Technical Report TR-04-17

# Thermal spike theory of athermal diffusion of fission products due to alpha decay of actinides in spent fuel $(UO_2)$

D. Olander, University of California Berkeley

March 2004

Svensk Kärnbränslehantering AB

Swedish Nuclear Fuel and Waste Management Co Box 5864 SE-102 40 Stockholm Sweden Tel 08-459 84 00 +46 8 459 84 00 Fax 08-661 57 19 +46 8 661 57 19



## Thermal spike theory of athermal diffusion of fission products due to alpha decay of actinides in spent fuel $(UO_2)$

D. Olander, University of California Berkeley

March 2004

This report concerns a study which was conducted for SKB. The conclusions and viewpoints presented in the report are those of the author and do not necessarily coincide with those of the client.

A pdf version of this document can be downloaded from www.skb.se

### Thermal spike theory of athermal diffusion of fission products due to alpha decay of actinides in spent fuel (UO<sub>2</sub>)

Radioactive decay of an actinide produces an alpha particle of typically 5 MeV and a recoil atom of ~100 keV. The alpha particle loses energy primarily by electronic stopping, which is quickly converted to heat. This is the origin of the "thermal spike" discussed by Matzke for fission fragments. Using the TRIM code, a 5 MeV alpha particle produces only 178 defects (vacancy-interstitial pairs), most of which are sufficiently widely separated that recombination is minimal. Figure 1 shows the TRIM output for a 5 MeV alpha particle entering  $UO_2$  from the left. The black dots at the end of the brush-like displacement damage pattern (2000 ions were injected) represent the stopped alpha particles, which are helium atoms. Examination of the tracks on the periphery show widely-spaced dots, each of which represents a nuclear collision of the alpha particle with a U or O ion. The dots merge towards the end of the alpha particle range because the atom-ion cross section increases with decreasing energy.

The recoil heavy element from the decay event produces ~1200 displacements /1/. The range of the recoil is only 25 nm, so most of the vacancies and interstitials recombine. The effect of recoils on the athermal diffusion coefficient is probably small, and is neglected in this analysis. Matzke argues that the enhanced diffusivity due to the fission fragments arises from two sources: the thermal spike and the pressure spike. Displacement damage is a minor contributor.



*Figure 1.* Damage pattern in  $UO_2$  produced by 5 MeV alpha particles.

The present work assumes that an alpha particle slowing down in UO<sub>2</sub> possesses a constant electronic stopping power and negligible nuclear stopping (99.7% of the particle's energy is lost by ionization /1/). The slowing down creates a line source of heat equal to  $8 \times 10^{-14}$  J/µm over the 10 µm range of the 5 MeV alpha particle in UO<sub>2</sub>.

The trajectories in Figure 1 do not look much like a line because the ordinate scale is much enlarged compared to the abscissa scale. The radial straggling is only  $\sim 0.6 \,\mu$ m.

### Thermal spike due to 5 MeV Alpha Particle in UO<sub>2</sub>

The transient temperature profile from a line source of heat is given by Carslaw and Jaeger /2/:

$$\Delta T = \frac{dE/dx}{4\pi kt} \exp\left(-\frac{r^2}{4\pi t}\right)$$
(1)

where dE/dx is the energy released from the line source per unit length (see above) and k is the thermal conductivity of UO<sub>2</sub> (~0.03 W/cm-K). The radial distance from the line is r and t is the time. Inserting these numbers into Equation (1) yields:

$$\Delta T = \frac{2.12}{t} \exp\left(-280\frac{r^2}{t}\right)$$
(2)

where r is in  $\mu m$  and t is in ns.

Equation (2) is plotted in Figure 2.



*Figure 2.* Temperature rise in  $UO_2$  resulting from passage of a 5 MeV alpha particle.

### **Diffusion Coefficient**

The "thermal" diffusion coefficient in a solid is given by the Einstein equation:

$$D = \frac{1}{6}a^2\beta \operatorname{vexp}(-E/RT) = D_0 \exp(-E/RT)$$
(3)

where

a = jump distance

 $\beta$  = number of sites surrounding equilibrium site

v = vibration frequency of atom in equilibrium site

E = activation energy for diffusion

R = gas constant

 $\beta v \exp(-E/RT) = \text{jump frequency per atom}$ 

The approach to athermal diffusion is to first determine the jumps of a solute atom (e.g., Xe) due to the alpha particle track from a single decay event. The jumps are caused by the momentary increase in temperature, as given by Equation (2). It is assumed that the base temperature of the spent fuel is low enough that the jump frequency, and hence the solute diffusivity, is negligible. A differential cylindrical volume  $2\pi r dr L$ , where L is the range of the alpha particle, contains  $2\pi r dr L\rho_i$  atoms of species i, where  $\rho_i$  is the concentration of this species (atoms of i per unit volume). In this volume element and in time dt, the number of jumps of species i is:

$$dj_i = 2\pi r dr L\rho_i dt v_i \exp \left[-\frac{E_i/R}{\Delta T(r,t)}\right]$$

Integrating over r and t yields the jumps of species i per alpha particle:

$$j_{i} = \pi L \rho_{i} v_{i} \int_{0}^{\infty} dr^{2} \int_{0}^{\infty} dt \exp\left[-\frac{E_{i}/R}{\Delta T(r^{2},t)}\right]$$
(4)

The spatial variable of integration has been switched from r to  $r^2$  because the square appears in Equation (2).

The rate of disintegration of actinide n per unit volume is  $\lambda_n N_n$ , where  $\lambda_n$  is the decay constant and  $N_n$  is the atom density of the actinide. The number of jumps of fission product i per unit volume and per unit time due to decays of actinide n is  $\lambda_n N_n j_i$ . Dividing by the density of species i,  $\rho_i$ , gives the frequency of jumping of an atom of i, which is the equivalent of  $\beta vexp(-E/RT)$  in Equation (3). Multiplying Equation (4) by  $a^2\beta/6$  yields the athermal diffusivity of species i due to alpha particles from actinide n:

$$D_{i,n}^* = (\frac{1}{6}a^2\beta v_i)\pi L\lambda_n N_n \int_0^\infty dr^2 \int_0^\infty dt \exp\left[-\frac{E_i/R}{\Delta T(r^2,t)}\right]$$

From Equation (3), the terms in the parentheses in the above equation constitutes the preexponential factor of the Arrhenius form of the diffusivity of i, so the athermal diffusivity of fission product i due to actinide n is:

$$D_{i,n}^{*} = \pi D_{o,i} L \lambda_n N_n \int_0^\infty dr^2 \int_0^\infty dt \, exp\left[-\frac{E_i/R}{\Delta T(r^2, t)}\right]$$
(5)

For i = Xe,  $E_{xe} = 293 \text{ kJ/mole /3/ and so the double integral in Equation (5) is equal to <math>6.54 \times 10^{-12} \text{ }\mu\text{m}^2\text{-ns}$ , or  $6.54 \times 10^{-29} \text{ cm}^2\text{-s}$ . The pre-exponential factor is  $D_{o,Xe} = 7.6 \times 10^{-6} \text{ cm}^2\text{/s}$  and the alpha particle range is  $L = 10^{-3} \text{ cm}$ . The athermal diffusivity of species i in the spent fuel is the sum of Equation (5) over all actinides:

$$D_{Xe}^{*} = \sum D_{Xe,n}^{*} = 1.6 \times 10^{-36} \sum_{n} \lambda_{n} N_{n}$$
(6)

where  $\lambda_n$  is in s<sup>-1</sup> and N<sub>n</sub> is in atoms/cm<sup>3</sup>. Table 1 gives the components of the sum for PWR fuel with a burnup of 60 MWd/kgU after 20 years of cooling.

Nuclide Dis/s-cm<sup>3</sup> × 10<sup>-8</sup> Pu 238 25.0 Pu 239 1.3 Pu 240 1.9 Am 241 22.8 Am 243 0.4 Cm 243 0.1 Cm 244 20.9 Total 72.4

Table 1. Alpha activity in spent fuel (only nuclides with activities >10<sup>7</sup> dis/s-cm<sup>3</sup> included).

Inserting the total alpha activity from Table 1 into Equation (6) gives an athermal diffusivity for Xe of:

$$D_{Xe}^* = 1.2 \text{ x } 10^{-26} \text{ cm}^2/\text{s}$$

This value is five orders of magnitude smaller than the value estimated by Poinssot et al /4/.

### References

- /1/ H J Matzke, Solid State Phenomena, 30 (1993) 355
- /2/ Carslaw and Jaeger, "Conduction of Heat in Solids", p 258 Oxford Press (1959)
- /3/ J A Turnbull and E Kolstad, Inter. Seminar on Fission Gas Behavior in Water Reactor Fuels, Paper No. 3.4, Cadarache. France (2000)
- /4/ C Poinssot et al, Mat. Res. Soc. Symp. Proc. 713 (2002) 615

ISSN 1404-0344 CM Digitaltryck AB, Bromma, 2004