

Prediction of Swelling Pressures of Different Types of Bentonite in Dilute Solutions

Model development and simulations

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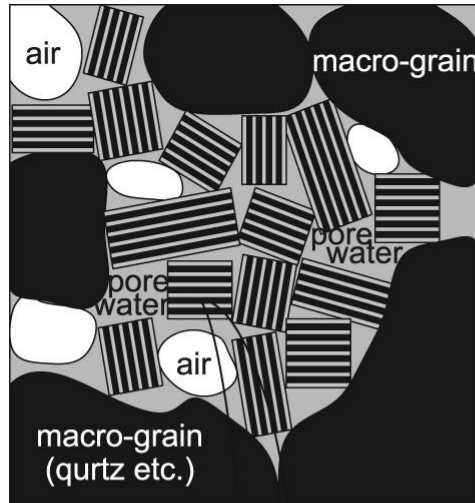
Bentonite Buffer


Candidate buffers

➤ **MX-80 (Na-bentonite)**

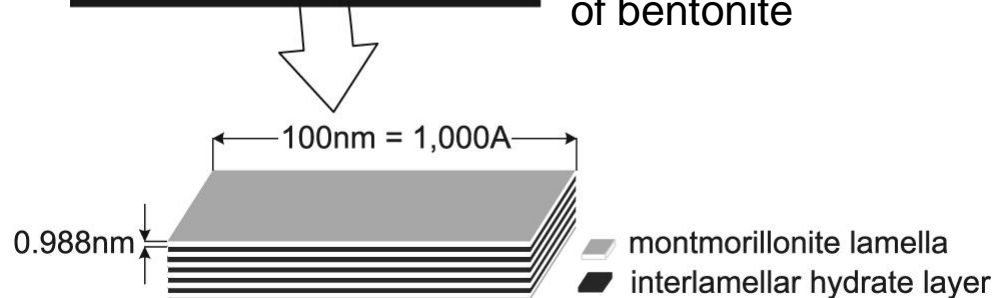
➤ **Deponit CA-N (Ca-bentonite)**

> 80 % smectite



 A stack of montmorillonite lamellae

Microscopic structure
of bentonite



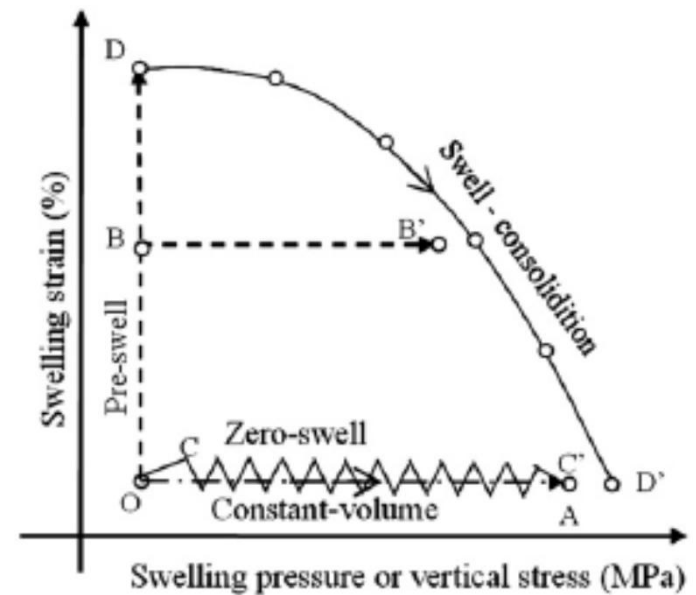
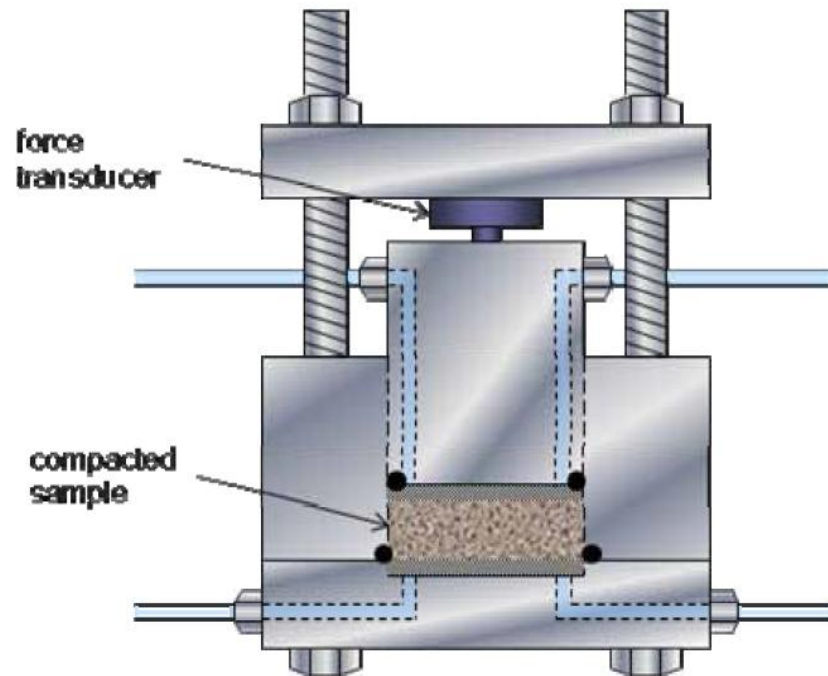
(b) A stack of montmorillonite lamellae



Bentonite clay

Swelling Pressures

➤ Measurements



Swelling Pressures

➤ Available models

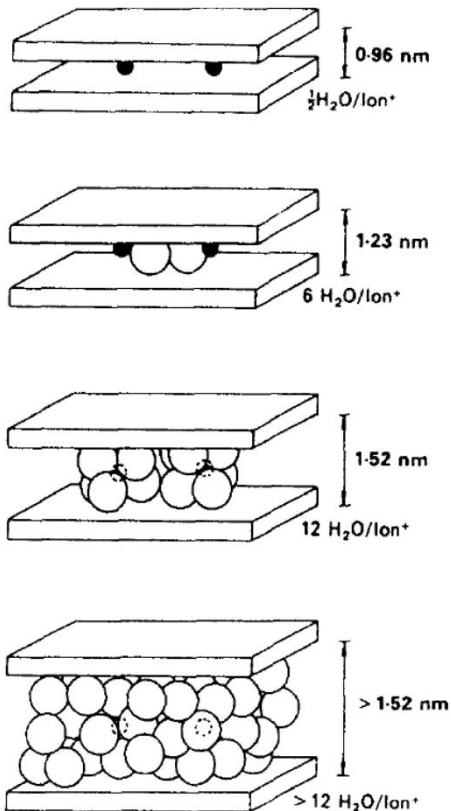
- Empirical models (simple regression expressions)
- Phenomenological models (like BBM, BExM, etc.)
- Thermodynamic models (based on the fact of $p = s$)
- Diffuse double-layer models (like DLVO, DLVOE, etc.)
- Statistical mechanical models (like DFT, IET, etc.)
-

Swelling Mechanisms

➤ Important processes

- Crystalline swelling (interlayer swelling)
- Osmotic swelling (interparticle swelling)
- Breakup of montmorillonite particles (stacks)
- Demixing of exchangeable cations
- Co-volume swelling
- Brownian swelling

Crystalline Swelling



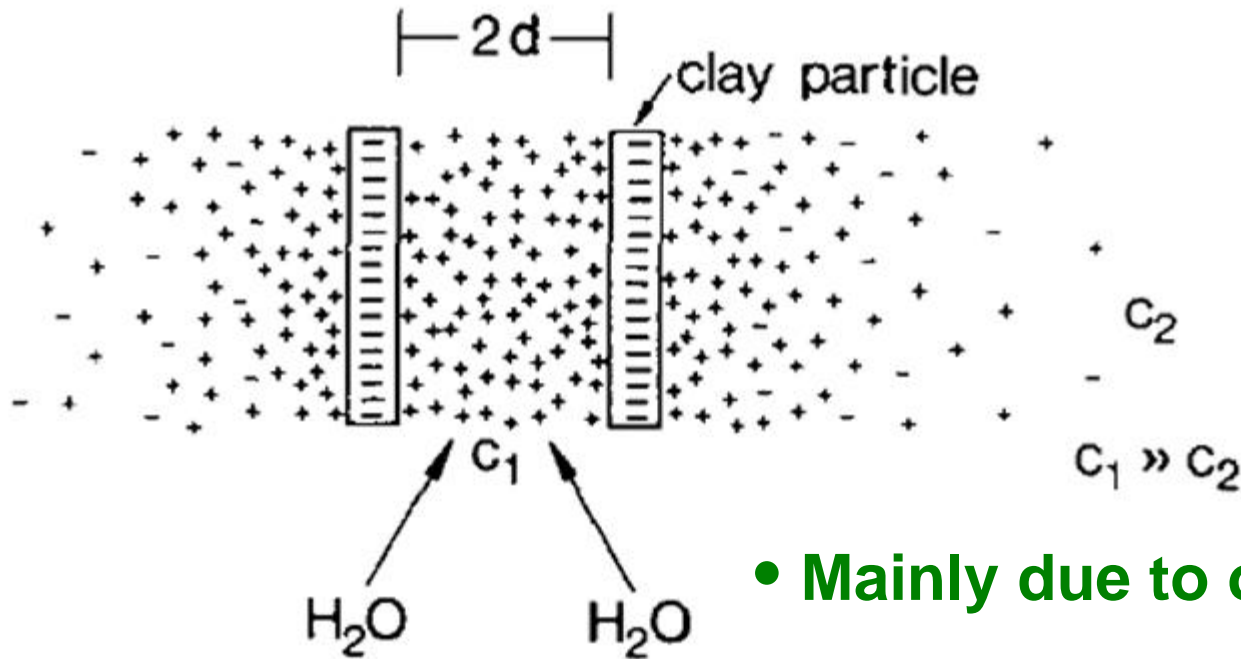
- Mainly due to hydration of cations and surface charge sites
- Take up water layer-wisely layer after layer up to 3 or 4 layers

Basal spacings (in nm)

Exchangeable cation	p_v/p_0			
	0	0.5	0.7	1
Na^+	0.95	1.24	1.51	M
K^+	1	1.24	d	1.5
Mg^{2+}	0.95	1.43	d	1.92
Ca^{2+}	0.95	1.5	1.5	1.89

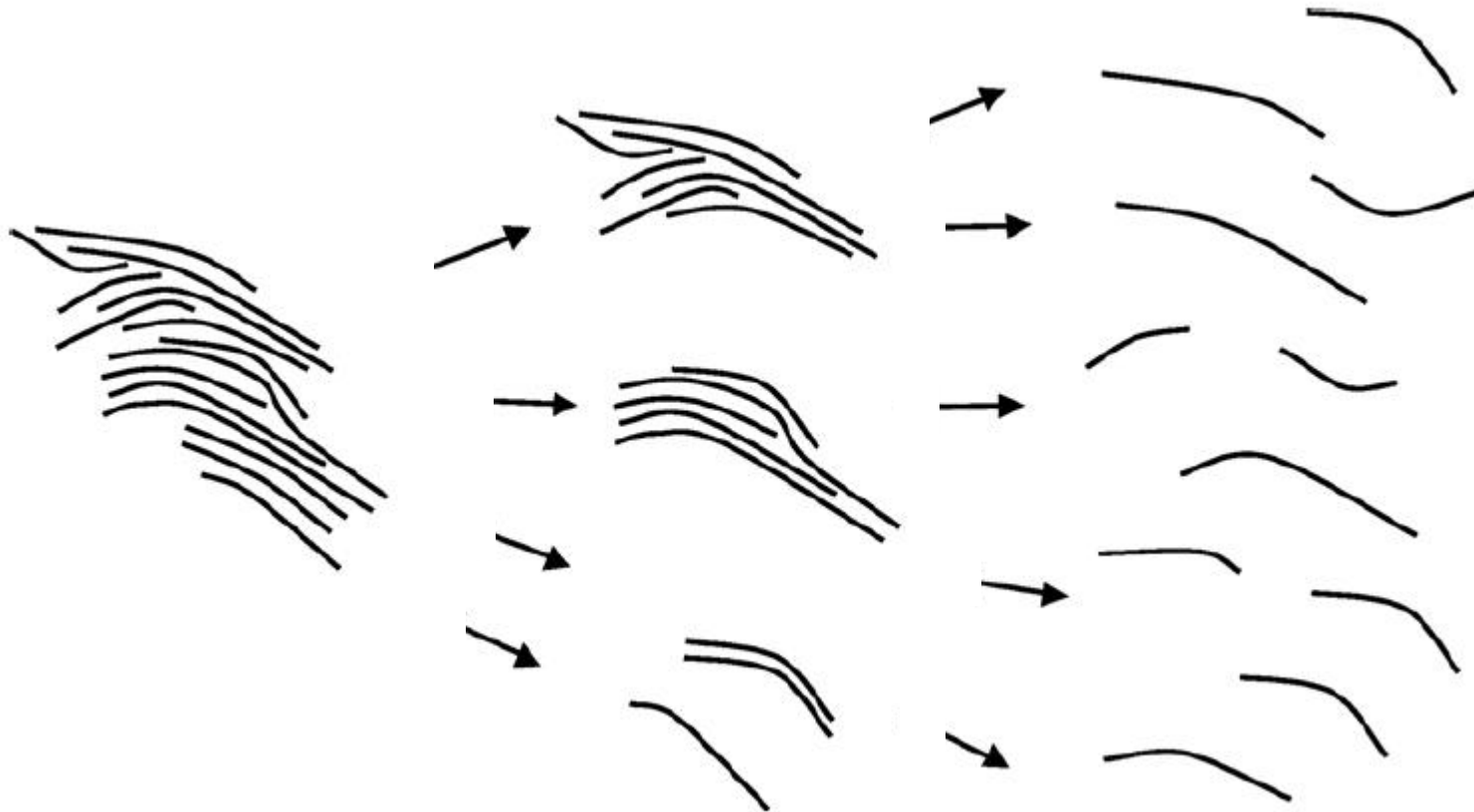
d: diffuse reflections; M: macroscopic swelling.

Osmotic Swelling

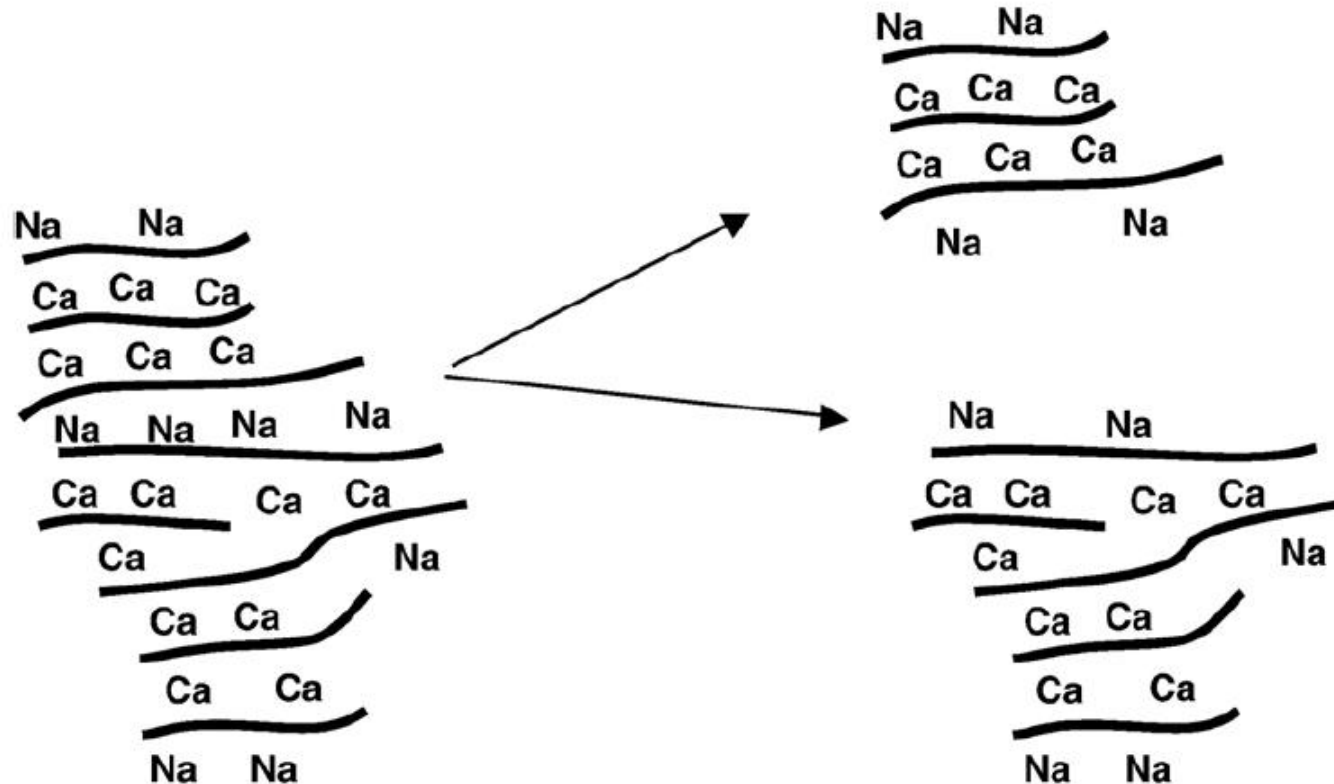


- Mainly due to overlapping of diffuse double-layers
- Depending on the pore water chemistry (ν , c , σ , etc.)

Breakup of Mont. Particles

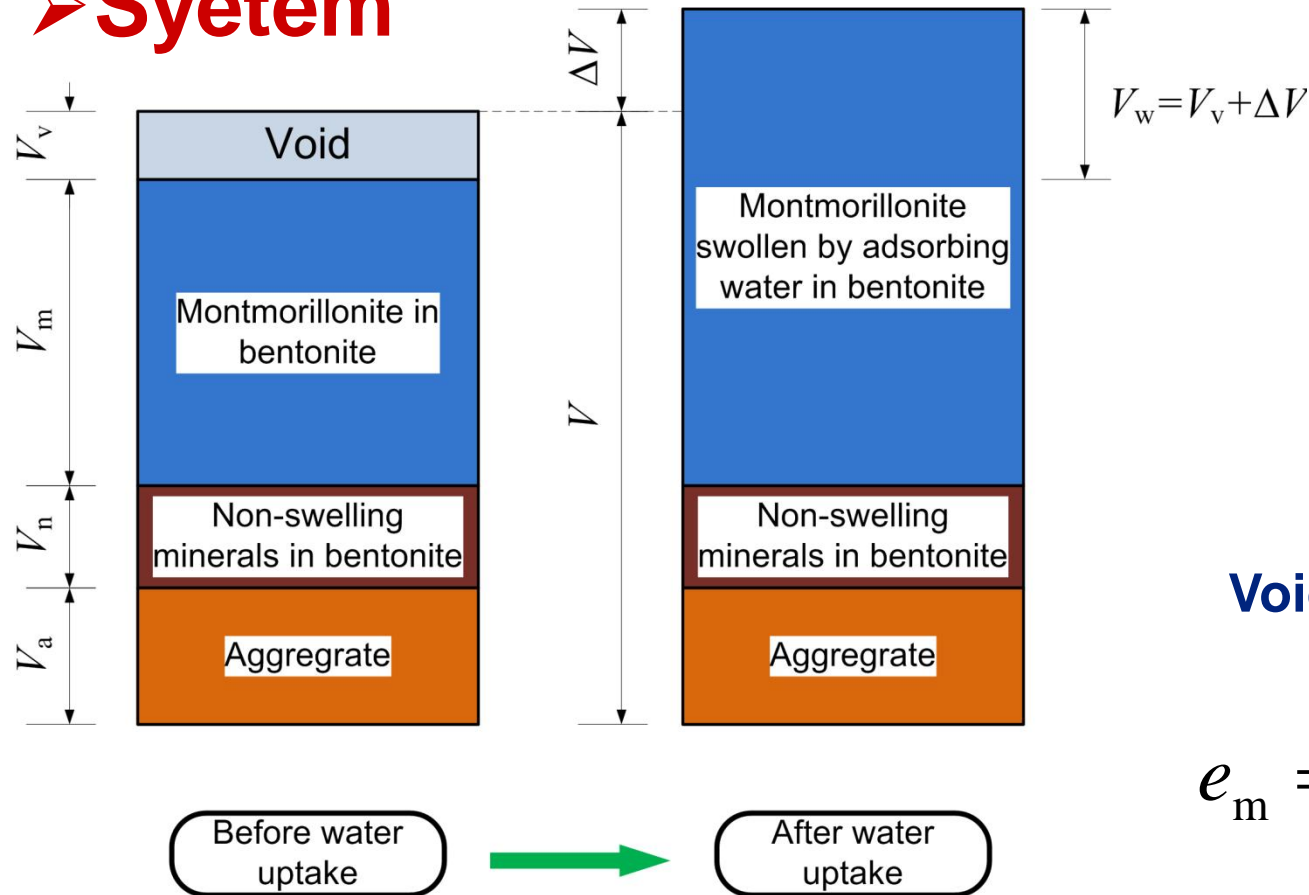


Cation Demixing



Model Development

➤ Syetem

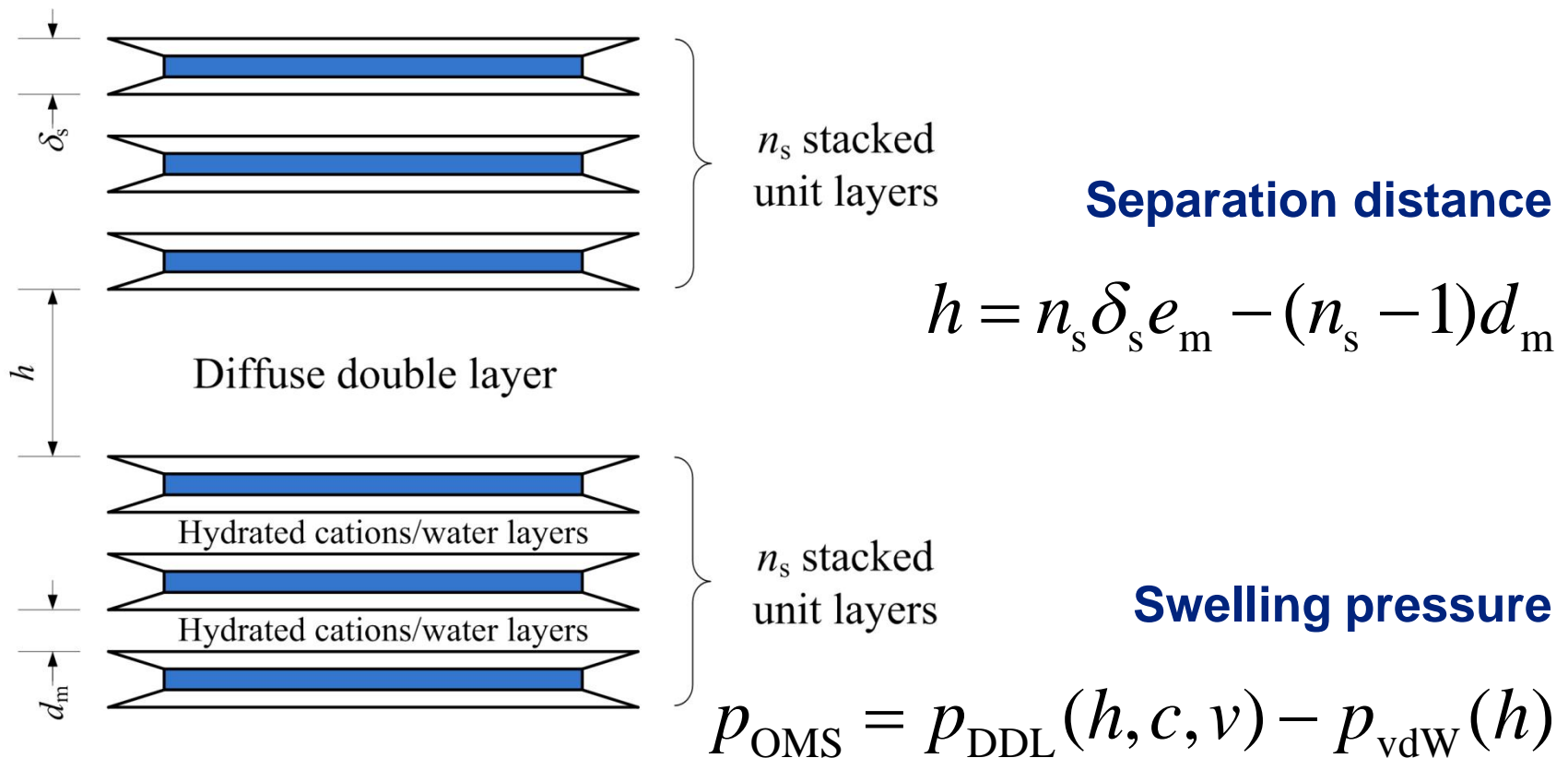


Void raio of mont.

$$e_m = e \frac{\rho_m}{\rho_s} \frac{1}{\alpha C_m}$$

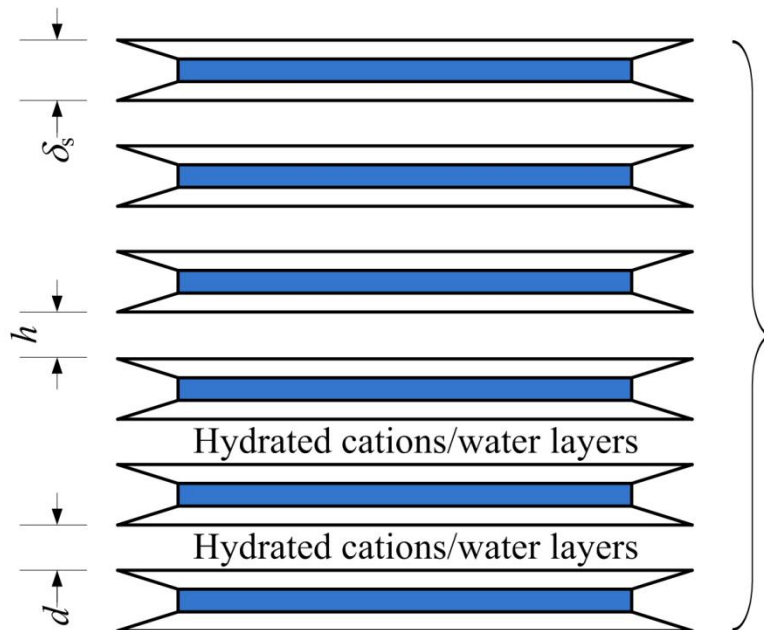
Model Development

➤ Fully developed osmotic swelling



Model Development

➤ Just initiated crystalline swelling



n_s stacked
unit layers

$n_s \rightarrow \infty$
 $d < d_m$

Separation distance

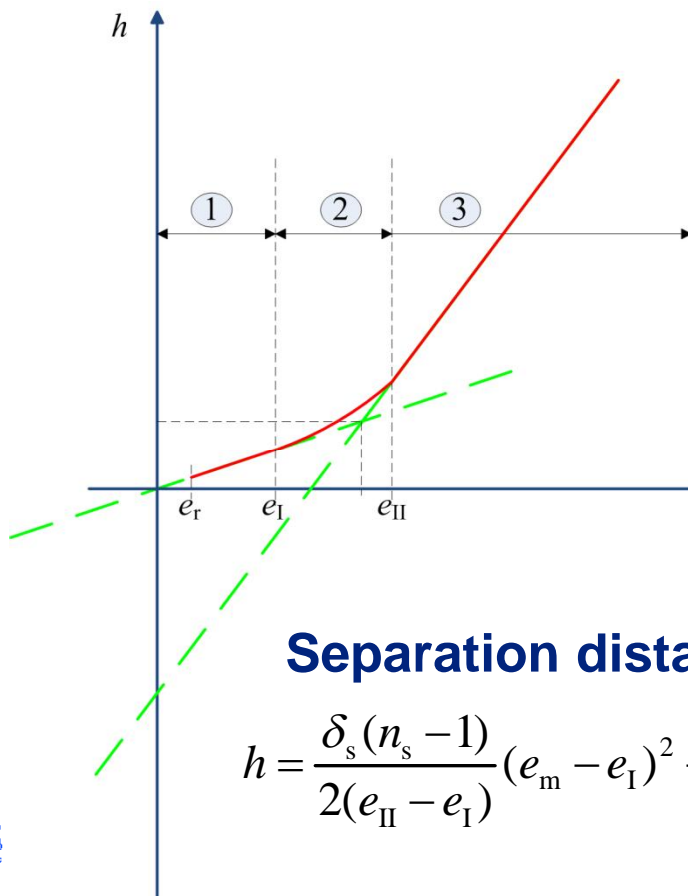
$$h = \delta_s e_m$$

Swelling pressure

$$p_{\text{CSS}} = s = k \exp(-h/l)$$

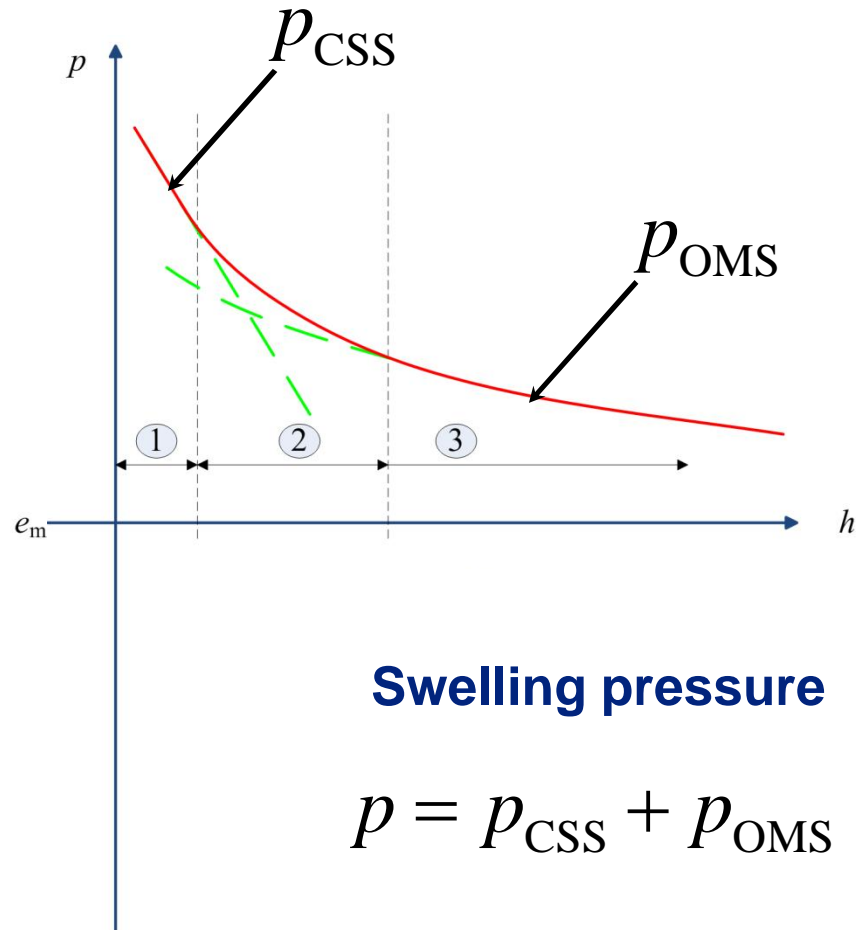
Model Development

➤ Transition region



Separation distance

$$h = \frac{\delta_s (n_s - 1)}{2(e_{II} - e_I)} (e_m - e_I)^2 + \delta_s e_m$$

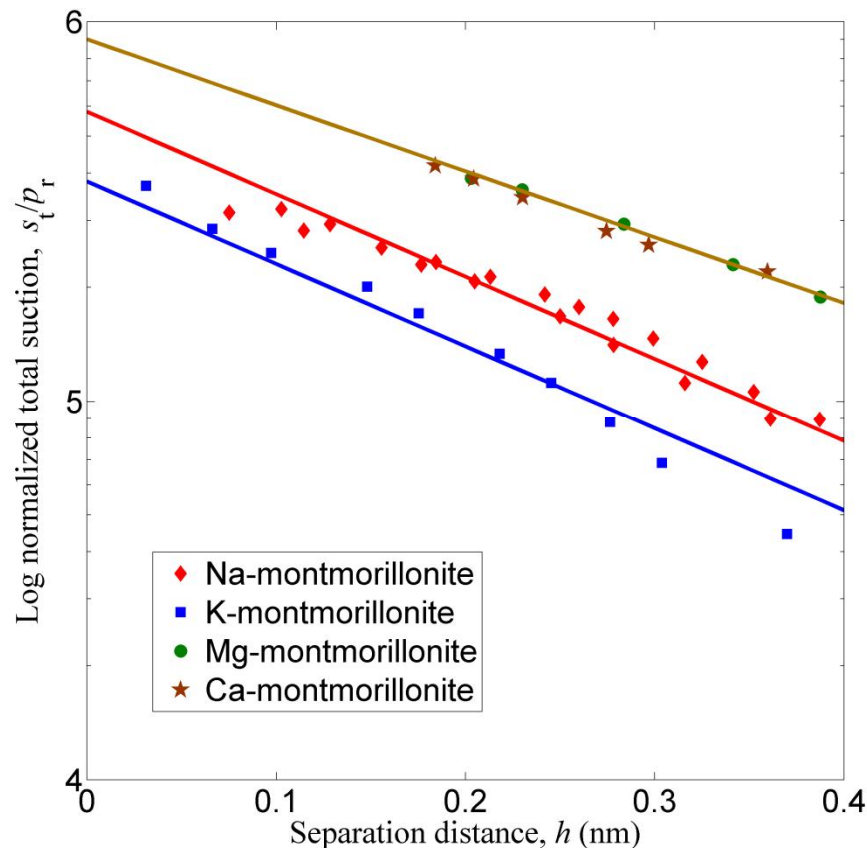


Swelling pressure

$$p = p_{\text{CSS}} + p_{\text{Oms}}$$

Model Parameters

➤ Determination of k and l

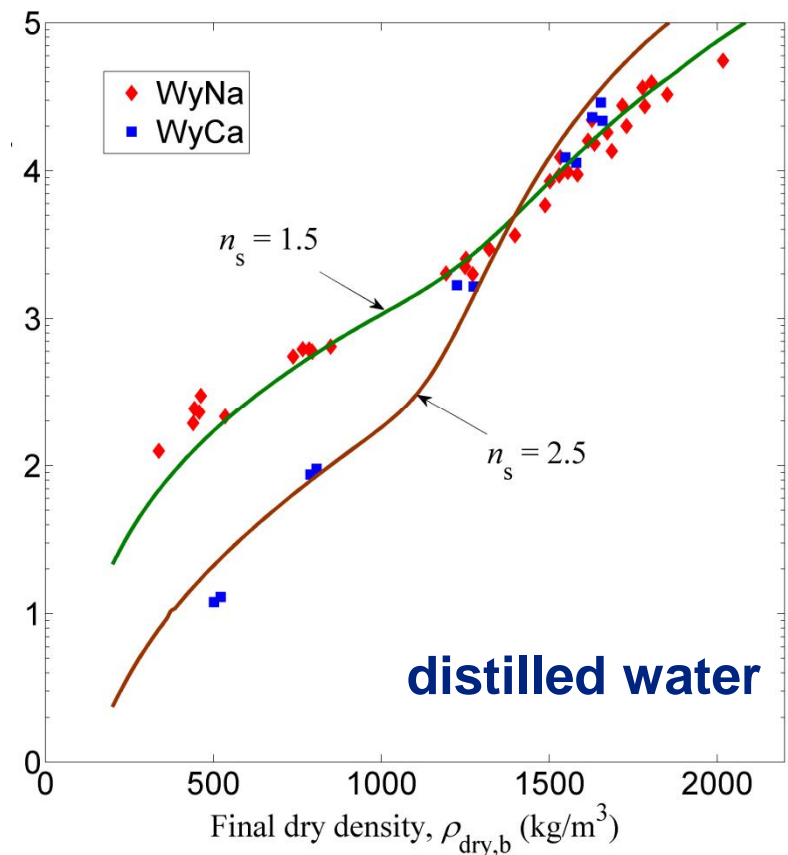
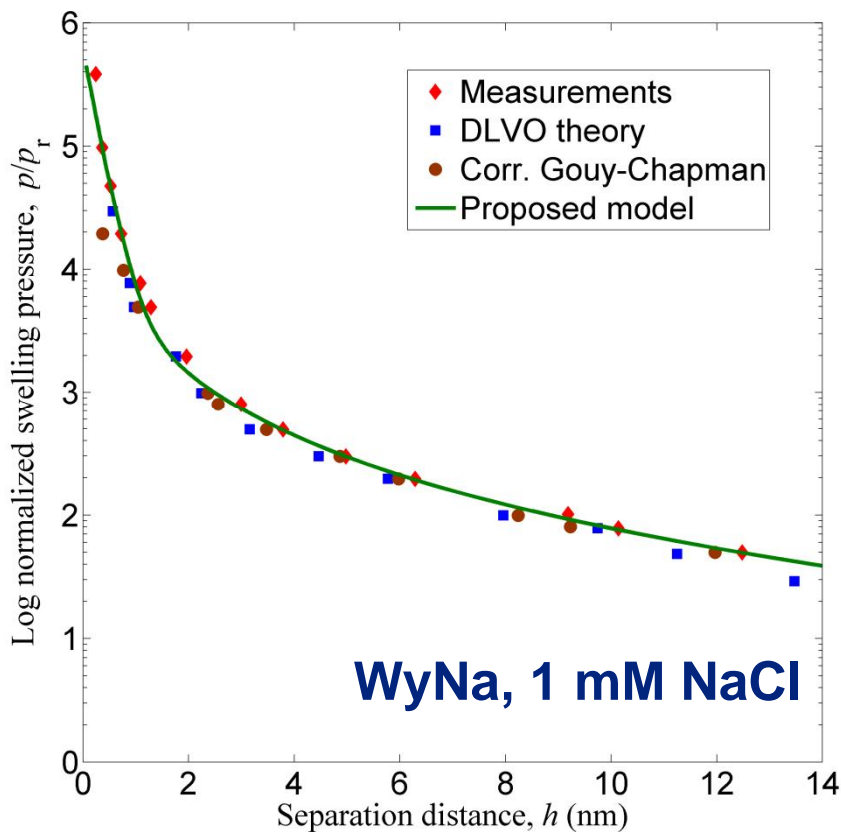


- The only unknown parameter is n_s
- The others can be determined independently

Types	Pre-exponential factor k (Pa)	Decay length l (nm)
Na-mont.	5.8×10^8	0.20
K-mont.	3.8×10^8	0.20
Mg-mont.	9.0×10^8	0.25
Ca-mont.	9.0×10^8	0.25

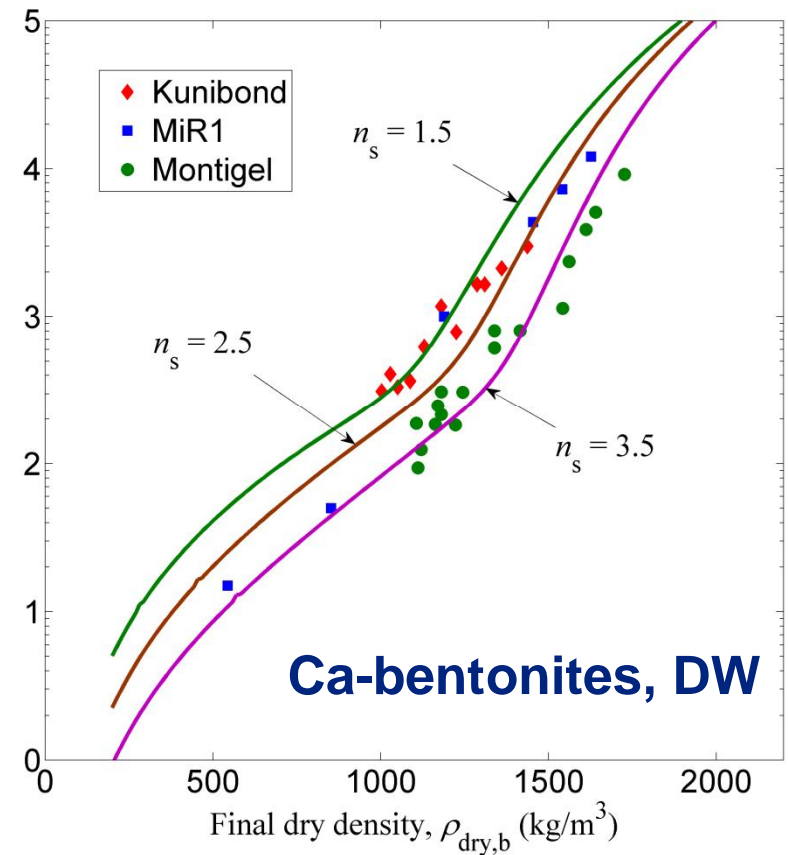
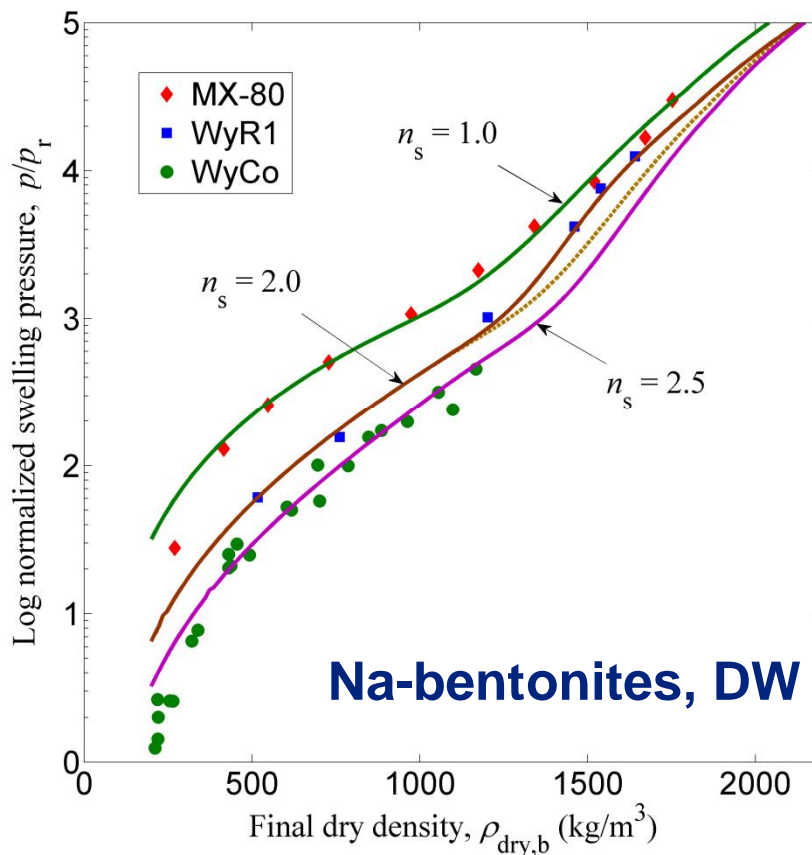
Model Predictions

➤ Benchmark tests



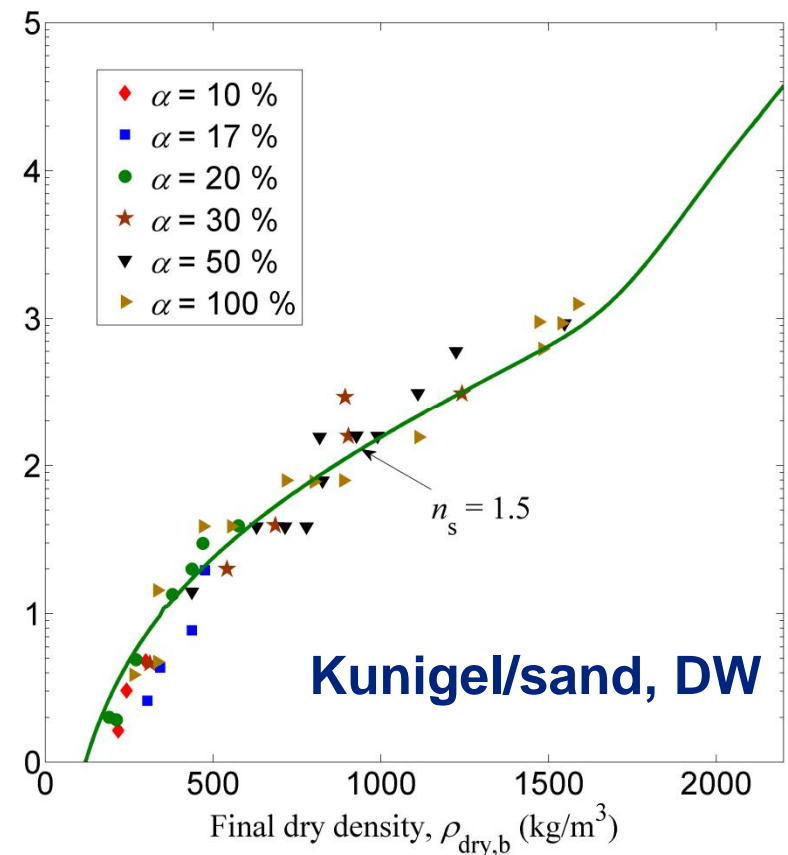
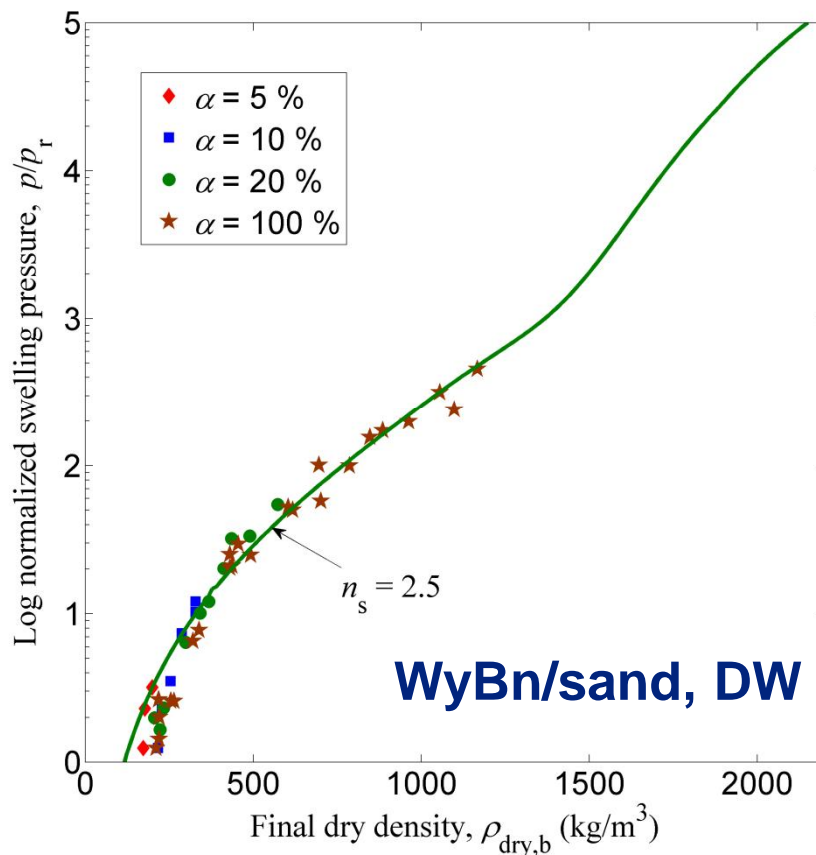
Model Predictions

➤ Natural bentonites



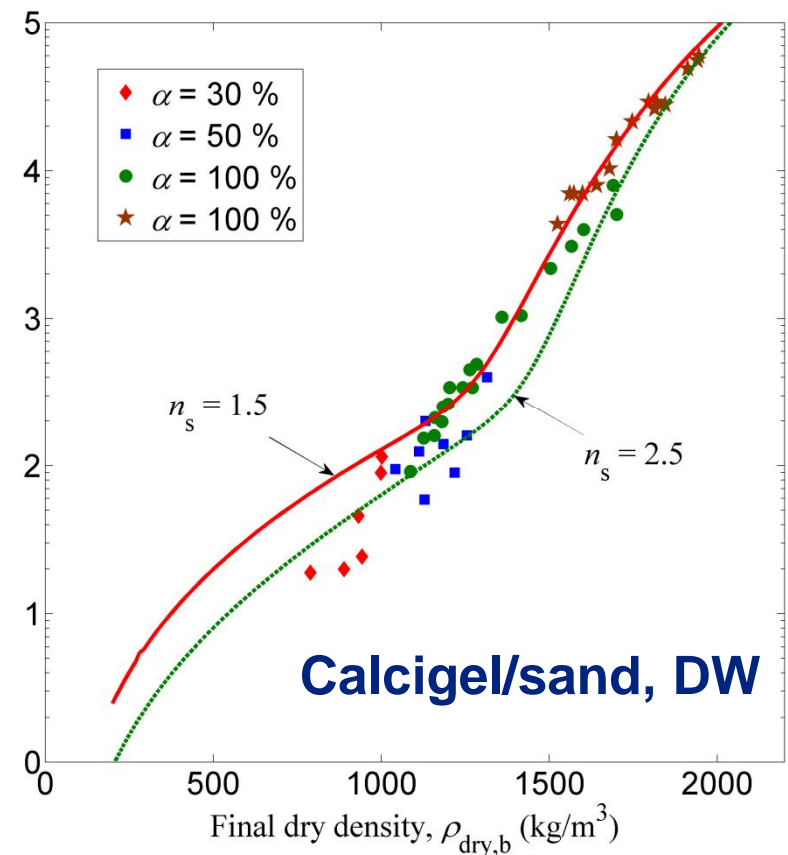
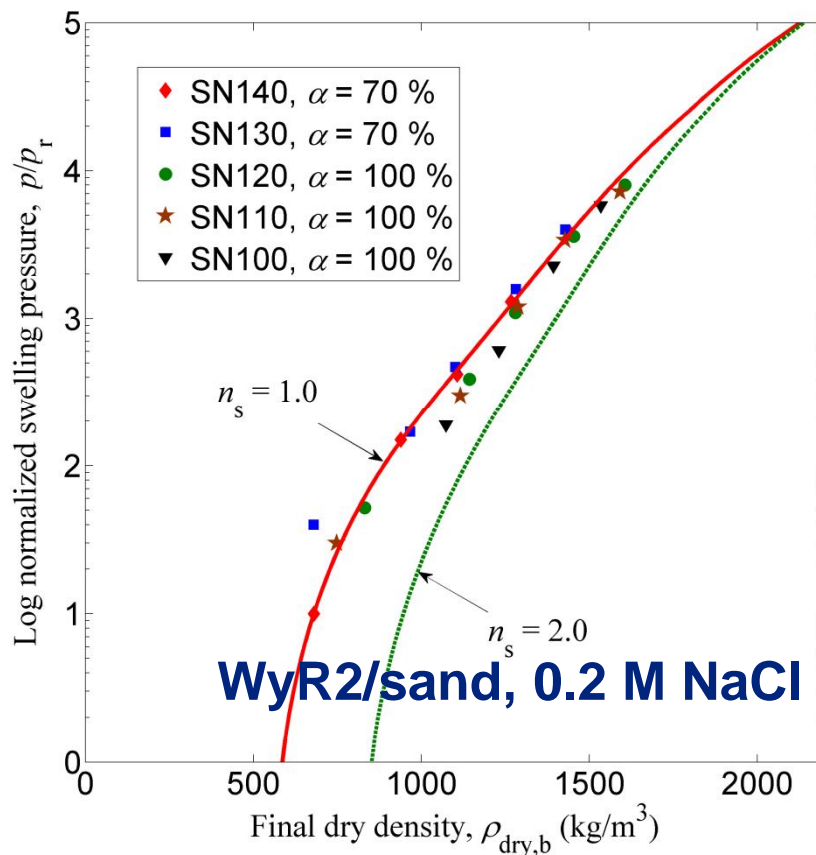
Model Predictions

➤ Bentonite/sand mixtures



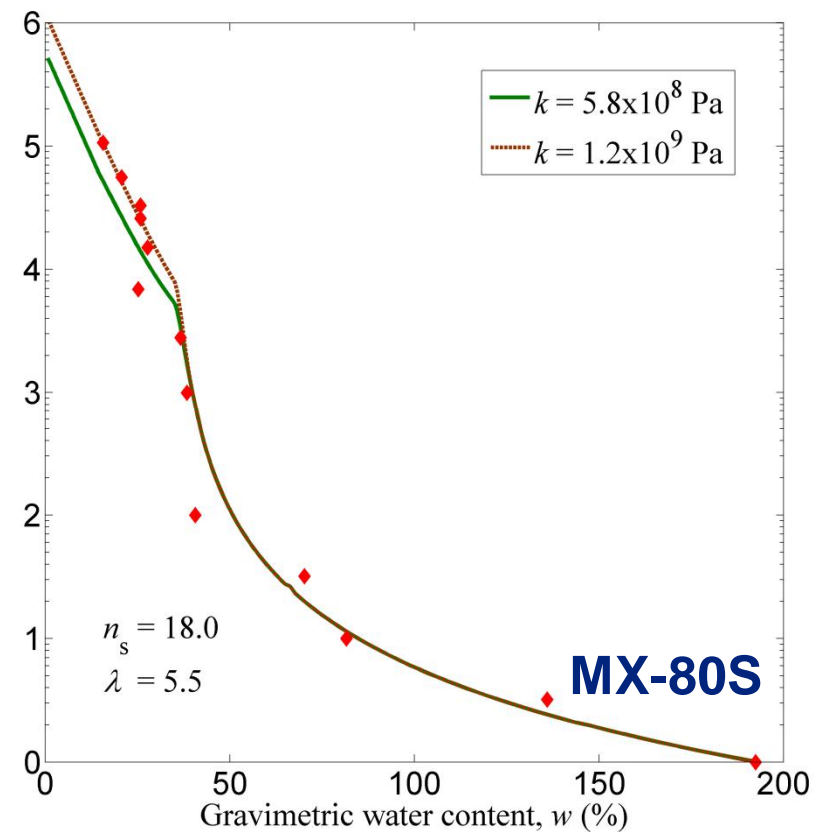
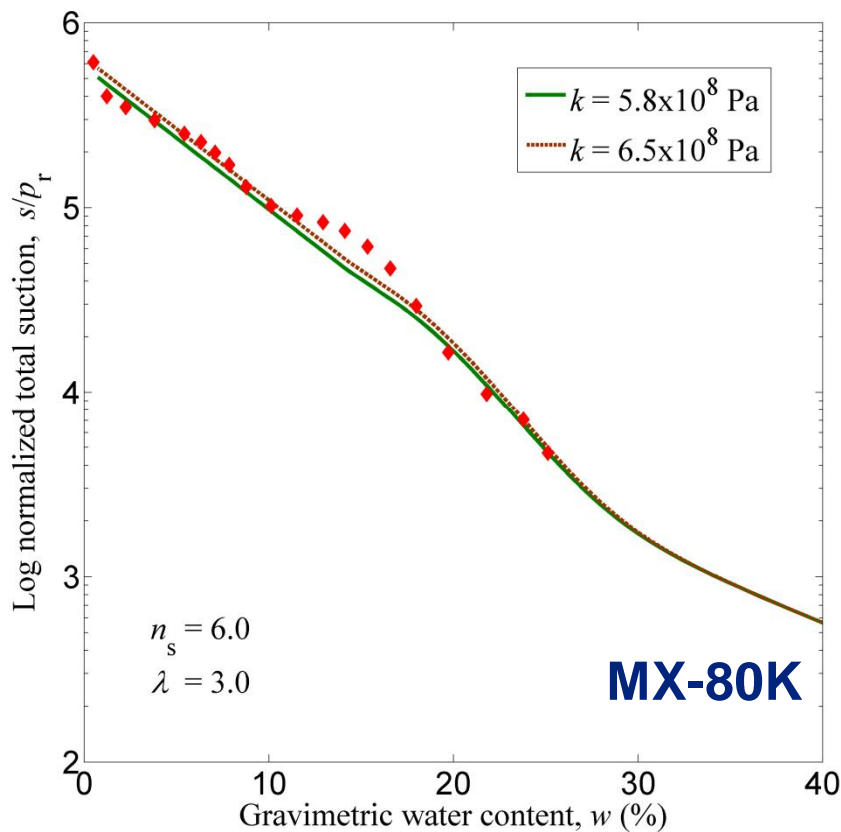
Model Predictions

➤ Bentonite/sand mixtures



Model Predictions

➤ Water retention curves



Conclusions

- A mechanistic model is developed
- The predictions agree well with experiments
- The only unknown parameter is n_s
- It also works well for water retention curves
- The n_s parameter and its dependence on the types of bentonite and the electrolyte, etc. need to be further investigated