\ 35 \\ 20 \\ 40 \\ \end{array} $	$\begin{array}{c} 0.27\\ 0.33\\ 0.31\\ 0.34\\ 0.37\\ 0.31\\ 0.32\\ 0.31\\ 0.32\\ 0.29\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.31\\ 0.33\\ 0.32\\ 0.31\\ 0.33\\ 0.37\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.29 \end{array}$	$\begin{array}{c} 24.7\\ 20.5\\ 18.0\\ 13.2\\ 5.1\\ 1.3\\ 3.7\\ 16.8\\ 24.0\\ 23.4\\ 26.2\\ 7.8\\ 22.1\\ 20.2\\ 19.5\\ 4.9\\ 3.4\\ 1.6\\ 0.6\\ 7.6\\ 21.3\\ 16.6\\ 21.5\\ \end{array}$	$\begin{array}{c} 21.8\\ 17.0\\ 11.5\\ 8.5\\ 4.5\\ 2.2\\ 3.2\\ 9.0\\ 14.3\\ 17.9\\ 22.0\\ 4.8\\ 10.3\\ 11.9\\ 13.7\\ 3.5\\ 4.4\\ 3.2\\ 3.2\\ 1.8\\ 10.7\\ 16.0\\ 14.2\\ 1.8\\ 10.7\\ 16.0\\ 14.2\\ 13.0\\ \end{array}$	$\begin{array}{c} 40.8\\ 32.6\\ 28.1\\ 9.8\\ 0.4\\ 0.3\\ 0.1\\ 6.6\\ 33.2\\ 39.2\\ 42.2\\ 0.5\\ 8.4\\ 18.7\\ 13.4\\ 0.5\\ 0.7\\ 0.6\\ 0.5\\ 2.7\\ 35.7\\ 32.4\\ 26.3\\ \end{array}$

Table A4.1 continued

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Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concen I ⁻ [%]	tration Cr-EDTA [%]
17	1 2 3 4 5 6 7 8 9 10 11 2 3 4 5 6 7 8 9 10 11 2 13 14 5 16 17 8 9 20 21 22 3 24 25	1.891	53 74 36 17 12 30 51 30 46 68 63 103 89 79 80 97 102 13 29 49 73 92 35 55 88	$\begin{array}{c} 0.30\\ 0.29\\ 0.28\\ 0.31\\ 0.34\\ 0.32\\ 0.30\\ 0.33\\ 0.30\\ 0.31\\ 0.32\\ 0.31\\ 0.32\\ 0.31\\ 0.32\\ 0.31\\ 0.33\\ 0.34\\ 0.35\\ 0.27\\ 0.32\\ 0.31\\ 0.34\\ 0.33\\ 0.32\\ 0.31\\ 0.32\\ 0.31\\ 0.32\\ 0.26 \end{array}$	$\begin{array}{c} 2 \ 0 \ . \ 7 \\ 8 \ . \ 2 \\ 2 \ 6 \ . \ 3 \\ 2 \ 3 \ . \ 1 \\ 2 \ 2 \ . \ 2 \\ 2 \ 5 \ . \ 5 \\ 2 \ 6 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \ 0 \ . \ 8 \\ 2 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ . \ 8 \ 0 \ 0 \ . \ 8 \ 0 \ 0 \ . \ 8 \ 0 \ 0 \ . \ 8 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0$	12.5 6.1 25.0 19.1 18.6 20.7 14.7 13.6 16.0 11.1 12.0 1.8 5.3 8.2 5.7 3.6 3.6 19.2 16.9 9.6 4.3 1.9 9.2 5.4 1.1	13.7 0.0 34.7 31.9 32.0 38.2 28.6 28.0 29.7 4.8 12.5 0.0 0.0 1.6 0.0 0.0 1.6 0.0 0.0 29.1 24.7 4.6 0.0 0.0 10.5 0.0 0.0 10.5 0.0 0.0 0.0 10.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0
18	$ \begin{array}{c} 1\\2\\3\\4\\5\\6\\7\\8\\9\\10\\11\\12\\13\\14\\15\\16\\17\\18\\9\\20\\21\\22\\3\\24\\25\\26\end{array} $	2.031	$ \begin{array}{r} 8 \\ 27 \\ 45 \\ 64 \\ 80 \\ 100 \\ 96 \\ 74 \\ 88 \\ 53 \\ 69 \\ 33 \\ 23 \\ 52 \\ 41 \\ 68 \\ 89 \\ 69 \\ 47 \\ 28 \\ 13 \\ 28 \\ 48 \\ 64 \\ 64 \\ 88 \\ \end{array} $	$\begin{array}{c} 0.33\\ 0.34\\ 0.36\\ 0.35\\ 0.35\\ 0.32\\ 0.32\\ 0.27\\ 0.32\\ 0.27\\ 0.32\\ 0.27\\ 0.30\\ 0.32\\ 0.31\\ 0.34\\ 0.33\\ 0.32\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.31\\ 0.33\\ 0.31\\ 0.31\\ 0.33\\ 0.31\\ 0.33\\ 0.31\\ 0.33\\ 0.31\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\ 0.33\\$	17.7 27.9 13.2 2.4 0.2 0.1 0.1 0.3 0.1 3.3 0.5 13.0 12.5 2.1 3.0 0.2 0.4 1.7 2.0 12.3 24.0 8.3 1.2 0.6 0.1 0.1	17.9 17.8 9.3 2.9 0.6 0.1 0.2 0.8 0.4 5.2 1.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12.1 16.1 7.9 2.3 1.2 0.7 0.4	$\begin{array}{c} 27.6\\ 32.3\\ 7.6\\ 0.1\\ 0.3\\ 0.0\\ 0.2\\ 0.0\\ 0.2\\ 0.0\\ 0.1\\ 0.4\\ 0.0\\ 7.4\\ 10.5\\ 0.3\\ 0.8\\ 0.1\\ 0.5\\ 0.3\\ 0.8\\ 0.1\\ 0.0\\ 0.2\\ 0.2\\ 6.8\\ 27.1\\ 3.0\\ 0.0\\ 0.1\\ 0.1\\ 0.1\\ 0.1\\ 0.1\\ 0.1\\ 0$

Table A4.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	Cr-EDTA
19	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 7 18 9 20 21 22 23 24	2.079	56 74 90 106 35 16 9 29 38 66 31 86 84 101 99 9 29 22 51 54 71 94 67 89	$\begin{array}{c} 0.27\\ 0.27\\ 0.28\\ 0.28\\ 0.29\\ 0.32\\ 0.32\\ 0.29\\ 0.29\\ 0.28\\ 0.30\\ 0.32\\ 0.31\\ 0.27\\ 0.26\\ 0.25\\ 0.25\\ 0.28\\ 0.30\\ 0.32\\ 0.30\\ 0.31\\ 0.31\\ 0.31\\ 0.32\\ 0.29\\ 0.28 \end{array}$	$ \begin{array}{c} 19.8\\ 7.5\\ 1.4\\ 0.3\\ 35.3\\ 30.2\\ 32.8\\ 33.8\\ 14.5\\ 8.7\\ 21.9\\ 14.8\\ 2.3\\ 1.0\\ 6.9\\ 21.7\\ 37.6\\ 27.6\\ 29.6\\ 27.3\\ 9.6\\ 5.6\\ 10.8\\ 1.2\\ \end{array} $	15.89.04.11.326.726.025.924.615.210.216.011.17.82.85.614.429.318.918.216.512.41.98.12.6	$\begin{array}{c} 9.3\\ 0.7\\ 0.0\\ 0.3\\ 39.2\\ 42.7\\ 46.0\\ 34.4\\ 4.8\\ 2.9\\ 23.1\\ 14.5\\ 0.6\\ 0.2\\ 4.9\\ 25.6\\ 52.2\\ 35.9\\ 26.1\\ 24.4\\ 0.6\\ 0.0\\ 2.0\\ 0.1\\ \end{array}$
20	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	2.239	86 101 80 102 86 101 64 61 75 65 47 43 27 41 14 73 47 60 28 11 43 20	$\begin{array}{c} 0.25\\ 0.23\\ 0.26\\ 0.30\\ 0.30\\ 0.24\\ 0.28\\ 0.25\\ 0.29\\ 0.27\\ 0.29\\ 0.29\\ 0.29\\ 0.29\\ 0.29\\ 0.28\\ 0.28\\ 0.28\\ 0.28\\ 0.28\\ 0.28\\ 0.28\\ 0.28\\ 0.29\\ 0.24\\ 0.29\\ 0.24\\ 0.29\\ 0.30\\ 0.26\\ 0.27\end{array}$	26.8 10.7 29.7 5.1 11.8 1.1 30.8 40.3 8.4 14.4 26.8 34.7 27.9 31.4 34.3 40.1 39.2 49.6 36.4 18.4 18.4 43.5 41.0	16.88.917.94.98.72.219.828.96.710.419.329.822.519.640.628.534.335.329.417.537.834.5	$\begin{array}{c} 8 & . & 8 \\ 0 & . & 3 \\ 1 & 5 & . & 3 \\ 1 & . & 2 \\ 4 & . & 5 \\ 0 & . & 3 \\ 3 & 5 & . & 4 \\ 5 & 0 & . & 7 \\ 1 & . & 2 \\ 3 & . & 5 \\ 3 & 2 & . & 2 \\ 5 & 4 & . & 8 \\ 3 & 9 & . & 1 \\ 3 & 2 & . & 6 \\ 5 & 2 & . & 2 \\ 2 & 8 & . & 9 \\ 5 & 3 & . & 0 \\ 5 & 4 & . & 0 \\ 4 & 7 & . & 9 \\ 3 & 2 & . & 5 \\ 5 & 9 & . & 3 \\ 5 & 6 & . & 1 \end{array}$

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Table A4.1 continued

Core No.		Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	ntration Cr-EDTA [%]
21	1	2.624	103	0.28	46.5	27.8	45.2
	2		87	0.29	36.5	28.8	54.3
	3		70	0.29	36.3	44.8	54.3
	4		53	0.30	40.1	37.7	64.4
	5		35	0.31	35.5	28.6	56.9
	6		17	0.31	28.5	34.3	47.4
	7		100	0.31	37.3	24.8	47.7
	8		82	0.31	35.2	28.3	58.9
	9		64	0.32	30.5	29.1	51.9
	10		45	0.30	32.4	29.9	52.9
	11		26	0.34	41.1	34.2	64.7
	12		8	0.28	34.8	27.4	57.3
	13		9 3 [°]	0.30	43.3	24.6	42.9
	14		77	0.29	38.2	29.6	57.9
	15		58	0.28	34.8	32.6	59.1
	16		41	0.28	34.6	30.8	55.4
	17		2 5	0.28	39.0	34.4	59.5
	18		76	0.29	40.4	26.8	45.3
	19		56	0.28	38.1	31.1	57.1
	20		102	0.29	47.0	29.6	54.3
	21		83	0.30	38.5	33.1	54.6
	22		61	0.28	35.6	32.3	53.2
	23		42	0.27	42.4	37.6	60.4
	24		28	0.26	45.5	40.5	62.7
	25		11	0.32	36.3	26.0	54.6
	26		95	0.30	39.9	26.7	50.1
	27		77	0.28	40.6	33.5	62.0
	28		60	0.27	41.2	35.8	58.6
	29		46	0.31	44.6	37.3	62.0
	30		75	0.26	37.7	28.9	57.6

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Table A4.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	ntration Cr-EDTA [%]
22	1	2.672	79	0.34	27.8	25.1	39.7
	2		95	0.29	41.4	31.2	50.5
	3		100	0.31	35.7	23.1	41.4
	4		94	0.29	41.8	25.4	33.0
	5		70	0.34	34.4	26.4	49.8
	6		60	0.32	26.2	37.0	40.9
	7		79	0.28	44.4	27.3	38.1
	8		73	0.30	41.6	36.5	63.1
	9		99	0.29	40.5	29.3	50.6
	10		79	0.30	38.7	33.9	59.6
	11		56	0.30	. 41.2	37.0	62.8
	12		59	0.31	35.4	30.1	53.1
	13		79	0.27	42.5	34.2	59.9
	14		41	0.32	35.2	31.3	52.9
	15		36	0.30	40.5	35.6	62.3
	16		42	0.29	44.7	39.3	64.3
	17		63	0.29	34.4	32.1	54.7
	18		51	0.28	49.0	38.9	73.9
	19		61	0.29	41.0	30.8	55.4
	20		41	0.25	47.2	43.1	70.7
	21		31	0.28	42.0	36.4	64.8
	22		17	0.33	33.0	30.3	51.9
	23		23	0.32	41.6	36.8	66.8
	24		19	0.32	38.8	32.9	55.4

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Table A4.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	ntration Cr-EDTA [%]
1 E	1 2 3 4 5 6 7 8 9 10 11 12 13 14	0.314	200 174 202 197 165 248 236 167 187 173 216 215 229 219	0.37 0.26 0.40 0.31 0.32 0.32 0.40 0.32 0.40 0.32 0.28 0.42 0.35 0.32 0.31 0.30	11.330.09.522.37.42.89.113.419.017.111.812.27.414.4	12.128.511.420.210.55.88.614.719.515.713.414.711.212.1	$\begin{array}{c} 9.1\\ 39.6\\ 10.0\\ 23.8\\ 5.0\\ 0.8\\ 7.5\\ 16.5\\ 20.8\\ 21.0\\ 9.3\\ 10.4\\ 4.0\\ 12.4 \end{array}$
2 E	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	0.374	177 236 246 	0.27 0.30 0.33 0.34 0.30 0.38 0.32 0.38 0.32 0.38 0.30 0.29 0.29 0.29 0.29 0.29 0.29 0.33 0.27 0.30	$\begin{array}{c} 23.1\\ 12.2\\ 1.8\\\\ 12.1\\ 14.8\\ 11.2\\ 9.6\\ 11.8\\ 12.4\\ 12.1\\ 22.0\\ 8.3\\ 15.9\\ 3.7 \end{array}$	26.0 14.1 17.5 12.0 19.7 14.0 11.8 14.6 28.1 21.1 17.6 18.1	$ \begin{array}{c} 28.6\\ 7.1\\ 0.5\\ \end{array} $ $ \begin{array}{c} 10.7\\ 13.0\\ 10.3\\ 5.9\\ 10.4\\ 20.9\\ 9.5\\ 26.1\\ 2.7\\ 21.0\\ 1.9\\ \end{array} $
3 E	1 2 3 4 5 6 7 8 9 10 11 12 13	0.424	2 3 9 2 2 3 1 9 1 1 5 8 1 7 3 2 2 8 1 9 7 2 5 0 1 8 9 2 1 7 2 2 3 2 0 1 1 8 5	0.28 0.29 0.43 0.38 0.24 0.32 0.21 0.29 0.37 0.29 0.40 0.29 0.40 0.28	20.8 13.9 20.4 12.9 16.4 9.8 17.5 17.8 7.8 16.0 17.8 16.0 17.8 16.4 14.6	21.7 13.6 19.6 11.7 16.5 7.7 15.4 16.2 7.5 12.2 13.3 12.0 13.6	22.7 18.9 31.3 16.1 17.2 13.1 17.2 16.0 14.3 15.7 22.8 21.9 23.6
4 E	1 2 3 4 5 6 7 8	0.849	180 234 245 166 201 241 211 163	0.36 0.29 0.32 0.33 0.38 0.26 0.32 0.34	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 2 \end{array}$	0.0 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.2 0.0 0.1 0.0 0.4 0.2 0.0

Table A4.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	conce I- [%]	ntration Cr-EDTA [%]
5 E	1 2 3 4 5 6 7 . 8	0.904	234 166 244 137 215 248 196 154	0.24 0.28 0.26 0.28 0.27 0.25 0.25 0.27 0.29	0.2 0.2 0.3 0.2 0.2 0.2 0.3 0.3 0.2	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	$\begin{array}{c} 0 & . & 0 \\ 0 & . & 2 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 2 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \end{array}$
6 E	1 2 3 4 5 6 7	1.136	2 5 0 1 5 3 2 0 5 2 0 7 1 7 2 2 3 3 1 7 3	0.26 0.25 0.29 0.28 0.28 0.28 0.28 0.29 0.28	0.3 0.2 0.2 0.1 0.2 0.2 0.2 0.2	0.0 0.0 0.0 0.0 0.0 0.0 0.0	$\begin{array}{c} 0 \ . \ 3 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \end{array}$
7 E	1 2 3 4 5 6 7 8	1.235	250 155 214 198 226 236 184 174	0.32 0.28 0.23 0.30 0.27 0.24 0.31 0.29	0.0 0.1 0.2 0.1 0.1 0.1 0.1 0.1 0.1	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \end{array}$	0.0 0.2 0.0 0.4 0.4 0.4 0.0
8 E	1 2 3 4 5 6 7 8	1.409	155 250 200 210 177 238 235 173	0.37 0.60 0.32 0.32 0.40 0.28 0.39 0.32	0.2 0.1 0.2 0.1 0.2 0.2 0.2 0.1 0.2	0.0 0.1 0.0 0.0 0.0 0.0 0.0 0.0	0.4 0.2 0.5 0.0 0.0 0.1 0.0 0.0
9 E	1 2 3 4 5 6 7 8	1.455	250 155 212 202 172 175 235 232	0.50 0.28 0.32 0.18 0.34 0.38 0.45 0.33	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 2 \\ 0 \ . \ 3 \\ 0 \ . \ 2 \\ 0 \ . \ 1 \\ 0 \ . \ 2 \end{array}$	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \end{array}$	$\begin{array}{c} 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \end{array}$
10E	1 2 3 4 5 6 7	1.596	250 153 202 211 237 	0.38 0.36 0.30 0.32 0.36 	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 2 \\ 0 \ . \ 1 \\ \hline \end{array}$	0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0

Table A4.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	tration Cr-EDTA [%]
11E	1 2 3 4 5 6 7 8	1.646	252 153 216 202 176 241 233 168	0.31 0.28 0.37 0.35 0.34 0.41 0.37 0.30	0.1 0.2 0.1 0.1 0.1 0.1 0.1 0.1 0.1	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \end{array}$	0.1 0.7 0.0 0.0 0.5 0.0 0.0 0.0
12E	1 2 3 4 5 6 7 8	1.786	251 153 215 203 241 179 173 232	0.29 0.28 0.27 0.38 0.29 0.33 0.38 0.35	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \end{array}$	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.3 0.0 0.0 0.0 0.0 0.0 0.0 0.0
13E	1 2 3 4 5 6 7 8	1.838	248 153 214 195 180 238 232 170	0.32 0.35 0.31 0.34 0.36 0.29 0.37 0.32	0.0 0.0 0.0 0.0 0.0 0.0 0.1 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \end{array}$
14E	1 2 3 4 5 6 7 8	1.966	250 153 201 214 180 170 240 234	0.31 0.28 0.30 0.34 0.38 0.31 0.36 0.33	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 1 \\ 0 \ . \ 2 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \end{array}$	0.0 0.0 0.0 0.0 0.0 0.1 0.0 0.0	0.1 0.7 0.4 0.4 0.6 0.0 0.4 0.4
15E	1 2 3 4 5 6 7 8	2.036	2 5 2 1 5 3 2 1 2 2 0 3 2 4 0 2 3 4 1 7 2 1 7 7	0.30 0.28 0.28 0.28 0.36 0.29 0.30 0.30	0.1 0.2 0.1 0.2 0.2 0.2 0.2 0.4 0.2	0.0 0.1 0.1 0.0 0.0 0.0 0.0	0.5 0.6 0.2 0.0 0.0 0.1 0.3 0.5
. 6 E	1 2 3 4 5 6 7 8	2.174	250 150 212 207 178 235 173 237	0.39 0.33 0.38 0.37 0.32 0.37 0.37 0.37	0.2 0.1 0.2 0.1 0.1 0.1 0.2 0.1	0.0 0.3 0.0 0.1 0.4 0.1 0.2 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0

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Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	ntration Cr-EDTA [%]
17E	1 2 3 4 5 6 7 8	2.219	250 150 213 210 171 177 240 234	0.33 0.31 0.31 0.34 0.33 0.29 0.31 0.34	0.3 0.2 0.2 0.0 0.1 0.1 0.1 0.1	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \end{array}$	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
18E	1 2 3 4 5 6 7 8	2.269	2 4 6 1 5 5 2 0 6 2 0 8 1 7 6 2 3 2 2 3 2 2 0 8	0.32 0.29 0.32 0.31 0.30 0.30 0.30 0.37 0.32	0.4 0.2 0.3 0.1 0.2 0.2 0.3	0.2 0.1 0.2 0.1 0.1 0.1 0.2 0.2	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
19E	1 2 3 4 5 6 7 8 9 10 11 12	2.409	156 254 206 209 166 164 192 248 229 178 187 190	0.29 0.25 0.29 0.30 0.34 0.33 0.35 0.33 0.32 0.36 0.32 0.33	$\begin{array}{c} 0.8\\ 6.3\\ 7.0\\ 13.2\\ 1.6\\ 0.6\\ 4.5\\ 2.2\\ 3.1\\ 1.7\\ 4.3\\ 4.4 \end{array}$	$\begin{array}{c} 2 & . \\ 9 \\ 11 & . \\ 6 & . \\ 7 \\ 18 & . \\ 5 & . \\ 1 \\ 3 & . \\ 4 \\ 10 & . \\ 7 \\ 4 & . \\ 0 \\ 5 & . \\ 0 \\ 6 & . \\ 0 \\ 6 & . \\ 7 \end{array}$	$\begin{array}{c} 0 \ . \ 1 \\ 5 \ . \ 2 \\ 9 \ . \ 6 \\ 10 \ . \ 6 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 5 \ . \ 9 \\ 1 \ . \ 4 \\ 3 \ . \ 1 \\ 2 \ . \ 2 \\ 4 \ . \ 5 \\ 5 \ . \ 5 \end{array}$
2 O E	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	2.459	156 162 186 163 183 173 197 182 257 214 209 203 237 240 187 206 227	0.40 0.39 0.38 0.36 0.37 0.39 0.38 0.30 0.35 0.29 0.32 0.28 0.25 0.33 0.31 0.26	9.5 8.9 7.5 7.0 7.6 8.8 8.0 0.7 0.3 13.9 12.0 8.4 0.7 2.4 2.0 10.7	$ \begin{array}{r} 10.6\\ 10.7\\ 6.2\\ 9.2\\ 8.1\\ 7.2\\ 5.3\\ 2.0\\ 1.1\\ 11.8\\ 9.6\\ 10.5\\ 1.1\\ 2.4\\ 3.0\\ 9.5\\ \end{array} $	7.7 4.3 2.0 4.1 3.2 1.9 0.9 0.0 0.2 10.1 4.1 6.9 0.0 0.4 0.0 0.4 0.0 6.1

Table A4.1 continued

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Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	conce I ⁻ [%]	ntration Cr-EDTA [%]
21E	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	2.514	156 253 210 203 181 203 229 166 166 166 166 185 205 183 178 208 186 237 235	0.36 0.35 0.34 0.31 0.34 0.33 0.31 0.31 0.31 0.32 0.32 0.32 0.32 0.32 0.33 0.30 0.31 0.31 0.34 0.36 0.64	5.8 0.1 0.1 4.7 2.0 0.4 0.2 1.9 3.0 0.3 0.2 1.6 1.9 0.5 0.3 0.1 0.0	$\begin{array}{c} 4 . 9 \\ 0 . 1 \\ 0 . 1 \\ 2 . 4 \\ 2 . 7 \\ 0 . 9 \\ 0 . 3 \\ 4 . 5 \\ 2 . 4 \\ 0 . 9 \\ 0 . 5 \\ 3 . 4 \\ 4 . 2 \\ 1 . 6 \\ 0 . 6 \\ 0 . 1 \\ 0 . 2 \end{array}$	$\begin{array}{c} 2 & . & 8 \\ 0 & . & 0 \\ 0 & . & 2 \\ 0 & . & 1 \\ 0 & . & 1 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \end{array}$
22E	1 2 3 4 5 6 7 8 9 10	2.594	245 241 226 224 225 200 196 200 173 244	$\begin{array}{c} 0.31\\ 0.33\\ 0.32\\ 0.32\\ 0.34\\ 0.33\\ 0.31\\ 0.32\\ 0.31\\ 0.32\\ 0.31\\ 0.32 \end{array}$	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \end{array}$	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 1 \ . \ 0 \\ 0 \ . \ 0 \end{array}$	<pre>. 0.0 0.0 0.0 0.0 0.2 0.0 0.1 0.3 0.0 0.0</pre>
23E	1 2 3 4 5 6 7 8 9 10 11 12 13 14	2.644	217 202 166 180 165 187 209 197 220 213 185 184 184 202	0.29 0.29 0.30 0.30 0.30 0.30 0.30 0.31 0.28 0.31 0.31 0.31 0.31 0.30	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 2 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 2 \\ 0 \ . \ 1 \end{array}$	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 2 \\ 1 \ . \ 5 \\ 0 \ . \ 4 \\ 1 \ . \ 5 \\ 0 \ . \ 3 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 2 \\ 0 \ . \ 5 \\ 0 \ . \ 3 \\ 0 \ . \ 2 \\ 0 \ . \ 1 \end{array}$	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.4 0.0 0.0

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Table A4.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	ntration Cr-EDTA [%]
24E	1	2.759	180	0.30	0.1	0.0	0.0
	2		225	0.28	0.1	0.0	0.0
	3		193	0.29	0.2	0.0	0.0
	4		218	0.31	0.1	0.1	0.4
	5		161	0.32	0.0	0.0	0.0
	6		243	0.30	0.1	0.0	0.1
	7		160	0.31	0.1	0.0	0.0
	8		243	0.30	0.1	0.0	0.2
	9		198	0.31	0.2	0.0	0.3
	10		213	0.30	0.1	0.0	0.4
	11		220	0.34	0.1	0.0	0.1
	12		207	0.30	0.1	0.0	0.0
	13		217	0.31	0.0	0.0	0.1
	14		224	0.29	0.1	0.0	0.1

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Table A4.1 continued

Porosities and tracer concentrations, Part III.

Table A5.1 gives the notation of the sampling cores, depth in the injection hole, radial distance from the injection hole, porosity as well as the relative concentrations for Uranine, Iodide, and Cr-EDTA. The porosity is calculated from the weight difference a between wet and dry sampling core and an assumed uniform density of 2.62 g/cm³. The relative concentrations are calculated using the tracer concentration in the water after leaching (see chapter 3) and the porosity. The locations of the cores are given in Figure A5.1.



Figure A5.1. Location of cores in Part III.

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	ntration Cr-EDTA [%]
				<u>, , , , , , , , , , , , , , , , , , , </u>			
1	1	0.275	52	0.39	21.4	20.4	43.6
	2		43	0.30	28.7	29.7	60.5
	3		79	0.32	28.2	32.5	
	4		82	0.28	24.8	20.5	-
	5		82	0.34	17.9	15.4	-
	6		63	0.33	22.8	17.4	37.3
	7		60	0.33	19.4	20.8	43.2
	8		67	0.29	26.0	27.4	55.9
	9		56	0.33	24.6	27.5	53.0
	10		40	0.32	27.8	26.5	52.4
	11		97		—	-	-
	12		37	0.34	27.0	28.0	48.7
	13		73	0.31	24.0	23.9	38.3
	14		3 5	0.40	21.4	20.5	46.6
	15		13	0.29	23.8	24.7	56.9
	16		18	0.29	24.1	24.0	59.5
	17		18	0.29	30.6	31.8	68.0
2	1	0.485	86	0.32	28.8	34.9	66.6
	2		92	0.36	26.0	34.6	75.4
	3		80	0.38	30,0	16.6	86.2
	4		87	0.37	32.4	24.2	71.7
	5		71	0.40	26.9	36.0	90.6
	6		71	0.37	25.7	29.5	
	7		45	0.33	34.0	34.9	73.5
	8		62	0.34	34.8	40.8	78.5
	9		46	0.36	35.3	35.1	83.4
	10		61	0.36	33.9	32.3	76.8
	11		44	0.36	33.5	32.6	76.2
	12		28	0.35	26.8	30.2	71.8
	13		10	0.38	26.2	30.3	75.9

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Table A5.1. Porosity and concentration data, Part III

					Relative	conce	ntration
Core	No.	Depth	Distance	Porosity	Uranine	I -	Cr-EDTA
		[m]	[mm]	[%]	[%]	[%]	[%]
			,	<u></u>			
3	1	0 725	9.8	0.41	23.2	15.0	63.1
5	2	0.725	90	0 46	57.7	30.0	73.3
	3		80	0.39	48.7	35.8	77.2
	4		69	0.41	92.0	34.5	74.7
	5		79	0.42	26.8	31.9	69.6
	6		60	0.41	24.0	28.6	70.1
	7		80	0.43	72.4	29.2	66.8
	8		67	0.43	51.8	27.5	61.2
	9		60	0.44	28.1	35.0	75.1
	10		71	0.41	30.0	36.6	75.0
	11		52	0.42	29.1	35.6	82.2
	12		53	0.44	32.4	36.2	80.5
	13		41	0.46	29.6	33.8	81.9
	14		34	0.43	28.0	35.4	79.8
	15		14	0.35	26.2	32.6	62.7
	16		25	0.38	27.8	32.6	65.9
	17		44	0.42	22.4	30.9	66.9
	18		28	0.38	28.3	34.7	67.1
	19		9	0.36	30.3	38.1	67.7
	20		48	0.39	26.8	30.4	62.6
	21		61	0.39	23.6	26.9	66.4
	22		45	0.35	21.4	26.0	58.6
	23		22	0.35	25.9	34.4	70.2
	24		36	0.36	21.5	27.1	53.6
	25		94	0.48	27.1	27.2	61.2
4	1	0.775	94	0.42	23.6	32.6	79.0
	2	••••	78	0,42	39.0	31.9	80.2
	3		72	0.38	53.7	31.2	80.6
	4		96	0.40	106.9	31.3	71.9
	5		76	0.41	99.1	33.6	79.0
	6		73	0.43	27.8	34.4	70.8
	7		90	0.42	28.1	30.2	64.2
	8		78	0.40	29.2	34.7	68.6
	9		58	0.39	37.0	35.1	68.6
	10		65	0.40	24.1	28.6	58.0
	11		52	0.38	71.9	29.6	75.2
	12		57	0.42	30.9	35.9	79.8
	13		56	0.39	25.4	32.5	69.4
	14		40	0.37	29.3	35.0	83.2
	15		33	0.38	29.0	35.7	72.0
	16		40	0.41	31.0	36.9	81.8
	17		47	0.39	43.0	34.5	74.4
	18		2 5	0.40	26.4	32.4	72.2
	19		13	0.38	30.2	36.5	82.0
	20		21	0.38	29.4	36.3	78.6

Table A5.1 continued

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Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	conce I- [%]	ntration Cr-EDTA [%]
5	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	0.825	84 81 63 63 35 51 41 66 52 30 51 21 19 35 98 82	0.44 0.38 0.40 0.40 0.35 0.42 0.38 0.38 0.38 0.37 0.35 0.35 0.36 0.34 0.36 0.35 0.46 0.46 0.44	78.5 48.8 30.0 27.7 32.1 29.6 30.7 28.7 18.4 20.5 24.6 29.0 26.8 25.9 11.0 17.0	$\begin{array}{c} 27.6\\ 34.6\\ 36.0\\ 34.2\\ 37.2\\ 35.2\\ 35.4\\ 30.6\\ 21.2\\ 24.3\\ 28.6\\ 34.3\\ 31.3\\ 31.0\\ 16.0\\ 22.2\end{array}$	69.0 75.7 80.5 73.2 77.0 80.3 77.3 75.9 54.9 54.9 56.9 62.6 71.1 66.2 67.8 55.3 62.1
6	$ \begin{array}{c} 1\\ 2\\ 3\\ 4\\ 5\\ 6\\ 7\\ 8\\ 9\\ 10\\ 11\\ 12\\ 13\\ 14\\ 15\\ 16\\ 17\\ 18\\ 19\\ 20\\ 21\\ \end{array} $	0.975	93 74 53 33 15 88 67 46 30 14 80 61 46 34 61 46 34 64 84 68 48 34 57 75	$\begin{array}{c} 0.36\\ 0.38\\ 0.36\\ 0.37\\ 0.37\\ 0.35\\ 0.36\\ 0.36\\ 0.36\\ 0.36\\ 0.36\\ 0.35\\ 0.35\\ 0.41\\ 0.40\\ 0.45\\ 0.40\\ 0.45\\ 0.40\\ 0.45\\ 0.40\\ 0.39\\ 0.38\\ 0.41\\ 0.38\end{array}$	35.2 30.7 32.9 32.8 22.6 34.0 31.2 33.0 33.8 29.3 43.1 26.5 27.1 31.0 9.7 40.5 28.0 26.3 17.4 20.4 28.9	30.5 37.7 35.8 26.0 35.7 34.6 38.0 38.3 32.4 40.3 32.4 40.3 32.4 40.3 31.0 35.2 15.9 28.7 30.3 31.2 20.7 19.8 29.3	62.1 64.7 67.2 64.5 49.0 69.1 62.6 66.0 67.0 57.9 70.1 56.8 57.6 64.0 26.3 57.7 55.0 54.8 40.6 47.0 56.8

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Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concen I- [%]	Cr-EDTA
7	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	1.025	91 67 49 28 59 38 23 55 81 75 47 73 79 62 17 36 55	$\begin{array}{c} 0.43\\ 0.41\\ 0.42\\ 0.42\\ 0.42\\ 0.43\\ 0.42\\ 0.44\\ 0.42\\ 0.44\\ 0.42\\ 0.40\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.42\\ \end{array}$	26.5 29.1 28.5 21.0 30.5 32.2 20.1 31.4 29.7 29.5 22.8 26.1 36.0 30.0 24.5 23.4 23.4	28.0 33.5 32.9 25.4 34.9 36.8 23.8 34.8 34.8 34.0 32.3 24.1 27.7 34.1 33.8 27.6 24.8 23.1	56.2 57.2 54.8 50.1 62.7 60.8 45.2 62.3 60.4 57.6 51.3 57.2 65.5 58.8 52.8 49.7 49.8
8	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	1.075	100 77 53 33 15 92 66 44 66 38 90 67 43 21 36	0.45 0.48 0.46 0.48 0.44 0.46 0.45 0.45 0.45 0.45 0.44 0.46 0.45 0.45 0.45 0.45 0.44 0.46 0.45 0.44	28.1 30.9 27.9 17.0 19.9 29.2 30.0 27.7 29.2 26.3 41.0 37.3 20.9 27.9 12.2	30.0 35.1 32.3 20.0 21.7 31.5 34.0 31.6 33.3 29.6 32.9 28.4 24.6 30.9 15.0	64.8 63.5 61.8 38.0 46.6 64.2 60.4 57.4 61.1 60.0 66.9 59.6 51.1 58.5 34.0
9	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	1.225	100 79 59 39 19 88 62 36 18 31 57 85 61 80 40 82 60 40 19	$\begin{array}{c} 0.43\\ 0.48\\ 0.48\\ 0.44\\ 0.43\\ 0.45\\ 0.44\\ 0.42\\ 0.42\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.42\\ 0.42\\ 0.42\\ 0.42\\ 0.42\\ 0.42\\ 0.43\\ 0.43\\ 0.43\\ 0.43\\ 0.43\\ 0.51\\ 0.47\end{array}$	25.4 28.7 28.1 27.9 28.8 28.4 28.2 25.6 27.2 24.9 30.0 33.8 25.2 29.3 27.8 26.6 30.2 25.3 21.2	$\begin{array}{c} 24.1\\ 31.8\\ 31.2\\ 32.6\\ \hline \\ \\ \hline \\ 33.7\\ 29.0\\ 30.6\\ 28.9\\ 33.7\\ 34.6\\ 29.3\\ 30.9\\ 32.0\\ 29.3\\ 30.9\\ 32.0\\ 29.3\\ 33.1\\ 26.2\\ 23.6\\ \end{array}$	53.4 58.4 54.8 55.1 57.3 62.9 56.7 54.1 57.1 52.7 59.6 71.5 54.2 64.6 62.3 57.7 64.7 53.1 47.6

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	Cr-EDTA [%]
10	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	1.275	98 75 54 33 12 87 67 46 26 83 65 46 83 65 46 88 65 46 88 52 34 19 86 72 53	$\begin{array}{c} 0.37\\ 0.40\\ 0.42\\ 0.44\\ 0.43\\ 0.39\\ 0.46\\ 0.46\\ 0.46\\ 0.46\\ 0.46\\ 0.46\\ 0.42\\ 0.46\\ 0.44\\ 0.41\\ 0.40\\ 0.41\\ 0.41\\ 0.41\\ 0.41\\ 0.42\\ 0.44\\ 0.41\\ 0.42\\ 0.44\\ 0.41\\ 0.42\\ 0.44\\ 0.41\\ 0.42\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\ 0.44\\$	29.6 33.1 33.5 29.2 31.1 31.0 31.4 33.1 31.6 30.6 28.9 27.4 32.6 35.0 29.4 31.3 35.0 29.4 31.3 33.9 21.5 33.8 34.0	$\begin{array}{c} 28.9\\ 35.4\\ 35.7\\ 33.1\\ 32.4\\ 32.5\\ 34.0\\ 35.2\\ 34.2\\ 31.7\\ 32.0\\ 32.0\\ 32.0\\ 31.0\\ 32.0\\ 31.0\\ 32.0\\ 31.0\\ 34.4\\ 35.0\\ 37.2\\ 21.4\\ 34.0\\ 33.4\end{array}$	60.4 66.1 65.7 57.0 61.9 60.4 63.5 68.7 64.7 58.8 62.4 60.8 61.6 68.7 60.8 61.6 68.7 60.9 45.0 66.8 65.0
11	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	1.325	100 78 60 33 13 89 78 64 42 52 90 79 53 30 58	0.48 0.47 0.49 0.48 0.48 0.48 0.48 0.48 0.48 0.46 0.45 0.50 0.47 0.51 0.41 0.50 0.48	32.5 32.0 31.4 31.2 22.7 27.2 25.9 23.9 29.1 32.7 32.2 24.8 22.0 25.4 28.9	$\begin{array}{c} 2 \ 3 \ . \ 2 \\ 3 \ 2 \ . \ 6 \\ 3 \ 4 \ . \ 0 \\ 3 \ 5 \ . \ 6 \\ 2 \ 6 \ . \ 4 \\ 2 \ 9 \ . \ 0 \\ 2 \ 9 \ . \ 0 \\ 2 \ 7 \ . \ 6 \\ 3 \ 3 \ . \ 7 \\ 3 \ 6 \ . \ 4 \\ 2 \ 8 \ . \ 1 \\ 2 \ 3 \ . \ 4 \\ 2 \ 4 \ . \ 3 \\ 2 \ 9 \ . \ 8 \\ 3 \ 0 \ . \ 5 \end{array}$	57.7 67.6 65.5 65.2 52.0 61.0 59.4 57.3 61.4 69.3 68.5 57.7 57.5 61.6 66.6

lable AJ.1 Continue	Т	able	A5.1	cont	inue	1
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Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	ntration Cr-EDTA [%]
12	1 2 3 4 5 6 7 8 9 10 11 12	1.475	97 75 52 29 11 88 78 58 36 64 47 26	0.38 0.34 0.32 0.34 0.33 0.36 0.36 0.36 0.33 0.32 0.34 0.32 0.31	39.7 38.4 40.0 36.8 21.3 34.0 26.2 28.5 34.8 39.4 43.0 36.7	29.1 37.8 35.3 32.4 20.4 28.4 23.2 27.8 28.9 36.0 36.3 34.3	61.7 70.7 68.8 69.1 49.0 64.7 57.0 58.1 61.9 69.0 75.0 67.8
	13 14 15 16 17 18 19 20		86 76 66 54 46 29 42 19	0.32 0.34 0.33 0.32 0.36 0.33 0.33 0.33 0.32	37.4 33.4 37.9 32.6 37.3 33.1 22.2 23.5	31.3 30.1 38.2 31.8 39.0 36.0 23.2 25.8	67.9 63.3 66.3 66.4 66.2 62.6 48.2 53.3
13	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	1.525	100 74 53 27 85 61 58 39 38 17 88 68 47 70 86 13 30 56	$\begin{array}{c} 0.33\\ 0.35\\ 0.35\\ 0.31\\ 0.34\\ 0.35\\ 0.32\\ 0.30\\ 0.30\\ 0.27\\ 0.32\\ 0.31\\ 0.28\\ 0.31\\ 0.28\\ 0.31\\ 0.32\\ 0.31\\ 0.32\\ 0.31\\ 0.32\\ 0.31\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\ 0.30\\$	24.5 32.7 36.0 39.4 27.5 33.4 34.4 38.5 35.8 23.0 35.2 37.7 39.6 34.8 31.4 25.2 24.1 27.3	30.2 31.6 50.8 54.3 31.1 36.6 37.7 44.1 50.8 29.1 33.6 34.4 36.2 35.0 28.5 26.0 28.1 31.7	56.1 67.6 68.7 73.6 57.8 68.2 70.2 70.7 70.5 53.6 68.8 71.8 75.3 69.0 62.9 55.5 56.2 58.9

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Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	conce: I- [%]	ntration Cr-EDTA [%]
14	1 2 3 4 5 6 7 8 9 10 11 2 13 14 15 16 17 18 19	1.675	97 77 61 42 20 84 65 84 42 63 48 19 88 66 47 83 66 32 14	$\begin{array}{c} 0.31\\ 0.30\\ 0.32\\ 0.32\\ 0.32\\ 0.33\\ 0.32\\ 0.33\\ 0.34\\ 0.32\\ 0.32\\ 0.31\\ 0.30\\ 0.28\\ 0.31\\ 0.30\\ 0.28\\ 0.31\\ 0.30\\ 0.28\\ 0.31\\ 0.30\\ 0.31\\ \end{array}$	$\begin{array}{c} 21.0\\ 30.3\\ 29.0\\ 33.6\\ 32.6\\ 26.1\\ 30.1\\ 24.3\\ 32.4\\ 28.5\\ 29.5\\ 30.0\\ 26.7\\ 29.9\\ 33.0\\ 27.1\\ 28.2\\ 30.5\\ 34.1\\ \end{array}$	19.9 31.1 29.0 32.4 30.7 24.1 28.7 24.5 34.0 30.7 30.8 34.6 28.4 32.5 36.4 27.3 30.6 33.5 36.3	$\begin{array}{c} 48.8\\ 62.8\\ 56.6\\ 62.9\\ 62.3\\ 56.9\\ 60.5\\ 50.8\\ 62.5\\ 50.8\\ 62.5\\ 58.5\\ 60.0\\ 58.4\\ 61.9\\ 64.8\\ 67.2\\ 58.0\\ 63.6\\ 67.1\\ 68.0 \end{array}$
15	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	1.725	98 76 53 35 16 88 67 83 63 41 39 89 83 68 48 67 47 27	0.29 0.39 0.33 0.36 0.32 0.33 0.31 0.32 0.33 0.34 0.34 0.34 0.34 0.32 0.31 0.29 0.26 0.27 0.27 0.27	24.2 21.1 28.1 28.1 28.4 28.4 25.4 26.4 24.6 26.8 27.0 30.0 29.9 29.7 37.4 44.2 30.4 33.4	$\begin{array}{c} 2 2 . 0 \\ 2 1 . 5 \\ 3 1 . 3 \\ 3 1 . 2 \\ 3 3 . 2 \\ 2 3 . 8 \\ 2 5 . 9 \\ 2 4 . 7 \\ 2 5 . 9 \\ 2 4 . 7 \\ 2 5 . 9 \\ 2 8 . 8 \\ 3 1 . 0 \\ 2 4 . 8 \\ 3 1 . 0 \\ 2 4 . 8 \\ 3 0 . 7 \\ 3 9 . 1 \\ 3 1 . 6 \\ 3 2 . 9 \\ 3 7 . 7 \end{array}$	47.4 50.4 49.0 52.0 52.2 47.6 53.4 48.5 51.7 56.0 55.2 57.5 66.2 77.7 66.7 68.4 69.4

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	ntration Cr-EDTA [%]
16	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	1.775	97 77 56 32 16 89 65 45 24 77 60 87 75 66 48 62 40	0.34 0.34 0.33 0.32 0.33 0.32 0.36 0.36 0.33 0.33 0.33 0.33 0.33 0.33 0.33 0.31 0.33	27.0 32.2 27.8 31.0 25.4 29.3 28.9 25.6 25.3 31.9 26.8 27.8 35.7 34.0 37.9 29.5 20.0	17.7 24.7 28.9 33.0 30.9 21.0 25.2 27.6 29.3 25.8 19.9 27.6 29.7 37.2 27.6 29.7 37.2 27.6 23.2	37.8 54.4 53.2 59.5 53.6 49.6 53.8 48.0 52.7 56.1 53.9 47.8 63.2 61.0 70.7 61.0 47.0
17	18 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	1.825	22 98 77 53 31 12 80 68 80 46 63 43 22 85 65 76 46 61 42 22	0.33 0.31 0.28 0.31 0.32 0.32 0.32 0.34 0.31 0.32 0.33 0.32 0.33 0.32 0.33 0.33 0.33 0.33 0.32 0.33 0.32 0.33 0.32 0.33 0.32 0.33 0.32 0.32 0.32 0.33 0.32 0.33 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.33 0.32 0.33 0.32 0.33 0.32 0.33 0.32 0.33 0.32 0.33 0.32 0.32 0.33 0.32 0.32 0.33 0.32 0.32 0.33 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.32 0.29 0.30 0.30 0.30 0.32 0.32 0.29 0.30 0.30 0.32 0.30 0.32 0.32 0.32 0.32 0.29 0.30 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.29	29.8 23.1 37.1 25.8 28.0 18.8 23.3 33.0 21.9 25.3 26.0 24.7 21.6 26.7 30.9 28.2 36.2 29.0 27.7 31.2	30.7 14.1 24.9 26.5 29.6 26.1 15.6 25.4 17.1 26.0 22.9 24.7 26.2 16.8 26.4 21.7 35.0 26.8 30.1 31.6	

Table A5.1 continued

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Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	conce I - [%]	ntration Cr-EDTA [%]
18	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	1.975	96 74 53 30 11 90 81 68 50 27 65 42 87 69 53 30 12 67 42	0.28 0.27 0.31 0.25 0.29 0.24 0.24 0.24 0.24 0.28 0.27 0.27 0.26 0.24 0.25 0.26 0.24 0.25 0.26 0.22 0.22 0.22 0.22 0.24 0.27 0.27	$\begin{array}{c} 23.1\\ 37.6\\ 26.9\\ 25.9\\ 19.2\\ 23.5\\ 24.0\\ 24.1\\ 26.4\\ 22.3\\ 35.4\\ 30.4\\ 36.8\\ 27.4\\ 20.6\\ 22.8\\ 21.6\\ 35.5\\ 26.3\\ \end{array}$	12.5 24.0 24.6 27.6 22.9 14.3 16.0 18.9 24.6 24.3 28.5 29.9 18.2 19.7 23.1 29.0 27.0 26.4 26.9	20.2 63.3 58.6 58.9 46.6 34.1 45.0 52.5 59.4 55.6 74.3 68.8 38.4 57.2 55.4 59.3 54.4 65.4 60.5
19	$ \begin{array}{r} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 19 \\ \end{array} $	2.025	96 74 53 30 10 90 76 60 39 17 65 44 88 73 50 29 11 65 42	0.26 0.26 0.26 0.24 0.26 0.26 0.26 0.24 0.27 0.26 0.23 0.26 0.23 0.26 0.23 0.26 0.25 0.25 0.25 0.25 0.24 0.25 0.22 0.25 0.22	22.7 35.7 36.7 36.1 15.9 28.0 27.8 24.1 27.7 24.2 35.0 36.9 35.2 37.2 23.9 20.2 20.6 45.4 37.3	13.5 24.9 34.0 37.7 22.6 19.1 24.3 26.1 29.7 31.0 29.0 36.5 18.2 19.3 23.2 24.0 25.7 30.9 35.8	16.8 60.0 88.4 77.7 46.0 36.0 54.4 54.3 62.0 63.6 67.2 76.5 30.9 45.3 54.9 49.6 54.4 78.7 74.4

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	conce I- [%]	ntration Cr-EDTA [%]
20	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	2.175	100 78 58 33 12 86 76 57 26 16 64 45 94 80 63 41 18 69 42	0.20 0.20 0.20 0.21 0.20 0.21 0.20 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19	$ \begin{array}{c} 16.5\\ 42.8\\ 54.8\\ 50.4\\ 32.1\\ 29.2\\ 27.4\\ 34.5\\ 43.0\\ 35.0\\ 46.2\\ 54.4\\ 40.4\\ 44.2\\ 37.2\\ 31.2\\ 40.6\\ 59.0\\ 50.2\\ \end{array} $	14.4 33.9 50.2 48.2 38.0 24.3 26.0 31.8 39.6 40.1 43.1 50.2 25.9 30.8 35.2 34.3 41.9 46.9 49.7	40.0 86.8 109.25 98.2 67.3 67.5 63.0 76.8 92.0 77.4 95.0 113.0 75.9 86.2 77.6 66.7 83.5 109.9 100.5
21	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	2.225	93 71 49 29 12 92 82 68 55 30 88 55 30 88 52 86 74 74 38 16 65 42	0.18 0.20 0.20 0.20 0.18 0.18 0.18 0.18 0.19 0.17 0.18 0.17 0.18 0.15 0.19 0.19 0.19 0.21 	$\begin{array}{c} 46.0\\ 43.2\\ 41.8\\ 41.2\\ 47.4\\ 49.6\\ 45.1\\ 39.8\\ 47.5\\ 44.8\\ 62.2\\ 48.0\\ 52.9\\ 46.2\\ -\\ 34.3\\ 42.2\\ 40.7\\ 45.6 \end{array}$	29.5 36.5 42.2 42.0 51.2 31.5 35.8 34.9 43.2 43.3 48.7 43.6 34.0 35.3 - 38.6 42.5 35.0 43.8	90.0 95.0 87.4 87.0 100.3 92.5 92.9 82.5 96.8 91.0 124.6 93.8 96.0 95.3 - 72.7 84.9 83.5 93.9

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Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	conce I ⁻ [%]	ntration Cr-EDTA [%]
22	1 2 3 4 5 6 7 8 9 10 11 12 13 14	2.275	97 75 30 71 73 90 50 68 31 92 50 14 63 38	0.28 0.32 0.26 0.30 0.25 0.29 0.29 0.29 0.27 0.26 0.28 0.28 0.29 0.25 0.25 0.27 0.25 0.27	26.7 26.6 30.9 39.8 43.8 30.9 34.1 31.9 33.7 29.5 35.6 33.5 26.5 26.0	$ \begin{array}{r} 1 9 . 0 \\ 2 4 . 3 \\ 3 5 . 3 \\ 3 6 . 8 \\ 3 8 . 2 \\ 2 7 . 4 \\ 3 4 . 8 \\ 2 8 . 9 \\ 3 4 . 9 \\ 2 2 . 0 \\ 3 4 . 5 \\ 3 6 . 0 \\ 2 3 . 5 \\ 2 7 . 3 \\ \end{array} $	52.0 53.7 62.4 79.0 81.1 62.4 68.4 64.1 66.1 59.0 74.6 56.4 57.8 56.1
	15 16 17		40 63 83	0.26 0.28 0.30	24.2 31.5 31.9	26.5 25.9 21.0	53.6 59.0 52.6
23	$ \begin{array}{c} 1\\2\\3\\4\\5\\6\\7\\8\\9\\10\\11\\12\\13\\14\\15\\16\\17\\18\\19\\20\\21\\22\end{array} $	2.375	99 79 61 40 15 90 69 86 66 49 32 51 13 35 90 69 82 67 18 43 30 50	0.17 0.18 0.20 0.22 0.17 0.20 0.18 0.19 0.21 0.22 0.17 0.22 0.17 0.22 0.22 0.25 0.24 0.24 0.24 0.27 0.26 0.27 0.25 0.26	35.3 57.4 60.1 70.9 57.7 37.7 56.2 35.7 45.6 53.7 45.6 53.7 49.0 53.9 47.4 32.9 41.7 52.0 48.8 41.3 45.4 46.7 57.9 47.9	30.9 49.3 57.1 68.5 50.4 36.4 51.4 36.1 43.4 55.9 50.8 53.4 47.4 38.3 35.6 49.5 41.8 41.1 45.5 48.7 57.1 49.5	87.1 112.9 116.8 129.9 106.8 90.0 113.6 83.5 100.8 108.0 97.1 111.3 89.3 75.2 86.4 102.9 96.3 82.8 88.8 94.6 109.7 90.6

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Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	Cr-EDTA
24	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	2.425	94 70 48 27 11 92 77 58 24 63 89 72 45 20 61	0.30 0.29 0.32 0.28 0.30 0.32 0.30 0.31 0.30 0.31 0.30 0.30 0.30 0.29 0.32 0.28 0.28 0.30	18.317.815.617.120.828.223.923.422.622.240.735.130.428.725.5	18.7 23.9 22.8 22.5 25.0 23.8 23.3 24.1 23.4 26.1 26.5 33.4 31.2 29.6 27.5	46.8 44.4 39.1 43.5 49.4 60.9 52.2 52.2 50.0 54.2 63.8 69.5 62.7 60.5 60.0
2 5 ,	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	2.575	98 80 56 32 12 92 81 60 39 18 76 41 94 83 66 46 20 68 40	0.18 0.22 0.20 0.21 0.16 0.17 0.22 0.21 0.19 0.20 0.21 0.20 0.21 0.21 0.21 0.21 0.22 0.21 0.22 0.21 0.22 0.22	$\begin{array}{c} - \\ 47.2 \\ 49.6 \\ 46.0 \\ 32.4 \\ 42.0 \\ 42.5 \\ 43.6 \\ 35.8 \\ 20.8 \\ 43.1 \\ 27.1 \\ 39.6 \\ 44.4 \\ 47.5 \\ 37.2 \\ 37.1 \\ 49.3 \\ 47.2 \end{array}$	$\begin{array}{c} - \\ 47.4 \\ 49.6 \\ 47.1 \\ 33.0 \\ 37.1 \\ 39.2 \\ 37.1 \\ 32.7 \\ 24.0 \\ 40.7 \\ 37.6 \\ 28.8 \\ 38.9 \\ 42.2 \\ 38.8 \\ 38.9 \\ 42.2 \\ 38.3 \\ 36.4 \\ 47.7 \\ 46.6 \end{array}$	$\begin{array}{c} -\\ 117.2\\ 116.1\\ 111.4\\ 77.8\\ 116.9\\ 111.4\\ 101.0\\ 85.5\\ 56.4\\ 105.7\\ 72.0\\ 83.5\\ 111.6\\ 105.9\\ 88.3\\ 84.9\\ 112.4\\ 104.1 \end{array}$
26	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	2.625	97 76 51 29 10 92 83 67 45 22 67 40 91 75 52 25 66	0.18 0.17 0.17 0.16 0.21 0.14 0.14 0.14 0.16 0.13 0.14 0.16 0.13 0.14 0.16 0.13 0.14 0.16 0.13 0.18 0.17 0.18 0.12 0.18	38.6 57.1 65.7 62.9 29.4 95.4 39.2 52.1 72.3 57.9 59.4 78.1 40.3 51.7 38.8 45.6 59.8	30.4 52.7 63.3 63.4 37.1 32.6 39.6 51.5 68.5 51.1 52.5 74.2 32.1 47.2 40.3 53.0 53.7	92.0 126.2 128.0 126.8 79.4 93.1 102.9 113.3 147.3 122.4 126.3 160.0 82.5 110.0 91.0 120.0 129.5

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	conce I- [%]	ntration Cr-EDTA [%]
27	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	2.675	98 79 58 33 12 91 83 67 49 27 67 40 86 78 58 35 16 67 43	0.14 0.12 0.12 0.18 	75.3 66.4 88.5 62.0 71.6 54.4 56.7 52.7 57.9 59.6 46.0 42.0 26.9 26.6 25.3 59.6 66.3	$\begin{array}{c} 27.9\\ 69.1\\ 81.9\\ 61.0\\\\ 47.1\\ 55.3\\ 56.4\\ 47.9\\ 55.9\\ 57.2\\ 36.3\\ 44.2\\ 30.4\\ 29.7\\ 26.8\\ 53.3\\ 61.3\\ \end{array}$	$\begin{array}{c} 65.2\\ 139.0\\ 164.6\\ 118.2\\\\ 104.0\\ 118.1\\ 111.7\\ 104.4\\ 112.3\\ 111.8\\ 93.2\\ 89.3\\ 63.3\\ 67.5\\ 60.0\\ 112.0\\ 127.5\\ \end{array}$
28	$ \begin{array}{c} 1\\2\\3\\4\\5\\6\\7\\8\\9\\10\\11\\12\\13\\14\\15\\16\\17\\18\\19\\20\\21\\22\\3\\24\\25\\26\\27\\28\\9\\30\\31\\32\\33\end{array} $	2.825	$ \begin{array}{r} 1 \\ 0 \\ 8 \\ 6 \\ 3 \\ 1 \\ 9 \\ 9 \\ 3 \\ 8 \\ 1 \\ 9 \\ 7 \\ 7 \\ 5 \\ 6 \\ 2 \\ 5 \\ 1 \\ 8 \\ 6 \\ 7 \\ 7 \\ 5 \\ 2 \\ 5 \\ 1 \\ 8 \\ 6 \\ 7 \\ 7 \\ 9 \\ 7 \\ 4 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 9 \\ 7 \\ 7 \\ 9 \\ 7 \\ 7 \\ 9 \\ 7 \\ 7 \\ 9 \\ 7 \\ 7 \\ 9 \\ 7 \\ 7 \\ 9 \\ 7 \\ 7 \\ 9 \\ 7 \\ 7 \\ 9 \\ 7 \\ 7 \\ 9 \\ 7 \\ 7 \\ 9 \\ 7 \\ 7 \\ 9 \\ 7 \\ 7 \\ 7 \\ 9 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ $	0.19 0.21 0.22 0.18 0.18 0.19 0.17 0.17 0.18 0.21 0.21 0.21 0.21 0.21 0.22 0.22 0.20 0.26 0.20 0.19 0.22 0.20 0.19 0.22 0.22 0.20 0.19 0.22 0.22 0.22 0.22 0.25 0.22 0.22 0.22 0.25 0.20 0.19 0.22 0.25 0.20 0.19 0.22 0.25 0.20 0.21 0.21 0.21 0.24 0.22 0.220 0.25 0.22 0.225 0.220 0.21 0.25 0.20 0.119 0.25 0.20 0.219 0.25 0.20 0.219 0.25 0.20 0.219 0.25 0.20 0.219 0.25 0.20 0.219 0.219 0.25 0.20 0.119 0.25 0.20 0.219 0.210 0.119 0.25 0.20 0.219 0.22 0.210 0.119 0.25 0.20 0.219 0.210 0.219 0.25 0.200 0.219 0.210 0.219 0.25 0.200 0.219 0.210 0.219 0.25 0.200 0.219 0.210 0.219 0.25 0.200 0.210 0.210 0.210 0.210 0.210 0.210 0.210 0.210 0.210 0.210 0.210 0.210 0.210 0.210 0.210 0.210 0.210 0.2110 0.2110 0.2110 0.2110 0.200 0.200 0.200 0.118 0.117 0.114	$\begin{array}{c} 0.8\\ 3.2\\ 12.6\\ 52.2\\ 45.0\\ 1.8\\ 3.0\\ 6.8\\ 2.4\\ 8.0\\ 20.1\\ 44.0\\ 30.0\\ 24.9\\ 8.9\\ 45.2\\ 27.9\\ 31.0\\ 24.9\\ 8.9\\ 45.2\\ 27.9\\ 31.0\\ 23.3\\ 1.1\\ 3.2\\ 1.5\\ 30.2\\ 1.5\\ 30.2\\ 1.5\\ 30.2\\ 1.5\\ 30.2\\ 1.5\\ 30.2\\ 1.5\\ 30.2\\ 1.5\\ 30.5\\ 41.0\\ 55.2\\ 60.5\\ 41.0\\ 51.3\\ \end{array}$	$\begin{array}{c} 4.9\\ 9.6\\ 15.4\\ 46.2\\ 48.2\\ 7.0\\ 8.3\\ 12.2\\ 7.7\\ 13.6\\ 19.9\\ 41.3\\ 35.0\\ 22.3\\ 13.0\\ 42.4\\ 25.1\\ 33.2\\ 25.8\\ 5.1\\ 10.8\\ 7.0\\ 30.5\\ 15.6\\ 11.5\\ 42.4\\ 39.9\\ 38.2\\ 38.1\\ 52.3\\ 50.0\\ 42.1\\ 48.4 \end{array}$	$\begin{array}{c} 0.7\\ 0.7\\ 7.2\\ 82.3\\ 99.7\\ 0.3\\ 1.3\\ 2.2\\ 1.7\\ 5.2\\ 20.2\\ 80.0\\ 73.6\\ 26.5\\ 4.2\\ 99.7\\ 47.3\\ 74.4\\ 60.8\\ 1.0\\ 1.4\\ 50.5\\ 17.6\\ 6.4\\ 87.5\\ 78.3\\ 77.5\\ 89.2\\ 108.4\\ 121.8\\ 89.5\\ 114.2 \end{array}$

Table	A5.1	continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	Cr-EDTA
29	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	2.875	100 78 56 32 10 90 80 70 47 66 45 20 89 77 60 40 18 66 48	0.29 0.30 0.28 0.29 0.32 0.30 0.34 0.31 0.31 0.33 .0.32 0.34 0.33 0.32 0.34 0.33 0.37 0.33 0.37 0.33 0.32 0.32 0.32 0.32 0.34	21.0 41.7 45.7 36.8 27.6 36.8 26.4 37.8 38.8 23.4 25.7 29.9 25.9 30.6 23.2 27.2 34.1 43.6 34.3	15.0 21.8 29.2 27.1 27.1 21.4 17.0 22.5 26.8 17.1 20.0 24.7 17.7 17.7 17.9 19.6 25.5 29.4 24.4 23.2	34.4 49.2 63.7 65.2 46.1 55.9 41.8 50.2 64.5 43.1 54.2 53.7 35.3 32.1 38.9 57.3 65.1 55.3 58.7
30	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	2.925	98 78 57 33 12 88 65 81 43 61 20 41 91 85 71 48 63 26 45	$\begin{array}{c} 0.28\\ 0.28\\ 0.29\\ 0.27\\ 0.28\\ 0.28\\ 0.25\\ 0.26\\ 0.27\\ 0.26\\ 0.27\\ 0.26\\ 0.27\\ 0.26\\ 0.27\\ 0.27\\ 0.27\\ 0.27\\ 0.27\\ 0.27\\ 0.27\\ 0.27\\ 0.29\\ 0.29\\ \end{array}$	33.4 39.3 41.2 46.2 29.7 39.0 46.0 39.0 31.9 30.7 29.8 37.1 40.4 47.5 43.2 45.0 42.0 38.9 41.1	$\begin{array}{c} 26.9\\ 33.6\\ 35.3\\ 43.1\\ 31.0\\ 30.7\\ 38.2\\ 33.1\\ 36.5\\ 34.5\\ 32.4\\ 35.0\\ 31.4\\ 35.0\\ 31.4\\ 38.9\\ 38.0\\ 41.9\\ 38.4\\ 36.7\\ 38.3\\ \end{array}$	70.3 80.4 78.2 100.4 63.3 75.6 84.1 78.8 71.8 68.8 70.1 88.8 77.0 94.7 82.0 86.2 83.5 71.8 83.2
31	1 2 3 4 5 6 7 8 9 10 11 12 13	2.975	63 65 73 48 45 44 51 50 32 23 32 14	0.26 0.26 0.25 0.25 0.28 0.26 0.26 0.26 0.27 0.28 0.30 0.27 0.28 0.27 0.28 0.27	34.9 45.0 42.2 55.1 40.0 36.0 44.1 42.4 39.5 45.8 39.2 40.5 35.5	37.2 46.0 43.8 45.8 42.8 38.8 42.8 38.8 45.3 44.5 40.8 46.8 38.9 41.2 37.4	74.7 82.8 80.4 91.2 81.1 79.2 86.9 83.2 83.9 93.8 78.8 84.7 76.0

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	ntration Cr-EDTA [%]
1 F	1	0 345	162	0.36	27 2	29 1	56 /
1 L	2	0.545	203	0.30	27.2	29.1	10.4 45.8
	3		140	0.35	20.3	20.8	43.2
	4		217	0.41	12.0	16.3	16.6
	5		128	0.36	20.2	26.9	39.4
	6		196	0.36	18.5	16.2	33.3
	7		220	0.35	21.6	20.3	30.5
	8		169	0.36	15.7	15.4	36.8
	9		173	0.39	20.8	25.3	28.9
	10		180	0.36	22.0	22.7	43.2
	11		177	0.36	22.8	22.3	42.9
	12		148	0.38	15.0	26.7	33.4
	13		199	0.42	17.2	17.9	24.0
2 E	1	0.555	159	0.48	27.0	34.4	80.8
	2		206	0.41	24.0	29.8	35.1
	3		141	0.48	21.2	24.5	59.3
	4		214	0.42	22.7	30.9	66.8
	5		132	0.45	26.0	34.0	75.6
	6		193	0.54	21.9	31.2	79.1
	7		174	0.49	23.4	29.0	36.4
	8		232	0.44	23.0	30.0	55.0
	9		1/6	0.47	24.1	32.1	66.4
	10		157	0.48	24.0	31.0	/1.5
			191	0.48	24.3	29.8	/0.6
	12		100	0.47	30.8 26 /	34.0	49.5
	10		197	0.40	20.4	54.0	51.4
3 E	1	0.725	222	0.43	11.9	26.5	0.3
	2		127	0.46	35.3	28.6	65.4
	3		200	0.45	22.0	23.8	30.3
	4		168	0.47	17.5	34.4	12.1
	5		120	0.50	14.0	29.9	1.2
	6		255	0.49	13.1	22.9	12.7
	7		165	0.41	25.2	26.2	50.0
	8		140	0.43	27.2	32.3	17.9
	9		186	0.39	29.0	29.5	48.5
	10		213	0.45	12.9	27.8	6.6
			185	0.42	43.8	26.5	55.2
	12		186	0.46	11.4	31.4	1.7
	13		161	0.44	22.9	32.0	44.5

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Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concen I ⁻ [%]	tration Cr-EDTA [%]
4 E	1 2 3 4 5 6 7 8 9 10 11 12 13	0.775	2 2 6 1 3 4 2 0 2 1 7 0 2 0 1 1 3 5 2 2 5 1 6 2 1 8 1 2 0 3 2 0 2 1 6 2 1 5 7	$\begin{array}{c} 0.48\\ 0.42\\ 0.43\\ 0.42\\ 0.46\\ 0.38\\ 0.48\\ 0.42\\ 0.43\\ 0.43\\ 0.43\\ 0.52\\ 0.40\\ 0.40\\ 0.40\\ \end{array}$	$\begin{array}{c} 9.0\\ 16.8\\ 7.2\\ 13.4\\ 7.2\\ 15.0\\ 3.5\\ 14.5\\ 6.1\\ 4.8\\ 4.0\\ 9.4\\ 14.2 \end{array}$	$\begin{array}{c} 2 \ 3 \ . \ 7 \\ 2 \ 6 \ . \ 1 \\ 2 \ 0 \ . \ 5 \\ 3 \ 2 \ . \ 0 \\ 2 \ 8 \ . \ 9 \\ 2 \ 9 \ . \ 9 \\ 1 \ 7 \ . \ 2 \\ 2 \ 2 \ . \ 7 \\ 2 \ 5 \ . \ 5 \\ 2 \ 7 \ . \ 0 \\ 1 \ 7 \ . \ 6 \\ 3 \ 3 \ . \ 1 \\ 2 \ 6 \ . \ 7 \end{array}$	0.3 16.4 1.8 17.9 1.3 13.1 0.0 8.7 1.8 0.0 1.6 2.3 7.7
5 E	1 2 3 4 5 6 7 8 9 10 11 12 13	0.825	2 2 4 1 3 2 2 0 0 1 6 6 2 0 1 2 2 0 1 3 8 1 6 5 1 8 1 2 0 0 2 0 0 1 5 6 1 5 7	0.42 0.44 0.42 0.44 0.44 0.44 0.44 0.49 0.44 0.47 0.44 0.47 0.44 0.49 0.41 0.42	23.4 21.3 11.5 19.0 18.7 7.6 17.8 15.6 7.7 7.3 10.3 11.1 16.4	25.7 23.3 19.9 25.5 24.3 19.6 25.8 21.8 22.0 20.2 24.4 24.9 24.3	5.6 51.9 14.9 34.1 18.5 0.7 38.9 26.3 14.6 7.2 1.4 16.8 26.7
6 E	1 2 3 4 5 6 7 8 9 10 11	0.915	215 146 221 179 227 186 206 169 143 161 190	0.38 0.40 0.38 0.39 0.42 0.38 0.41 0.40 0.40 0.40 0.39 0.40	$5.9 \\ 17.2 \\ 14.5 \\ 7.9 \\ 2.4 \\ 16.3 \\ 7.1 \\ 12.1 \\ 17.6 \\ 8.2 \\ 4.6 \\ \end{cases}$	12.419.313.718.95.217.314.116.719.614.712.4	$\begin{array}{c} 0.4\\ 13.7\\ 5.4\\ 1.0\\ 0.8\\ 5.7\\ 2.0\\ 4.3\\ 24.3\\ 5.1\\ 0.4 \end{array}$
7 E	1 2 3 4 5 6 7 8 9 10 11 12 13	0.965	215 146 215 223 185 179 205 193 153 187 144 149 167	0.43 0.40 0.41 0.43 0.40 0.39 0.41 0.39 0.37 0.39 0.37 0.39 0.36 0.41 0.40	$\begin{array}{c} 6.6\\ 18.1\\ 5.2\\ 1.3\\ 11.0\\ 8.8\\ 2.5\\ 9.4\\ 15.8\\ 11.8\\ 24.9\\ 18.5\\ 24.1 \end{array}$	13.822.210.74.614.918.29.616.419.213.422.417.217.0	$\begin{array}{c} 0.3\\ 20.7\\ 0.3\\ 0.1\\ 4.4\\ 3.4\\ 0.0\\ 1.5\\ 13.8\\ 0.2\\ 11.4\\ 12.4\\ 14.9 \end{array}$

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	conce I - [%]	ntration Cr-EDTA [%]
8 E	1 2 3 4 5 6 7 8 9 10 11 12 13	1.115	215 139 146 130 182 156 179 173 215 223 182. 199 196	$\begin{array}{c} 0.40\\ 0.44\\ 0.48\\ 0.44\\ 0.46\\ 0.44\\ 0.43\\ 0.42\\ 0.42\\ 0.42\\ 0.42\\ 0.42\\ 0.42\\ 0.45\\ 0.43\end{array}$	9.1 19.0 27.5 23.2 23.9 18.8 17.8 23.1 19.2 13.2 20.0 15.9 21.8	6.6 22.0 19.7 23.3 16.6 24.3 19.5 17.8 11.6 10.3 14.9 13.2 14.3	5.2 32.8 54.0 9.3 15.6 24.4 8.4 56.7 16.0 9.6 42.6 24.4 37.6
9 E	1 2 3 4 5 6 7 8 9 10 11 12 13	1.265	213 150 216 140 224 178 187 132 182 208 191 171 154	0.33 0.41 0.38 0.36 0.35 0.30 0.38 0.36 0.35 0.35 0.35 0.35 0.35 0.32 0.32 0.36	$\begin{array}{c} 3 & . \\ 5 & . \\ 4 \\ 2 \\ 8 & . \\ 0 \\ 2 \\ 6 & . \\ 6 \\ 1 \\ 5 & . \\ 0 \\ 1 \\ 3 & . \\ 1 \\ 1 \\ . \\ 7 \\ 1 \\ 3 & . \\ 1 \\ 5 & . \\ 4 \\ 1 \\ 2 & . \\ 1 \\ 9 & . \\ 1 \\ 5 & . \\ 7 \\ 1 \\ 0 & . \\ 9 \end{array}$	13.68.714.716.311.617.99.711.913.014.011.212.713.2	$ \begin{array}{c} 1 . 2 \\ 0 . 0 \\ 55 . 2 \\ 15 . 0 \\ 33 . 2 \\ 0 . 5 \\ 27 . 6 \\ 3 . 3 \\ 0 . 9 \\ 27 . 2 \\ 8 . 0 \\ 2 . 5 \\ 0 . 9 \\ \end{array} $
10E	1 2 3 4 5 6 7 8 9 10 11 12 13	1.315	213 146 214 148 225 181 185 131 183 207 168 188 155	0.46 0.38 0.40 0.42 0.44 0.48 0.43 0.39 0.43 0.39 0.43 0.38 0.41 0.41 0.36	$\begin{array}{c} 6 & . & 2 \\ 0 & . & 6 \\ 2 & 1 & . & 6 \\ 2 & 3 & . & 0 \\ 5 & . & 4 \\ 1 & 4 & . & 6 \\ 7 & . & 8 \\ 4 & . & 3 \\ 2 & . & 9 \\ 6 & . & 2 \\ 1 & . & 1 \\ 8 & . & 9 \\ 3 & . & 6 \end{array}$	$\begin{array}{c} 9.0\\ 6.4\\ 10.4\\ 15.5\\ 8.9\\ 11.7\\ 6.2\\ 13.1\\ 9.8\\ 10.5\\ 6.3\\ 11.4\\ 12.9 \end{array}$	4.0 0.1 46.9 2.0 12.9 1.0 19.9 0.0 0.0 11.8 0.7 0.5 0.0

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	ntration Cr-EDTA [%]
11E	1 2 3 4 5 6 7 8 9 10 11 12 13	1.415	159 204 137 221 134 195 224 168 170 146 176 201 198	0.42 0.38 0.41 0.38 0.43 0.39 0.37 0.39 0.41 0.41 0.41 0.40 0.39 0.39 0.39	$\begin{array}{c} 0.4\\ 26.4\\ 27.6\\ 0.9\\ 5.3\\ 0.4\\ 8.6\\ 33.8\\ 10.7\\ 20.0\\ 1.1\\ 5.0\\ 24.9 \end{array}$	3.6 13.9 15.0 4.6 8.0 4.1 7.4 20.0 11.2 13.3 5.7 9.5 18.4	$\begin{array}{c} 0 & . & 0 \\ 2 & 0 & . & 6 \\ 2 & 0 & . & 1 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 2 \\ 0 & . & 2 \\ 4 & 3 & . & 8 \\ 0 & . & 4 \\ 0 & . & 7 \\ 0 & . & 1 \\ 0 & . & 1 \\ 8 & . & 0 \end{array}$
12E	1 2 3 4 5 6 7 8 9 10 11 12 13	1.565	161 206 135 215 194 130 167 222 173 151 158 191 197	0.38 0.38 0.38 0.41 0.37 0.39 0.38 0.39 0.38 0.39 0.38 0.42 0.45 0.43	$ \begin{array}{c} 1 . 2 \\ 1 6 . 1 \\ 2 0 . 3 \\ 1 . 6 \\ 0 . 7 \\ 1 . 1 \\ 3 3 . 0 \\ 3 . 1 \\ 1 0 . 0 \\ 4 . 0 \\ 8 . 6 \\ 3 . 5 \\ 1 1 . 4 \end{array} $	$\begin{array}{c} 2 \\ . \\ 5 \\ 11 \\ . \\ 3 \\ . \\ 0 \\ 2 \\ . \\ 9 \\ 1 \\ . \\ 6 \\ 5 \\ . \\ 7 \\ 16 \\ . \\ 7 \\ 5 \\ . \\ 2 \\ 6 \\ . \\ 9 \\ 5 \\ . \\ 2 \\ 11 \\ . \\ 0 \\ 3 \\ . \\ 4 \\ 10 \\ . \\ 2 \end{array}$	$\begin{array}{c} 0 & . & 0 \\ 1 & . & 4 \\ 0 & . & 2 \\ 0 & . & 2 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 8 & . & 9 \\ 0 & . & 2 \\ 8 & . & 0 \\ 1 & . & 7 \\ 0 & . & 4 \\ 0 & . & 3 \\ 7 & . & 3 \end{array}$
13E	1 2 3 4 5 6 7 8 9 10 11 12	1.615	221 131 203 169 222 200 164 178 181 208 179 158	0.41 0.40 0.42 0.42 0.44 0.37 0.36 0.36 0.37 0.37 0.37 0.37 0.35 0.36	0.4 9.4 17.6 0.2 2.5 0.6 26.9 3.6 0.8 1.5 18.4 10.6	$\begin{array}{c} 2 & . & 9 \\ 7 & . & 8 \\ 1 & 2 & . & 1 \\ 2 & . & 1 \\ 5 & . & 8 \\ 2 & . & 4 \\ 1 & 8 & . & 1 \\ 8 & . & 9 \\ 4 & . & 3 \\ 6 & . & 4 \\ 1 & 6 & . & 0 \\ 1 & 1 & . & 8 \end{array}$	$\begin{array}{c} 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 8 \\ 0 & . & 0 \\ 0 & . & 1 \\ 0 & . & 1 \\ 5 & . & 3 \\ 0 & . & 2 \\ 0 & . & 0 \\ 0 & . & 1 \\ 0 & . & 3 \\ 0 & . & 3 \end{array}$
14E	1 2 3 4 5 6 7 8 9 10 11 12	1.775	205 155 219 143 178 174 226 130 192 186 151 210	0.35 0.36 0.37 0.36 0.35 0.32 0.34 0.34 0.34 0.36 0.36 0.35 0.38	0.0 0.5 0.0 4.6 0.2 0.2 0.0 8.6 0.0 0.0 6.0 0.0	$\begin{array}{c} 0.7\\ 1.9\\ 0.5\\ 4.5\\ 3.0\\ 2.4\\ 0.3\\ 5.3\\ 1.0\\ 2.0\\ 8.0\\ 0.9\end{array}$	$\begin{array}{c} 0 & . & 0 \\ 0 & . & 1 \\ 0 & . & 2 \\ 0 & . & 1 \\ 0 & . & 1 \\ 0 & . & 2 \\ 0 & . & 2 \\ 0 & . & 1 \\ 0 & . & 2 \\ 0 & . & 4 \\ 0 & . & 1 \\ 0 & . & 2 \end{array}$

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	ntration Cr-EDTA [%]
15E	1 2 3 4 5 6 7 8 9 10 11 12 13	1.825	205 157 140 221 173 221 195 130 178 166 202 194 158	0.37 0.39 0.40 0.40 0.38 0.47 0.42 0.38 0.42 0.38 0.42 0.41 0.43 0.39 0.36	0.0 0.4 3.8 0.0 0.1 0.0 0.0 6.8 0.1 0.4 0.0 0.0 1.2	0,4 2.0 3.8 0.3 1.5 0.2 0.8 4.2 1.4 2.5 0.5 0.8 3.3	0.2 0.0 0.1 0.1 0.1 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2 0.2
16E	1 2 3 4 5 6 7 8 9 10 11 12 13	1.875	215 146 214 147 179 183 227 184 131 193 205 168 151	$\begin{array}{c} 0.41 \\ 0.39 \\ 0.39 \\ 0.43 \\ 0.42 \\ 0.41 \\ 0.44 \\ 0.41 \\ 0.39 \\ 0.42 \\ 0.40 \\ 0.41 \\ 0.41 \\ 0.43 \end{array}$	0.0 0.2 2.5 0.0 0.0 0.0 0.0 3.5 0.0 0.0 0.5 0.9 0.0	$\begin{array}{c} 0 \ . \ 2 \\ 1 \ . \ 4 \\ 3 \ . \ 3 \\ 0 \ . \ 3 \\ 1 \ . \ 4 \\ 0 \ . \ 1 \\ 0 \ . \ 7 \\ 3 \ . \ 3 \\ 0 \ . \ 6 \\ 0 \ . \ 3 \\ 3 \ . \ 5 \\ 3 \ . \ 5 \\ 0 \ . \ 8 \end{array}$	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \end{array}$
17E	1 2 3 4 5 6 7 8 9 10 11 12 13	2.025	206 161 220 135 179 174 225 194 135 186 154 206 174	0.32 0.36 0.35 0.34 0.38 0.35 0.36 0.36 0.36 0.36 0.36 0.36 0.36 0.36	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \end{array}$	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 3 \\ 0 \ . \ 0 \\ 2 \ . \ 6 \\ 0 \ . \ 5 \\ 0 \ . \ 5 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 2 \ . \ 1 \\ 0 \ . \ 4 \\ 2 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 5 \end{array}$	$\begin{array}{c} 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 2 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 1 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \end{array}$

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Table A5.1 continued

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Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I - [%]	ntration Cr-EDTA [%]
18E	1 2 3 4 5 6 7 8 9 10 11 12 13	2.075	212 151 145 216 186 225 133 186 181 192 207 152 171	0.35 0.38 0.38 0.34 0.36 0.34 0.38 0.35 0.34 0.35 0.34 0.33 0.34 0.35	$\begin{array}{c} 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 5 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \end{array}$	0.1 0.6 0.0 2.7 0.1 0.7 0.2 2.7 0.7 0.2 2.7 0.7 0.2 1.7 0.2	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \ . \ 0 \\ 0 \ . \ 0 \ . \ 0 \\ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \$
19E	1 2 3 4 5 6 7 8 9 10 11 12 13	2.225	205 157 141 220 225 172 131 191 177 204 165 192 158	0.38 0.36 0.33 0.35 0.38 0.33 0.32 0.35 0.35 0.36 0.37 0.32 0.32 0.32 0.33	$\begin{array}{c} 0 & . & 0 \\ 0 & . & 3 \\ 9 & . & 1 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 3 \\ 6 & . & 0 \\ 0 & . & 3 \\ 6 & . & 0 \\ 0 & . & 0 \\ 1 & . & 6 \\ 0 & . & 0 \\ 1 & . & 6 \\ 0 & . & 0 \\ 3 & . & 1 \end{array}$	0.5 1.9 7.3 0.6 0.3 2.3 5.2 0.9 4.2 1.0 6.1 1.9 7.3	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \ . \ 0 \\ 0 \ . \ 0 \ . \ 0 \\ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \ 0 \ . \$
20E	1 2 3 4 5 6 7 8 9 10 11 12 13	2.275	207 158 140 216 172 222 192 123 177 146 186 201 173	0.50 0.31 0.30 0.33 0.33 0.32 0.32 0.32 0.32 0.32	$\begin{array}{c} 0 & . & 0 \\ 1 & . & 8 \\ 1 & 7 & . & 6 \\ 0 & . & 0 \\ 0 & . & 5 \\ 0 & . & 0 \\ 0 & . & 0 \\ 1 & 7 & . & 2 \\ 0 & . & 3 \\ 4 & . & 3 \\ 0 & . & 3 \\ 0 & . & 3 \\ 0 & . & 0 \\ 0 & . & 4 \end{array}$	$ \begin{array}{r} 1.0\\ 4.5\\ 9.0\\ 1.5\\ 4.2\\ 0.9\\ 1.7\\ 9.4\\ 3.1\\ 7.6\\ 4.7\\ 1.8\\ 4.1\\ \end{array} $	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 1 \ . \ 5 \\ 0 \ . \ 2 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 2 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 2 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \end{array}$

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	ntration Cr-EDTA [%]
21E	1 2 3 4 5 6 7 8 9 10 11 12 13	2.325	157 203 133 220 171 131 194 164 223 144 179 172 204	0.34 0.31 0.32 0.33 0.35 0.34 0.32 0.34 0.35 0.35 0.35 0.35 0.36 0.34 0.31	0.0 2.0 22.7 0.0 1.2 1.9 0.0 27.8 0.0 27.8 0.0 4.7 5.8 0.1 0.1	$\begin{array}{c} 2 & . \\ 4 & . \\ 5 \\ 10 & . \\ 7 \\ 3 & . \\ 1 \\ 6 & . \\ 1 \\ 5 & . \\ 8 \\ 2 & . \\ 0 \\ 2 & . \\ 8 \\ 2 & . \\ 0 \\ 8 & . \\ 0 \\ 10 & . \\ 3 \\ 4 & . \\ 0 \\ 2 & . \\ 9 \end{array}$	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 8 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 4 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \end{array}$
22E	1 2 3 4 5 6 7 8 9 10 11 12 13	2.375	208 163 136 222 178 171 225 135 195 162 201 195 174	0.33 0.34 0.34 0.32 0.33 0.34 0.35 0.34 0.35 0.34 0.34 0.32 0.32 0.32	$\begin{array}{c} 0.1\\ 4.0\\ 28.6\\ 0.0\\ 4.3\\ 6.1\\ 0.0\\ 20.5\\ 0.2\\ 15.8\\ 0.2\\ 0.5\\ 0.5\\ \end{array}$	$\begin{array}{c} 2 & . & 2 \\ 4 & . & 8 \\ 1 & 3 & . & 8 \\ 2 & . & 0 \\ 9 & . & 0 \\ 6 & . & 8 \\ 1 & . & 0 \\ 1 & 1 & . & 2 \\ 2 & . & 5 \\ 1 & 4 & . & 1 \\ 4 & . & 0 \\ 4 & . & 8 \end{array}$	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 1 \ 2 \ . \ 8 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 1 \ . \ 9 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \end{array}$
23E	1 2 3 4 5 6 7 8 9 10 11 12 12	2.505	2 2 1 1 3 0 2 0 3 1 6 5 2 2 2 2 0 2 1 6 4 1 3 5 1 8 0 2 1 1 1 8 2 1 8 2 1 8 2 1 4 8	0.37 0.35 0.34 0.34 0.38 0.38 0.38 0.34 0.35 0.34 0.39 0.36 0.34 0.33	24.0 7.2 23.6 10.4 14.8 17.5 21.0 4.6 30.3 28.1 26.2 34.3 11.0	10.8 7.9 16.3 7.2 12.9 8.0 10.8 5.6 14.8 14.2 11.7 17.6 10.1	37.7 0.0 41.0 0.0 48.0 10.2 2.9 0.0 18.1 57.3 4.8 23.1 0.0

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Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	ntration Cr-EDTA [%]
24E	1 2 3 4 5 6 7 8 9 10 11 12 13	2.555	166 201 133 222 198 135 164 217 174 157 153 199 193	$\begin{array}{c} 0.36\\ 0.36\\ 0.34\\ 0.34\\ 0.35\\ 0.35\\ 0.35\\ 0.36\\ 0.35\\ 0.34\\ 0.36\\ 0.34\\ 0.34\\ 0.33\\ 0.37 \end{array}$	$ \begin{array}{r} 19.6\\ 3.9\\ 12.1\\ 2.3\\ 4.0\\ 13.6\\ 27.5\\ 2.4\\ 18.1\\ 12.7\\ 17.4\\ 7.9\\ 8.8 \end{array} $	12.9 4.5 7.7 4.2 7.6 11.1 11.0 4.4 11.5 10.4 10.6 9.6 7.8	$ \begin{array}{c} 1.5\\ 0.0\\ 25.4\\ 0.1\\ 1.8\\ 16.7\\ 2.0\\ 0.0\\ 9.1\\ 11.1\\ 15.2\\ 1.2\\ 0.1\\ \end{array} $
25E	1 2 3 4 5 6 7 8 9 10 11 12 13	2.705	2 2 0 1 2 9 2 0 0 1 6 5 2 2 2 2 0 2 1 5 8 1 4 0 1 8 0 2 0 7 1 8 2 1 7 8 1 5 0	0.36 0.35 0.38 0.32 0.36 0.34 0.36 0.40 0.35 0.38 0.32 0.38 0.35	$\begin{array}{c} 0 & . & 0 \\ 0 & . & 2 \\ 1 & 6 & . & 1 \\ 0 & . & 0 \\ 1 & 4 & . & 7 \\ 0 & . & 0 \\ 4 & . & 8 \\ 0 & . & 0 \\ 9 & . & 3 \\ 1 & 2 & . & 5 \\ 0 & . & 0 \\ 1 & 7 & . & 4 \\ 1 & . & 5 \end{array}$	0.4 2.7 8.1 0.1 6.4 0.1 7.1 0.5 10.4 7.4 0.3 12.8 5.9	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 1 \\ 1 \ 5 \ . \ 1 \\ 0 \ . \ 0 \\ 1 \ 4 \ . \ 8 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 1 \ . \ 2 \\ 0 \ . \ 0 \\ 1 \ . \ 7 \\ 0 \ . \ 0 \end{array}$
26E	1 2 3 4 5 6 7 8 9 10 11 12 13	2.755	216 146 215 182 225 133 184 183 192 209 156 171	0.32 0.38 0.36 0.34 0.36 0.37 0.36 0.38 0.32 0.34 0.34 0.34 0.37	$\begin{array}{c} 0 & . & 0 \\ 2 & . & 0 \\ 0 & . & 0 \\ 8 & . & 9 \\ 0 & . & 0 \\ 0 & . & 1 \\ 0 & . & 0 \\ 1 & 0 & . & 0 \\ 1 & 8 & . & 0 \\ 0 & . & 2 \\ 0 & . & 0 \\ 1 & 4 & . & 8 \\ 0 & . & 0 \\ 8 & . & 0 \end{array}$	$\begin{array}{c} 0.6 \\ 4.9 \\ 0.2 \\ 10.2 \\ 0.4 \\ 0.9 \\ 0.3 \\ 9.6 \\ 2.0 \\ 0.7 \\ 7.6 \\ 0.5 \\ 12.4 \end{array}$	$\begin{array}{c} 0 \ . \ 2 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 3 \ 3 \ . \ 8 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 3 \ . \ 2 \\ 0 \ . \ 0 \\ 1 \ 3 \ . \ 6 \\ 0 \ . \ 1 \\ 0 \ . \ 5 \end{array}$

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	ntration Cr-EDTA [%]
					an an an an Albert an an Albert an an Albert an Alb	6-16-5-00-00-00-00-00-00-00-00-00-00-00-00-0	
27E	1	2.905	164	0.31	30.3	10.3	17.1
	2		201	0.30	1.6	4.1	0.4
	3		231	0.31	0.6	3.4	0.1
	4		159	0.29	8.1	5.0	20.6
	5		196	0.31	4.0	6.9	0.1
	6		134	0.32	25.0	9.0	50.3
	7		218	0.34	0,8	2.6	0.6
	8		167	0.29	6.9	5.2	1.9
	9		172	0.31	22.3	13.6	3.4
	10		152	0.32	63.0	16.1	53.0
	11		195	0.32	2.8	7.2	0.0
	12		197	0.32	2.0	5.9	0.0
	13		158	0.31	28.5	10.3	12.6
28E	1	2.955	164	0.36	24.5	10.6	27.3
	2		201	0.37	13.1	9.0	4.8
	3		134	0.36	22.3	12.5	47.7
	4		216	0.39	5.6	4.2	4.3
	5		133	0.36	43.5	16.6	79.2
	6		193	0.36	14.7	8.7	11.1
	7		219	0.34	3.7	5.5	3.8
	8		171	0.36	22.6	11.4	24.0
	9		174	0.34	33.0	17.1	23.4
	10		144	0.35	40.3	18.4	67.2
	11		173	0.36	34.6	15.0	18.0
	12		201	0.34	5.4	6.7	7:4
	13		183	0.35	23.3	13.6	14.1

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Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer 1- [%]	cr-EDTA
1 R	1 2 3 4 5	0.075	2 3 6 2 4 6 2 3 0 2 4 7 2 2 5	0.35 0.34 0.34 0.34 0.34 0.43	15.0 9.3 8.9 13.9 8.9	22.0 19.2 22.0 20.1 16.2	8.1 4.7 3.5 9.8 5.6
2 R	1 2 3 4	0.345	236 223 228 246	0.28 0.31 0.30 0.27	14.3 11.9 18.5 14.0	19.6 13.3 16.4 15.5	2.9 9.4 14.4 7.2
3 R	1 2 3 4 5	0.475	236 244 230 249 220	0.31 0.33 0.31 0.35 0.32	0.2 0.3 1.4 0.2 1.4	4.7 3.0 7.4 2.7 9.0	0.0 0.0 0.2 0.5 0.5
4 R	1 2 3 4 5	0.625	2 3 6 2 4 5 2 3 2 2 4 8 2 2 3	0.36 0.34 0.36 0.34 0.38	6.5 3.0 8.8 3.5 14.4	6.4 5.5 6.7 5.0 9.6	0.4 0.3 0.3 0.6 0.4
5 R	1 2 3 4 5	0.775	2 3 7 2 4 3 2 3 1 2 5 3 2 2 3	0.32 0.34 0.32 0.34 0.34 0.33	0.5 0.3 1.1 0.1 1.9	4 . 2 3 . 2 5 . 4 2 . 6 6 . 5	0.1 0.2 0.3 0.4 0.6
6 R	1 2 3 4 5	0.965	2 3 7 2 4 5 2 3 0 2 5 2 2 2 0	0.37 0.52 0.38 0.41 0.34	13.1 7.1 10.6 9.0 16.3	9.2 6.5 7.9 7.1 9.9	0.4 0.0 3.9 0.9 3.1
7 R	1 2 3 4 5	1.015	236 244 230 248 221	0.44 0.42 0.44 0.41 0.44	10.6 11.6 11.2 7.6 15.6	8.7 7.5 9.8 6.7 9.8	7.7 6.6 2.7 3.1 16.8
8 R	1 2 3 4 5	1.065	236 247 231 250 223	0.42 0.42 0.40 0.42 0.43	12.5 14.2 11.1 7.8 15.5	9.7 9.2 11.0 8.0 10.0	8.9 17.4 0.6 2.1 16.6
9 R	1 2 3 4 5	1.185	234 227 243 247 220	0.35 0.36 0.38 0.38 0.38 0.36	15.2 15.6 13.4 11.8 17.9	11.6 13.8 10.8 9.9 13.9	7.1 9.1 4.6 2.8 17.0

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I - [%]	ntration Cr-EDTA [%]
10 R	1 2 3 4 5	1.235	2 3 5 2 3 1 2 4 5 2 5 0 2 2 3	0.39 0.39 0.40 0.38 0.40	3.3 5.2 1.2 2.0 2.5	4.5 9.4 7.0 7.4 6.1	0.0 0.0 0.0 0.0 0.0
11R	1 2 3 4 5	1.285	234 228 244 247 223	0.35 0.34 0.38 0.35 0.37	6.4 8.9 5.2 4.5 6.5	6.0 7.3 5.4 5.5 6.0	0.0 0.1 0.1 0.0 1.0
12R	1 2 3 4 5	1.335	2 3 4 2 2 2 2 4 2 2 4 7 2 2 3	0.36 0.38 0.34 0.36 0.34	7.8 10.9 7.8 4.6 14.3	5.9 6.9 6.6 5.0 8.7	0.0 0.1 0.1 0.0 0.3
13R	1 2 3 4 5	1.385	2 3 5 2 4 4 2 3 6 2 4 8 2 2 2	0.34 0.32 0.32 0.29 0.34	1.8 3.0 0.9 1.2 6.6	3.9 4.0 3.4 3.6 6.9	0.0 0.0 0.1 0.0 0.0
14 R	1 2 3 4	1.435	237 231 221 251	0.31 0.32 0.32 0.28	0.1 1.2 0.1 0.0	1.4 4.3 2.0 1.6	0.1 0.0 0.1 0.0
15R	1 2 3 4 5	1.485	236 247 231 250 221	0.32 0.35 0.31 0.32 0.31	0.0 0.0 0.0 0.0 0.2	0.9 0.9 0.6 0.6 3.5	0.0 0.0 0.0 0.0 0.0
16R	1 2 3 4 5	1.535	2 3 5 2 4 3 2 3 1 2 5 1 2 2 2	0.31 0.33 0.32 0.33 0.31	0.0 0.0 0.0 0.0 0.0	1.1 1.0 0.6 0.4 2.0	0.0 0.0 0.0 0.0 0.0
17R	1 2 3 4 5	1.585	2 3 5 2 4 6 2 3 1 2 4 7 2 2 0	0.30 0.29 0.31 0.31 0.27	0.0 0.0 0.0 0.0 0.0	0.8 0.8 0.5 0.4 1.6	0.0 0.0 0.0 0.0 0.0
18R	1 2 3 4 5	1.635	236 241 231 249 222	0.28 0.31 0.26 0.29 0.27	0.0 0.0 0.0 0.0 0.0	0.7 0.8 0.5 0.3 1.1	0.0 0.0 0.0 0.0 0.0

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer 1- [%]	Cr-EDTA
19R	1 2 3 4 5	1.685	2 3 5 2 2 9 2 4 4 2 4 7 2 2 3	0.30 0.30 0.28 0.30 0.30	0.0 0.0 0.0 0.0 0.0	0.5 0.6 0.4 0.3 0.7	0.0 0.0 0.0 0.0 0.0
20 R	1 2 3 4 5	1.735	236 233 242 249 219	0.29 0.29 0.29 0.29 0.29 0.29	0.0 0.0 0.0 0.0 0.0	0.2 0.2 0.2 0.1 0.4	0.0 0.0 0.0 0.0 0.0
21R	1 2 3 4 5	1.850	2 3 8 2 4 7 2 2 9 2 5 0 2 2 4	0.33 0.29 0.31 0.29 0.33	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \end{array}$	0.6 0.5 0.4 0.2 1.2	0.0 0.0 0.0 0.0 0.0
22 R	1 2 3 4 5	1.900	2 3 5 2 2 7 2 4 2 2 5 1 2 2 4	0.34 0.32 0.33 0.33 0.33 0.35	$\begin{array}{c} 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 1 \end{array}$	0.9 0.8 0.8 0.4 1.5	0.0 0.0 0.0 0.0 0.0
23R	1 2 3 4 5	1.950	2 3 7 2 4 6 2 3 0 2 2 3 2 5 0	0.32 0.33 0.32 0.30 0.30 0.33	0.0 0.0 0.0 0.1 0.0	1.0 0.7 0.7 1.7 0.5	0.0 0.0 0.0 0.0 0.0
24R	1 2 3 4 5	2.000	2 3 7 2 4 4 2 2 9 2 5 0 2 2 1	0.31 0.30 0.29 0.33 0.31	0.0 0.0 0.0 0.0 0.0	0.8 0.7 0.6 0.3 1.2	0.0 0.0 0.0 0.0 0.0
25R	1 2 3 4 5	2.050	2 3 7 2 4 5 2 3 1 2 5 0 2 2 3	0.30 0.31 0.29 0.29 0.29	0.0 0.0 0.0 0.0 0.0	1.1 0.8 1.0 0.6 1.6	0.0 0.0 0.0 0.0 0.0
26 R	1 2 3 4 5	2.100	2 3 6 2 4 7 2 2 9 2 5 0 2 2 4	0.28 0.27 0.30 0.26 0.30	0.0 0.0 0.0 0.0 0.0	1.4 1.1 1.0 0.8 1.8	0.0 0.0 0.0 0.0 0.0
27R	1 2 3 4 5	2.200	2 3 3 2 2 6 2 4 3 2 4 7 2 2 1	0.29 0.30 0.29 0.32 0.30	0.6 0.9 0.3 0.2 1.8	4.3 4.0 3.0 2.9 5.3	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \end{array}$

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	tration Cr-EDTA [%]
28R	1 2 3 4 5	2.250	2 3 6 2 4 5 2 3 0 2 5 0 2 2 4	0.29 0.30 0.29 0.31 0.29	1.2 1.2 0.7 0.3 4.5	5.9 6.0 4.2 3.7 7.1	0.0 0.0 0.0 0.0 0.2
29R	1 2 3 4 5	2.300	2 3 3 2 2 7 2 4 2 2 4 5 2 2 2	0.30 0.34 0.31 0.34 0.34	0.6 0.6 0.3 0.1 2.0	6.1 5.4 5.1 3.3 7.8	0.0 0.2 0.0 0.0 0.2
30 r	1 2 3 4 5	2.350	2 3 3 2 2 8 2 4 1 2 4 6 2 2 2	0.32 0.34 0.31 0.29 0.32	0.6 0.9 0.3 0.5 1.9	5.2 6.5 3.3 4.2 6.1	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 2 \\ 0 \ . \ 1 \end{array}$
31R	1 2 3 4 5	2.450	2 3 6 2 4 4 2 2 9 2 5 0 2 2 3	0.32 0.32 0.31 0.33 0.34	4.7 4.2 5.2 1.4 11.9	7.6 7.1 6.4 4.4 10.1	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 2 \end{array}$
3 2 R	1 2 3 4 5	2.500	2 3 8 2 4 6 2 3 2 2 4 9 2 2 5	0.33 0.30 0.31 0.42 0.34	2 . 8 2 . 3 3 . 5 0 . 8 7 . 8	8.0 7.2 8.4 4.6 11.1	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \end{array}$
33R	1 2 3 4 5	2.550	2 3 8 2 4 8 2 3 1 2 5 0 2 2 4	0.28 0.28 0.28 0.28 0.28 0.28	0.7 0.7 0.5 0.2 3.2	5.4 5.4 5.6 4.0 9.2	0.1 0.0 0.0 0.0 0.0
34 R	1 2 3 4 5	2.600	2 3 8 2 4 5 2 2 9 2 5 1 2 2 4	0.29 0.30 0.30 0.28 0.29	0.3 0.3 0.1 0.0 2.0	4.6 3.8 3.2 2.3 6.9	0.0 0.0 0.0 0.0 0.1
35R	1 2 3 4 5	2.650	2 3 7 2 4 5 2 2 9 2 5 0 2 2 4	0.31 0.30 0.32 0.31 0.33	0.5 0.4 0.2 0.1 1.8	4 . 3 3 . 4 2 . 8 2 . 4 5 . 0	0.0 0.0 0.0 0.1 0.0
36 R	1 2 3 4 5	2.700	2 3 7 2 4 9 2 3 2 2 5 0 2 2 2	0.32 0.30 0.28 0.34 0.30	0.6 0.8 0.4 0.1 2.4	4.9 5.6 6.1 3.1 7.6	0.0 0.0 0.0 0.1 0.2

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Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	ntration Cr-EDTA [%]
37R	1 2 3 4 5	2.800	2 3 7 2 4 5 2 3 0 2 5 3 2 2 6	0.31 0.31 0.35 0.33 0.33	37.8 33.7 39.2 28.2 34.6	20.9 19.0 20.3 12.9 21.1	60.0 54.9 55.4 34.6 58.0
38R	1 2 3 4 5	2.850	2 3 6 2 4 3 2 2 8 2 5 2 2 2 3	0.31 0.30 0.32 0.31 0.32	36.5 29.3 35.9 20.4 38.7	17.8 13.7 15.2 11.1 17.2	32.2 29.2 27.9 13.7 42.3
39R	1 2 3 4 5	2.960	2 3 4 2 2 8 2 4 6 2 5 0 2 2 9	0.31 0.30 0.29 0.30 0.32	2.0 1.1 1.3 0.3 3.2	7.0 5.1 5.7 3.6 6.8	0.0 0.3 0.2 0.0 0.0
40 R	1 2 3 4 5	3.010	2 3 5 2 3 0 2 4 3 2 4 8 2 2 3	0.30 0.29 0.29 0.28 0.30	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \end{array}$	2.5 2.3 2.3 1.6 2.7	0.0 0.0 0.0 0.0 0.0
41R	1 2 3 4 5	3.060	2 3 4 2 3 1 2 4 5 2 4 7 2 2 3	0.29 0.28 0.29 0.26 0.33	0.0 0.0 0.0 0.0 0.0	0.7 0.6 0.5 0.4 0.5	0.0 0.0 0.0 0.0 0.0
42 R	1 2 3 4 5	3.110	236 242 227 247 221	0.30 0.30 0.30 0.30 0.31	0.0 0.0 0.0 0.0 0.0	0.1 0.1 0.1 0.1 0.1	0.0 0.0 0.0 0.0 0.0
43R	1 2 3 4 5	3.220	2 3 8 2 4 7 2 3 2 2 5 0 2 2 2	0.33 0.34 0.29 0.30 0.32	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0

Table A5.1 continued

	Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I~ [%]	ntration Cr-EDTA [%]
	lA	1 2	-0.125	217 209	0.40 0.43	0.1 0.1	2.8 3.2	0.0 0.0
	2 A	1 2 3 4 5	-0.005	215 210 225 228 202	0.39 0.35 0.36 0.36 0.38	11.9 9.0 9.6 6.3 13.2	8.4 7.7 7.0 6.3 6.8	0.0 0.1 0.1 0.0 0.0
	3 A	1 2 3 4 5	0.045	217 208 227 229 202	0.34 0.35 0.38 0.35 0.39	19.3 20.2 19.4 28.2 16.3	13.6 12.7 11.5 9.8 10.5	4.5 5.3 1.6 0.6 22.2
	4 A	1 2 3 4 5	0.175	216 207 224 229 200	0.34 0.33 0.33 0.34 0.32	25.1 21.4 22.6 21.8 24.4	24.8 19.6 19.7 18.0 14.1	48.0 42.6 42.6 42.3 44.1
	5 A	1 2 3 4 5	0.225	2 1 4 2 0 7 2 2 3 2 2 6 1 9 9	0.36 0.38 0.33 0.35 0.32	19.6 23.3 20.3 22.0 20.0	19.4 21.1 19.4 20.4 17.5	37.9 44.9 39.5 40.9 40.0
	6 A	1 2 3 4 5	0.355	2 1 4 2 0 6 2 2 0 2 2 7 2 0 2	0.31 0.36 0.33 0.34 0.36	22.7 23.3 22.9 20.4 21.7	22.6 22.2 20.9 18.4 19.8	44.2 41.2 46.3 43.9 38.9
	7 A	_	0.405	_	_	_		_
	8 A	1 2 3 4 5	0.575	216 207 224 229 205	0.40 0.38 0.38 0.39 0.40	23.1 15.3 18.0 32.4 43.0	18.3 14.3 17.0 16.1 15.5	18.0 37.3 16.5 7.5 39.7
	9 A	1 2 3 4 5	0.625	214 207 223 228 201	0.40 0.39 0.40 0.42 0.40	10.0 12.8 9.3 9.2 15.4	14.4 12.8 13.7 12.2 15.3	0.3 2.4 0.2 0.2 3.3
1	0 A	1 2 3 4 5	0.675	2 1 5 2 1 0 2 2 2 2 2 8 2 0 2	0.37 0.37 0.38 0.38 0.38 0.39	1.6 1.6 1.2 0.5 2.4	8.6 7.9 7.4 5.3 6.9	0.3 0.2 0.2 0.4 0.4

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Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	ntration Cr-EDT/ [%]
11A	1 2 3 4 5	0.725	215 207 226 231 205	0.40 0.38 0.38 0.39 0.39	0.6 1.0 0.2 0.2 0.6	5.1 4.7 3.5 3.3 5.4	0.0 0.0 0.0 0.0 0.0
12A	1 2 3 4 5	0.775	214 209 223 225 201	0.37 0.38 0.37 0.40 0.40	7.0 11.4 3.4 6.4 7.1	7.4 6.9 4.9 6.1 6.1	1.2 9.0 0.1 1.2 1.6
13A	1 2 3 4 5	0.915	214 209 222 229 203	0.36 0.38 0.37 0.36 0.38	20.7 23.4 15.8 20.2 26.0	11.7 11.3 7.6 9.0 13.1	9.4 19.4 1.5 10.1 9.2
14 A	1 2 3 4 5	1.015	216 206 224 227 203	0.38 0.38 0.39 0.42 0.39	23.9 29.6 11.8 21.4 29.1	14.2 12.9 8.2 10.4 14.1	11.1 29.6 0.4 9.4 3.1
15A	1 2 3 4 5	1.115	2 1 3 2 0 6 2 2 1 2 2 5 2 0 0	0.41 0.41 0.42 0.42 0.38	9.7 16.8 3.6 6.4 19.9	10.2 10.9 7.6 8.3 12.5	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 4 \end{array}$
16A	1 2 3 4 5	1.215	2 1 4 2 0 7 2 2 4 2 2 7 2 0 3	0.40 0.39 0.38 0.38 0.38 0.39	1.0 4.1 0.3 1.0 1.3	7.4 8.4 4.1 5.4 6.7	0.0 0.2 0.0 0.1 0.1
17A	1 2 3 4 5	1.345	2 2 0 2 3 3 2 0 7 2 2 4 2 1 4	0.37 0.33 0.37 0.39 0.32	0.8 0.2 1.7 0.2 1.8	3.8 2.5 4.1 2.7 3.8	0.2 0.0 0.3 0.1 0.0
18A	1 2 3 4 5	1.395	215 208 224 229 204	0.32 0.33 0.33 0.32 0.32	0.6 0.1 1.6 0.2 0.8	4.1 2.4 4.3 2.8 3.6	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \end{array}$
19A	1 2 3 4 5	1.445	2 1 5 2 1 0 2 2 2 2 2 8 2 0 5	0.30 0.31 0.31 0.30 0.29	0.0 0.0 0.2 0.0 0.0	2.9 1.7 3.7 2.5 2.3	0.0 0.0 0.0 0.0 0.0

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	ntration Cr-EDTA [%]
20 A	1 2 3 4 5	1.595	218 230 206 225 210	0.30 0.29 0.30 0.29 0.30	0.0 0.0 0.1 0.0 0.0	1.6 0.7 1.8 1.2 1.3	0.0 0.0 0.0 0.0 0.0
21A	1 2 3 4 5	1.645	218 207 223 231 200	0.32 0.30 0.31 0.31 0.31	0.0 0.0 0.1 0.0 0.0	1.8 0.8 1.8 1.0 1.4	0.0 0.0 0.0 0.0 0.0
22 A	1 2 3 4 5	1.745	2 1 4 2 0 7 2 2 6 2 2 7 2 0 3	0.35 0.35 0.36 0.35 0.34	0.0 0.0 0.1 0.0 0.0	1.0 0.5 1.2 0.8 1.1	0.0 0.0 0.0 0.0 0.0
23A	1 2 3 4 5	1.795	216 208 227 227 201	0.36 0.37 0.35 0.32 0.35	0.0 0.0 0.0 0.0 0.0	0.7 0.3 0.6 0.6 0.6	0.0 0.0 0.0 0.0 0.0
24 A	1 2 3 4 5	1.895	216 211 226 227 202	0.31 0.30 0.32 0.31 0.31	0.0 0.0 0.0 0.0 0.0	0.3 0.1 0.4 0.2 0.3	0.0 0.0 0.0 0.0 0.0
25 A	1 2 3 4 5	1.945	2 1 7 2 1 1 2 2 6 2 2 9 2 0 5	0.29 0.30 0.32 0.29 0.30	0.0 0.0 0.0 0.0 0.0 0.0	0.3 0.1 0.3 0.2 0.2	0.0 0.0 0.0 0.0 0.0
26A	1 2 3 4 5	2.195	217 210 226 228 204	0.29 0.28 0.29 0.29 0.29 0.30	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \end{array}$	1.4 0.7 1.4 1.0 1.3	0.0 0.0 0.0 0.0 0.0
27A	1 2 3 4 5	2.280	217 208 224 229 204	0.30 0.32 0.32 0.30 0.30	2.3 0.7 3.7 1.1 1.1	4 . 4 2 . 3 4 . 3 2 . 7 3 . 5	0.1 0.0 0.0 0.1 0.0
28A	1 2 3 4 5	2.330	2 1 5 2 1 2 2 2 4 2 3 0 2 0 3	0.34 0.32 0.34 0.33 0.33	6.7 1.1 17.4 2.6 6.7	5.9 2.9 5.7 3.7 5.4	0.0 0.0 0.3 0.0 0.0

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I - [%]	ntration Cr-EDTA [%]
29A	1 2 3 4 5	2.380	218 231 206 226 212	0.32 0.30 0.33 0.28 0.32	5.7 1.2 10.3 3.4 4.5	7.9 4.8 6.5 6.8 6.5	0.0 0.1 0.2 0.1 0.0
30 A	1 2 3 4 5	2.430	219 231 205 227 210	0.30 0.32 0.30 0.28 0.31	2.0 0.3 7.7 0.9 2.8	8.2 4.2 9.1 6.0 6.7	0.3 0.2 0.0 0.0 0.0
31A	1 2 3 4 5	2.480	2 1 3 2 1 0 2 2 4 2 2 8 2 0 2	0.27 0.32 0.28 0.31 0.31	1.9 0.3 4.0 0.9 3.7	7.7 4.5 8.2 5.6 7.0	0.2 0.0 0.2 0.0 0.1
32A	1 2 3 4 5	2.530	2 1 5 2 0 9 2 2 6 2 2 8 2 0 6	0.32 0.30 0.32 0.29 0.28	1.0 0.4 2.6 0.4 2.3	5.0 2.5 5.6 3.3 6.1	0.0 0.1 0.0 0.0 0.0
33A	1 2 3 4 5	2.680	216 209 226 228 206	0.32 0.35 0.36 0.34 0.32	0.1 0.0 0.3 0.0 0.5	2.8 1.9 3.0 1.8 3.9	0.0 0.0 0.0 0.0 0.0
34A	1 2 3 4 5	2.730	2 1 7 2 1 2 2 2 5 2 3 1 2 0 4	0.32 0.32 0.32 0.31 0.31	0.6 0.1 2.5 0.2 1.7	6.4 3.6 7.9 4.7 7.9	0.2 0.0 0.0 0.0 0.0
3 5 A	1 2 3 4	2.780	2 1 4 2 0 8 2 2 5 2 2 7	0.33 0.33 0.32 0.34	3.5 1.0 9.3 1.0	$ \begin{array}{c} 11.1\\ 6.7\\ 10.6\\ 6.1 \end{array} $	0.0 0.0 0.0 0.0
36A	1 2 3 4 5	2.830	2 1 5 2 1 0 2 2 6 2 2 8 2 0 3	0.33 0.29 0.32 0.31 0.31	4.4 2.6 8.2 1.6 13.3	12.8 10.3 11.6 9.4 17.1	0.0 0.0 0.1 0.0 0.2
37A	1 2 3 4 5	2.880	2 1 7 2 1 1 2 2 4 2 2 9 2 0 3	0.31 0.32 0.31 0.31 0.31	8.6 4.4 12.7 4.5 22.5	13.8 11.3 12.0 10.1 14.9	0.1 0.2 0.8 0.1 1.2

Table	A5.1	continued

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Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I [%]	ntration Cr-EDTA [%]
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38A	1	2.930	220	0.31	12.5	14.8	2.1
	2		231	0.32	3.5	10.9	0.2
	3		206	0.32	24.9	12.4	16.4
	4		224	0.32	6.0	8.8	5.0
	5		208	0.34	19.8	13.4	0.0

Table A5.1 continued

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Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I - [%]	ntration Cr-EDTA [%]
1 X	1 2 3 4 5 6 7 8 9	-0.325	358 272 327 258 317 343 295 282 340	0.39 0.42 0.39 0.41 0.40 0.41 0.40 0.41 0.40 0.43 0.42	$\begin{array}{c} 0 & . & 0 \\ 3 & . & 0 \\ 0 & . & 0 \\ 0 & . & 6 \\ 0 & . & 2 \\ 0 & . & 0 \\ 0 & . & 3 \\ 2 & . & 7 \\ 0 & . & 0 \end{array}$	0.2 1.4 0.3 1.0 0.6 0.2 0.6 1.7 0.4	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 2 \ . \ 8 \\ 0 \ . \ 0 \end{array}$
2 X	1 2 3 4 5 6 7 8 9	-0115	357 273 328 304 311 352 294 334 285	0.34 0.31 0.32 0.36 0.31 0.33 0.37 0.36 0.33	0.7 20.8 0.8 8.7 10.9 0.3 3.6 3.3 25.5	1.1 9.3 2.4 6.7 5.6 1.2 4.4 2.8 11.0	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 6 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 3 \\ 0 \ . \ 8 \end{array}$
3x	1 2 3 4 5 6 7 8 9 10	0.035	3 5 7 2 7 4 3 2 5 3 0 9 3 2 0 3 4 8 3 3 7 2 9 3 2 7 8 2 9 6	0.37 0.35 0.37 0.34 0.35 0.28 0.34 0.35 0.34 0.35 0.34 0.33	$\begin{array}{c} 0 & . & 0 \\ 2 & 2 & . & 8 \\ 0 & . & 6 \\ 0 & . & 4 \\ 1 & . & 3 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 8 & . & 2 \\ 1 & 4 & . & 4 \\ 1 & 9 & . & 1 \end{array}$	0.4 8.8 1.8 1.4 2.1 1.1 0.4 5.8 8.9 9.0	$\begin{array}{c} 0 & . & 0 \\ 2 & . & 3 \\ 0 & . & 1 \\ 0 & . & 2 \\ 0 & . & 3 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 0 \\ 5 & . & 5 \\ 1 & . & 2 \end{array}$
4 X	1 2 3 4 5 6 7 8 9	0.235	3 5 8 2 7 3 3 1 1 3 2 4 3 1 9 3 4 5 3 4 4 2 9 9 2 8 5	0.35 0.36 0.32 0.35 0.32 0.39 0.36 0.35 0.35 0.32	$\begin{array}{c} 0 & . & 0 \\ 1 & 5 & . & 4 \\ 0 & . & 5 \\ 0 & . & 6 \\ 0 & . & 9 \\ 0 & . & 0 \\ 0 & . & 0 \\ 4 & . & 2 \\ 1 & 2 & . & 2 \end{array}$	0.2 8.8 1.3 2.6 3.7 0.7 0.3 4.6 9.6	$\begin{array}{c} 0 & . & 0 \\ 0 & . & 1 \\ 0 & . & 1 \\ 0 & . & 2 \\ 0 & . & 3 \\ 0 & . & 0 \\ 0 & . & 1 \\ 0 & . & 2 \\ 0 & . & 3 \end{array}$
5 X	1 2 3 4 5 6 7 8 9	0.435	3 5 7 2 7 8 3 1 3 3 2 7 3 2 2 3 4 1 3 4 9 2 9 4 2 8 8	0.32 0.32 0.32 0.32 0.31 0.35 0.31 0.31 0.34	0.2 20.6 2.7 2.1 1.8 0.3 0.3 9.4 11.9	$\begin{array}{c} 7 . 1 \\ 16 . 9 \\ 10 . 6 \\ 9 . 2 \\ 11 . 1 \\ 6 . 7 \\ 6 . 9 \\ 13 . 2 \\ 15 . 6 \end{array}$	$\begin{array}{c} 0 \ . \ 1 \\ 9 \ . \ 9 \\ 0 \ . \ 2 \\ 0 \ . \ 3 \\ 0 \ . \ 3 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \end{array}$

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer 1- [%]	ntration Cr-EDTA [%]
6 X	1 2 3 4 5 6 7 8 9	0.545	356 270 330 304 321 304 354 334 256	$\begin{array}{c} 0.36 \\ 0.40 \\ 0.38 \\ 0.43 \\ 0.42 \\ 0.46 \\ 0.51 \\ 0.43 \\ 0.41 \end{array}$	18.5 10.6 9.5 11.9 9.8 5.2 15.3 13.3 9.1	$ \begin{array}{r} 19.8\\ 21.3\\ 20.0\\ 23.1\\ 24.1\\ 20.3\\ 22.5\\ 21.4\\ 24.5 \end{array} $	13.1 0.4 2.8 10.7 6.5 0.2 8.3 13.2 2.4
7x	1 2 3 4 5 6 7 8 9	0.715	360 268 322 306 346 296 281 341 318	0.44 0.45 0.44 0.43 0.42 0.45 0.45 0.41 0.38 0.43	2 2 . 6 2 4 . 5 5 7 . 3 1 9 . 4 3 3 . 1 2 7 . 6 2 7 . 2 3 3 . 3 2 7 . 8	24.8 20.6 30.1 27.2 26.6 28.9 30.9 	79.7 77.7 83°.8 44.4 75.5 77.4 76.9 79.7
8 X	1 2 3 4 5 6 7 8 9 10 11 12 13	0.765	362 273 328 313 352 301 279 341 318 344 334 297 298	0.39 0.38 0.35 0.41 0.35 0.35 0.35 0.37 0.39 0.39 0.41 0.36 0.36 0.43	30.7 33.4 25.3 28.4 56.0 28.1 30.9 27.2 29.4 31.3 29.9 31.8 42.9	27.6 29.7 25.6 30.8 33.1 22.3 25.6 23.3 23.9 25.5 25.5 25.8 26.5 27.2	98.0 66.2 46.9 108.6 89.2 47.8 68.9 80.3 71.0 87.1 60.4 60.0 75.1
9 X	1 2 3 4 5 6 7 8 9	0.815	363 272 325 305 321 348 294 337 278	0.38 0.41 0.33 0.37 0.40 0.43 0.44 0.38 0.37	24.4 14.8 22.2 25.4 23.5 20.2 17.7 26.5 19.7	16.0 15.0 15.5 19.3 21.5 16.6 20.2 21.8 18.0	43.8 20.3 4.6 52.0 28.6 31.7 7.2 54.0 35.7
10X	1 2 3 4 5 6 7 8 9	0.965	3 6 3 2 6 8 3 2 6 3 1 8 3 2 2 3 5 2 2 9 5 3 4 4 2 8 2	0.35 0.40 0.42 0.37 0.38 0.37 0.37 0.37 0.40 0.38	$ \begin{array}{c} 6.3\\ 10.3\\ 4.6\\ 7.0\\ 6.1\\ 5.6\\ 10.4\\ 6.0\\ 7.6\\ \end{array} $	8.9 7.7 5.4 12.2 10.3 7.6 9.5 10.3 10.4	0.9 2.3 0.1 0.1 0.0 0.2 1.0 0.8 0.2

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Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	e concen I ⁻ [%]	Cr-EDTA
11X	1 2 3 4 5 6 7 8 9	1.015	364 271 326 311 320 351 290 346 282	0.38 0.39 0.38 0.40 0.40 0.42 0.42 0.42 0.39 0.38	9.7 3.4 1.0 5.0 2.1 2.9 1.7 9.1 4.7	$ \begin{array}{r} 1 \ 0 \ . \ 0 \\ 9 \ . \ 3 \\ 4 \ . \ 8 \\ 1 \ 2 \ . \ 7 \\ 8 \ . \ 8 \\ 7 \ . \ 8 \\ 6 \ . \ 9 \\ 1 \ 0 \ . \ 6 \\ 1 \ 2 \ . \ 2 \\ \end{array} $	9.2 0.2 0.1 0.7 0.1 0.3 0.1 11.6 0.4
12X	1 2 3 4 5 6 7 8 9 10 11 12 13	1.065	365 269 327 310 318 351 299 341 283 332 342 292 305	$\begin{array}{c} 0.41 \\ 0.38 \\ 0.42 \\ 0.43 \\ 0.41 \\ 0.40 \\ 0.42 \\ 0.44 \\ 0.40 \\ 0.42 \\ 0.44 \\ 0.40 \\ 0.39 \\ 0.42 \\ 0.42 \\ 0.41 \end{array}$	$ \begin{array}{c} 11.4\\ 5.5\\ 0.6\\ 10.0\\ 3.2\\ 4.2\\ 0.7\\ 10.0\\ 9.6\\ 1.5\\ 7.4\\ 2.0\\ 6.3\\ \end{array} $	9.4 8.2 4.2 $10.18.67.25.411.510.76.010.17.610.0$	$ \begin{array}{c} 10.6\\ 0.1\\ 0.2\\ 0.2\\ 0.5\\ 0.0\\ 2.1\\ 0.3\\ 0.0\\ 0.3\\ 0.1\\ 0.3 \end{array} $
13X	1 2 3 4 5 6 7 8 9	1.115	3 6 2 2 6 9 3 3 0 3 0 6 3 4 5 3 5 3 3 0 0 2 8 0 3 2 2	0.41 0.42 0.41 0.39 0.38 0.44 0.42 0.39 0.39 0.40	10.610.41.214.112.75.31.516.36.0	7.8 7.4 4.3 9.8 8.4 6.8 5.2 10.5 8.0	$ \begin{array}{c} 1 . 4 \\ 0 . 0 \\ 0 . 0 \\ 0 . 4 \\ 5 . 7 \\ 0 . 2 \\ 0 . 1 \\ 2 . 2 \\ 0 . 1 \end{array} $
14X	1 2 3 4 5 6 7 8 9	1.165	360 270 330 310 349 343 299 282 319	0.36 0.41 0.42 0.43 0.42 0.42 0.42 0.42 0.42 0.43 0.42	7.6 15.1 1.6 8.1 3.9 6.0 3.5 13.9 4.0	5.3 8.4 4.2 7.8 4.7 4.4 5.8 8.5 5.6	$\begin{array}{c} 0 & . & 0 \\ 1 & . & 7 \\ 0 & . & 1 \\ 0 & . & 1 \\ 0 & . & 3 \\ 0 & . & 1 \\ 0 & . & 1 \\ 4 & . & 4 \\ 0 & . & 2 \end{array}$
15X	1 2 3 4 5 6 7 8 9	1.215	362 272 329 303 352 299 281 339 321	0.43 0.41 0.44 0.51 0.44 0.48 0.48 0.42 0.46	1.0 13.4 1.6 3.2 0.6 6.0 12.0 0.9 1.8	2.9 5.1 2.5 5.6 2.0 3.5 6.1 3.8 3.6	0.0 7.4 0.0 0.1 0.1 0.1 3.3 0.2 0.2

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer 1 ⁻ [%]	ntration Cr-EDTA [%]
16X	1 2 3 4 5 6 7 8 9 10 11 12 13	1.265	362 271 329 310 356 298 342 278 319 295 333 303 303 335	$\begin{array}{c} 0.44 \\ 0.41 \\ 0.39 \\ 0.44 \\ 0.43 \\ 0.41 \\ 0.41 \\ 0.41 \\ 0.43 \\ 0.42 \\ 0.42 \\ 0.42 \\ 0.42 \\ 0.42 \\ 0.42 \\ 0.42 \\ 0.42 \end{array}$	$\begin{array}{c} 0 \ . \ 1 \\ 1 \ 1 \ . \ 7 \\ 1 \ . \ 0 \\ 1 \ . \ 5 \\ 0 \ . \ 1 \\ 6 \ . \ 9 \\ 0 \ . \ 2 \\ 7 \ . \ 0 \\ 1 \ . \ 3 \\ 8 \ . \ 1 \\ 0 \ . \ 6 \\ 2 \ . \ 2 \\ 0 \ . \ 4 \end{array}$	2.0 6.3 2.9 4.6 2.0 4.3 2.8 6.8 3.9 6.0 2.6 5.0 3.0	$\begin{array}{c} 0 \ . \ 0 \\ 0 \ . \ 6 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 2 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 1 \end{array}$
17X	1 2 3 4 5 6 7 8 9	1.315	3 6 1 2 6 9 3 2 8 3 1 7 3 2 5 3 5 2 2 9 9 3 4 4 2 8 6	0.45 0.40 0.37 0.41 0.40 0.39 0.35 0.40 0.38	0.4 16.5 4.3 1.8 3.3 1.0 10.0 0.8 7.6	$ \begin{array}{r} 1.6\\ 6.2\\ 2.5\\ 3.4\\ 3.4\\ 1.7\\ 4.1\\ 2.3\\ 6.3 \end{array} $	$\begin{array}{c} 0 \ . \ 0 \\ 2 \ 0 \ . \ 6 \\ 0 \ . \ 3 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 5 \ . \ 9 \\ 0 \ . \ 1 \\ 2 \ . \ 3 \end{array}$
18X	1 2 3 4 5 6 7 8 9 10	1.405	3 6 4 2 7 5 3 3 0 3 1 8 3 1 7 3 5 2 2 9 6 3 4 6 2 8 8 2 9 6	0.40 0.42 0.39 0.42 0.45 0.44 0.37 0.44 0.40 0.40	0.1 3.6 0.4 1.2 1.0 0.1 1.5 0.2 2.1 2.1	0.4 1.8 0.7 1.3 1.2 0.5 1.3 0.6 1.7 1.4	$\begin{array}{c} 0 \ . \ 2 \\ 1 \ . \ 3 \\ 0 \ . \ 2 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 2 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 1 \end{array}$
19X	1 2 3 4 5	1.555	364 271 319 300 302	0.37 0.34 0.34 0.36 0.29	0.0 0.0 0.0 0.0 0.0	0.1 0.3 0.2 0.2 0.2	0.0 0.0 0.0 0.0 0.0
20 X	1 2 3 4 5	1.765	364 271 329 309 314	0.33 0.27 0.30 0.31 0.27	0.0 0.0 0.0 0.0 0.0	0.0 0.2 0.0 0.1 0.1	0.0 0.0 0.0 0.0 0.0
21X	1 2 3 4 5	1.815	361 273 321 302 307	0.32 0.35 0.34 0.34 0.40	0.0 0.0 0.0 0.0 0.0	0.0 0.1 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0

Table A5.1 continued

	Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	cr-EDTA
	22X	1 2 3 4 5	1.965	366 274 299 312 299	0.32 0.32 0.32 0.33 0.33 0.31	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0
	23X	1 2 3 4 5	2.015	365 272 307 318 303	0.33 0.32 0.32 0.33 0.33	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0
3	24X	1 2 3 4 5 6 7 8 9	2.065	3 6 4 2 7 3 3 2 8 3 1 7 2 9 5 3 5 6 3 5 1 2 8 5 3 2 5	0.36 0.35 0.36 0.35 0.40 0.37 0.39 0.38 0.34	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
	2 5 X	1 2 3 4 5 6 7 8 9	2.215	366 272 330 313 296 356 347 284 321	0.39 0.37 0.42 0.38 0.40 0.37 0.35 0.36 0.38	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \\ 0 \ . \ 0 \end{array}$	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
	26X	1 2 3 4 5 6 7 8 9	2.265	367 272 331 311 354 302 345 285 321	0.37 0.40 0.40 0.37 0.44 0.37 0.37 0.37 0.37 0.39	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
	27X	1 2 3 4 5 6 7 8 9	2.315	365 272 330 324 355 283 313 346 285	0.37 0.36 0.36 0.36 0.37 0.36 0.39 0.41 0.35	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concen I ⁻ [%]	tration Cr-EDTA [%]
28X	1 2 3 4 5	2.415	361 274 331 317 323	0.32 0.32 0.28 0.30 0.33	0.0 0.0 0.0 0.1 0.0	0.0 0.1 0.0 0.1 0.0	0.0 0.0 0.0 0.0 0.0
29X	1 2 3 4 5	2.625	344 277 312 361 331	0.28 0.28 0.28 0.41 0.38	0.0 0.0 0.0 0.0 0.0	0.1 0.6 0.2 0.0 0.0	0.0 0.0 0.0 0.0 0.0
30X	1 2 3 4 5	2.675	359 274 324 314 323	0.39 0.30 0.33 0.34 0.47	0.0 0.0 0.0 0.0 0.0	0.1 0.2 0.1 0.0 0.0	0.0 0.0 0.0 0.0 0.0
31X	1 2 3 4 5	2.815	364 274 330 314 323	 0.33 0.35 0.33 0.33 0.32 	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0
32X	1 2 3 4 5	2.965	3 6 4 2 7 2 3 2 8 3 2 0 3 2 2	0.28 0.26 0.28 0.29 0.28	$\begin{array}{c} 0 & . & 0 \\ 0 & . & 1 \\ 0 & . & 0 \\ 0 & . & 0 \\ 0 & . & 1 \end{array}$	0.2 1.0 0.2 0.2 0.3	0.0 0.0 0.0 0.0 0.0
33 <i>X</i>	1 2 3 4 5 6 7 8 9	3.015	3 6 4 2 7 3 3 3 3 3 1 2 3 5 7 3 0 1 3 4 6 3 3 6 3 0 7	0.30 0.27 0.32 0.30 0.24 0.27 0.34 0.30 0.29	0.1 1.0 0.2 0.2 0.3 0.6 0.0 0.0 0.6	0.4 1.0 0.4 0.9 0.8 0.8 0.5 0.7 1.6	0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
34X	1 2 3 4 5 6 7 8 9 10 11 12 13	3.065	271 324 331 363 302 318 284 354 346 289 320 298 311	0.28 0.28 0.34 0.32 0.31 0.28 0.28 0.28 0.31 0.31 0.31 0.30 0.29 0.30 0.29	6.2 0.6 0.7 0.1 1.9 0.2 3.0 0.2 3.0 0.2 0.1 2.5 0.6 1.3 0.8	4.1 1.4 0.9 0.4 1.8 1.4 3.3 0.6 0.4 3.1 1.6 2.6 2.0	0.4 0.1 0.0 0.3 0.0 0.0 0.3 0.1 0.1 0.1 0.0 0.0 0.0

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Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	ntration Cr-EDTA [%]
1T	1 2 3 4 5	-0.025	216 200 233 219 214	0.37 0.39 0.37 0.36 0.38	19.2 16.3 2.5 9.2 13.3	9.6 10.0 3.4 8.4 8.9	18.9 20.1 5.4 4.7 23.6
2 T	1 2 3 4 5	0.025	214 199 232 213 218	0.37 0.35 0.38 0.35 0.36	21.9 22.0 11.8 15.8 14.2	14.8 14.5 10.4 12.4 10.8	24.0 25.6 11.8 22.6 12.1
3 T	1 2 3 4	0.075	217 201 232 216	0.32 0.35 0.32 0.35	25.1 25.3 18.4 19.3	21.9 19.9 14.7 17.2	24'.2 26.2 18.1 27.7
4 T	1 2 3 4	0.325	214 195 213 220	0.33 0.32 0.30 0.27	32.1 19.6 18.3 23.8	30.0 18.4 16.9 22.4	68.6 47.0 40.0 46.7
5 T	1 2 3	0.375	215 210 199	0.36 0.31 0.30	32.3 33.2 30.8	32.8 27.3 30.9	70.7 62.6 68.4
6 T	1 2 3 4	0.425	214 198 207 226	0.30 0.26 0.34 0.32	24.4 35.4 36.2 24.0	28.1 32.7 31.0 22.8	52.8 65.9 77.0 59.0
7 T	1 2 3	0.475	217 201 217	0.34 0.28 0.34	27.3 18.5 28.8	21.5 18.4 24.3	52.8 43.6 65.4
8 T	1 2 3 4	0.595	215 226 208 198	0.33 0.33 0.31 0.33	25.1 21.3 20.4 26.0	20.4 15.6 16.6 19.9	54.7 44.3 21.2 41.0
9 T	1 2 3	0.695	218 203 209	0.41 0.43 0.37	10.8 8.2 9.7	9.7 10.1 10.9	11.1 2.4 1.0
10T	1 2 3 4	0.745	2 1 9 2 0 5 2 3 4 2 1 3	0.35 0.36 0.34 0.35	15.5 15.0 21.3 7.5	13.9 13.4 15.1 10.5	2 . 5 1 . 3 2 . 1
11T	1 2 3 4	0.795	216 200 231 214	0.41 0.39 0.36 0.40	24.6 23.4 25.0 28.2	14.2 13.2 12.7 14.6	1 . 8 3 . 2 2 . 4 8 . 6

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Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	ntration Cr-EDTA [%]
12T	1 2 3 4 5	0.845	216 200 231 214 220	0.36 0.39 0.37 0.37 0.37 0.39	40.6 21.4 21.9 25.2 22.0	18.2 11.6 15.7 16.3 14.4	25.2 20.7 16.6 40.6 6.1
13T	1 2 3 4 5	0.895	215 201 230 214 218	0.35 0.36 0.39 0.35 0.36	31.3 27.2 31.6 23.3 30.6	18.2 14.6 14.9 13.8 14.0	33.2 26.8 19.0 41.2 6.0
14T	1 2 3 4 5	0.945	216 200 232 213 219	0.39 0.37 0.40 0.38 0.39	32.6 27.9 37.7 23.7 16.9	13.4 14.2 9.6 12.8 10.4	8.0 0.3 0.1 4.7
15T	1 2 3 4 5	0.995	215 200 229 216 219	0.34 0.34 0.33 0.36 0.33	29.4 43.8 26.7 31.2 24.0	19.0 19.5 17.2 14.3 16.8	1.1 15.4 7.6
16T	1 2 3 4 5	1.045	217 204 233 219 213	0.39 0.36 0.39 0.40 0.40	19.2 37.7 24.7 23.1 24.0	22.3 21.3 14.3 16.3 17.0	0.7 0.0 0.0 0.3 0.1
17T	1 2 3 4 5	1.095	217 204 231 215 223	0.41 0.42 0.42 0.43 0.43	21.7 17.0 26.3 22.3 23.3	18.1 16.3 15.3 17.9 15.4	6.4 5.4 2.5 4.2 2.6
18T	1 2 3 4 5 6	1.145	214 198 207 226 230 218	0.45 0.44 0.44 0.47 0.47 0.44 0.42	15.0 16.4 22.3 42.8 19.9 21.4	12.9 10.9 12.6 11.9 13.4 14.6	36.5 33.8 26.8 20.3 30.2
19T	1 2 3 4 5	1.195	214 198 230 215 218	0.37 0.38 0.36 0.41 0.40	30.9 28.5 27.3 22.5 28.8	17.8 14.1 15.5 14.4 14.7	37.0 40.0 38.8 46.6 10.1
20T	1 2 3 4	1.290	216 203 230 219	0.32 0.32 0.33 0.31	12.6 23.2 6.7 19.3	15.7 17.0 10.4 13.0	0.0 0.3 0.1 1.0

Table A5.1 continued

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Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I- [%]	Cr-EDTA
21 T	1 2 3 4 5	1.340	216 199 231 214 219	0.35 0.37 0.40 0.38 0.34	14.0 21.8 5.8 18.0 4.5	13.8 13.0 8.8 11.4 8.7	$\begin{array}{c} 0 \ . \ 1 \\ 0 \ . \ 1 \\ 0 \ . \ 0 \\ 0 \ . \ 3 \\ 0 \ . \ 1 \end{array}$
2 2 T	1 2 3 4 5	1.390	2 1 5 2 0 3 2 2 9 2 1 5 2 2 0	0.30 0.27 0.29 0.29 0.31	24.2 30.8 25.4 29.6 11.3	16.7 20.7 16.1 13.4 11.0	0.0 0.0 0.0 0.3 0.1
2 3 T	1 2 3 4 5	1.540	216 200 229 216 216	0.27 0.30 0.26 0.27 0.27	10.1 10.7 4.7 4.8 3.7	10.7 8.1 8.8 6.8 6.5	0.0 0.1 0.2 0.4 0.1
24T	1 2 3 4 5	1.590	217 201 232 214 219	0.32 0.36 0.26 0.33 0.33	1 . 5 2 . 8 0 . 5 1 . 0 1 . 7	5.8 5.0 3.7 3.7 3.1	0.0 0.0 0.0 0.0 0.0
2 5 T	1 2 3 4 5	1.640	216 202 228 216 219	0.27 0.27 0.27 0.28 0.28	0.4 0.6 0.2 0.5 0.1	4.1 3.6 3.9 2.9 2.9	0.0 0.0 0.0 0.0 0.0
2 G T	1 2 3 4	1.690	2 0 9 1 9 6 2 2 5 2 1 8	0.26 0.24 0.25 0.28	0.1 0.1 0.1 0.0	1.9 1.5 1.8 1.8	0.0 0.0 0.0 0.0
27 T	1 2 3 4 5	1.840	212 198 224 215 218	0.25 0.22 0.24 0.25 0.26	0.4 0.2 0.4 0.2 0.1	1.2 0.9 1.5 0.7 1.3	0.0 0.0 0.0 0.0 0.0
28T	1 2 3 4 5	1.890	2 1 6 2 0 3 2 3 2 2 1 6 2 2 2 2	0.35 0.34 0.41 0.37 0.34	0.0 0.0 0.0 0.0 0.0	0.6 0.6 0.4 0.3 0.9	0.0 0.0 0.0 0.0 0.0
29T	1 2 3 4 5	1.940	215 200 229 217 217	0.32 0.30 0.31 0.30 0.30	0.0 0.0 0.0 0.0 0.0	0.5 0.4 0.3 0.2 0.4	0.0 0.0 0.0 0.0 0.0

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	e concer I ⁻ [%]	ntration Cr-EDTA [%]
30T	1 2 3 4 5	1.990	215 200 229 217 218	0.35 0.36 0.39 0.35 0.40	0.0 0.0 0.0 0.0 0.0	0.3 0.3 0.3 0.4 0.2	0.0 0.0 0.0 0.0 0.0 0.0
31T	1 2 3 4 5	2.040	211 198 225 206 214	0.29 0.28 0.31 0.28 0.30	0.0 0.0 0.0 0.0 0.0	0.4 0.4 0.3 0.5 0.2	0.0 0.0 0.0 0.0 0.0
3 2 T	1 2 3 4 5	2.160	215 200 229 209 213	0.34 0.36 0.33 0.36 0.34	3.2 0.7 8.8 1.8 1.0	7.7. 4.0 8.6 4.5 4.7	0.0 0.0 0.0 0.2 0.0
3 3 T	1 2 3 4 5	2.210	2 1 7 2 3 1 2 0 6 2 1 3 2 2 5	0.40 0.38 0.38 0.40 0.38	12.1 4.1 33.2 15.0 7.7	10.8 8.0 11.9 9.7 8.3	0.2 0.0 6.9 0.3 0.0
34T	1 2 3 4 5	2.260	213 199 230 215 219	0.35 0.37 0.35 0.36 0.35	20.9 10.1 41.3 29.0 16.4	12.7 8.8 13.6 10.8 10.5	0.3 0.2 11.2 3.6 0.3
3 5 T	1 2 3 4	2.410	217 202 231 217	0.30 0.27 0.26 0.21	6.2 4.5 29.0 20.2	6.8 5.5 12.5 10.2	0.2 0.2 1.0 0.5
36T	1 2 3 4 5	2.460	214 199 230 216 216	0.30 0.30 0.30 0.30 0.29	3 . 5 2 . 1 5 . 4 4 . 5 2 . 0	5.8 4.1 8.2 8.6 3.6	0.2 0.0 0.2 0.2 0.2 0.2
37 T	1 2 3 4 5	2.510	213 199 228 215 217	0.30 0.35 0.33 0.36 0.33	3.0 0.8 5.0 2.9 2.0	7.6 4.7 13.1 13.7 5.8	0.0 0.0 0.0 0.2 0.1
3 8 T	1 2 3 4 5	2.660	215 201 230 219 220	0.31 0.30 0.32 0.33 0.32	1.9 0.6 5.1 2.7 0.6	6.4 5.3 6.6 7.7 3.6	0.0 0.0 0.0 0.0 0.0 0.1

Table A5.1 continued

Core	No.	Depth [m]	Distance [mm]	Porosity [%]	Relative Uranine [%]	concer I ⁻ [%]	ntration Cr-EDTA [%]
39T	1 2 3 4 5	2.710	214 200 229 216 216	0.32 0.30 0.31 0.31 0.29	5.8 1.4 11.4 8.9 2.2	7.0 5.3 6.6 12.3 4.9	0.1 0.1 0.2 0.2 0.4
4 0 T	1 2 3 4 5	2.760	219 232 207 212 225	0.32 0.33 0.30 0.31 0.30	3.0 1.4 8.6 5.0 2.8	6.0 6.3 6.0 7.8 7.2	0.1 0.0 0.1 0.2 0.3
4 1 T	1 2 3 4 5	2.810	215 200 230 215 218	0.27 0.26 0.26 0.26 0.26 0.25	3.9 1.4 6.5 4.0 2.2	8.0 6.3 6.7 7.7 7.2	0.1 0.2 0.2 0.4 0.3
4 2 T	1 2 3 4 5	2.860	215 200 230 212 219	0.27 0.30 0.30 0.29 0.31	3.5 1.2 7.3 3.6 1.0	5.9 4.6 5.3 5.9 2.8	0.1 0.2 0.1 0.2 0.2
4 3 T	1 2 3 4 5	2.910	2 2 1 2 3 4 2 0 6 2 1 2 2 2 6	0.33 0.31 0.30 0.26 0.34	1.0 0.6 2.8 2.4 0.4	3.0 3.6 4.7 6.4 1.7	0.0 0.1 0.1 0.2 0.1
44T	1 2 3 4 5	2.960	2 2 0 2 3 3 2 0 5 2 1 4 2 2 4	0.34 0.30 0.23 0.25 0.28	0.3 0.1 1.5 0.8 0.1	2.2 1.7 4.6 7.8 1.0	0.0 0.0 0.1 0.1 0.2
4 5 T	1 2 3 4 5	3.010	215 200 229 217 218	0.31 0.32 0.32 0.33 0.33 0.30	0.0 0.0 0.0 0.0 0.0	0.8 0.5 1.3 3.4 0.3	0.0 0.0 0.1 0.2 0.2

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Table A5.1 continued

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197**9**

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Preliminary investigations of deep ground water microbiology in Swedish granitic rocks

Karsten Pedersen University of Göteborg December 1987

TR 88-02

Migration of the fission products strontium, technetium, iodine, cesium and the actinides neptunium, plutonium, americium in granitic rock

Thomas Ittner¹, Börje Torstenfelt¹, Bert Allard² ¹Chalmers University of Technology ²University of Linköping January 1988

TR 88-03

Flow and solute transport in a single fracture. A two-dimensional statistical model

Luis Moreno¹, Yvonne Tsang², Chin Fu Tsang², Ivars Neretnieks¹

¹Royal Institute of Technology, Stockholm, Sweden ²Lawrence Berkeley Laboratory, Berkeley, CA, USA January 1988

TR 88-04

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J A Marinsky, M M Reddy, J Ephraim, A Mathuthu US Geological Survey, Lakewood, CA, USA Linköping University, Linköping State University of New York at Buffalo, Buffalo, NY, USA April 1987

TR 88-05

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